

CM01 – Concrete and Masonry Structures 1 HW6 – Slab supported on four sides



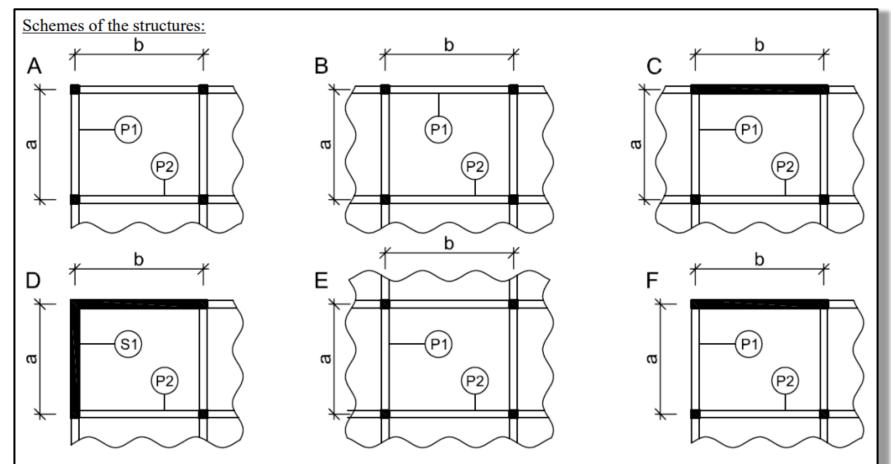
Author: Jakub Holan Last update: 24.10.2023 13:55

Task 2



Task 2 – Slab supported on four sides

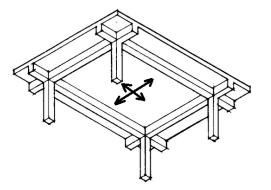
In Task 2, two-way slab supported on four sides will be designed.

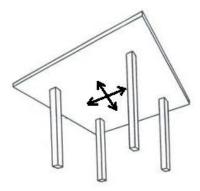


beton4life

Comparison of Tasks 1 to 3

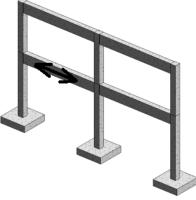






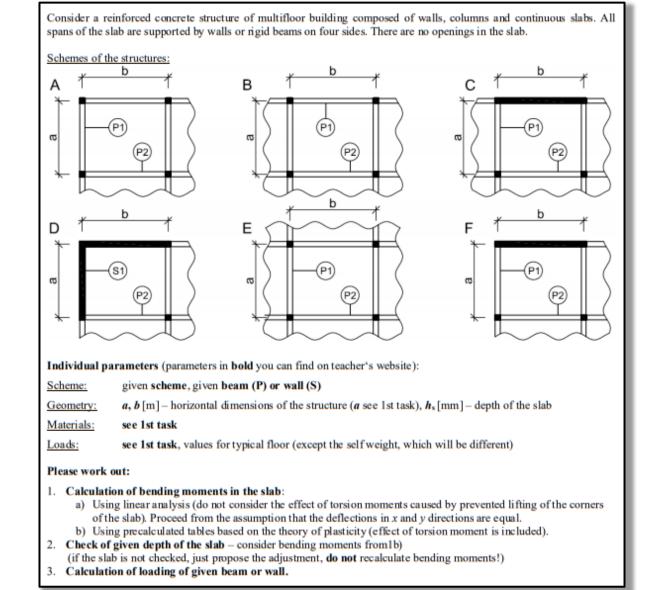
Two-way slab supported on 4 sides – **Task 2**

Two-way flat slab – **Task 3**



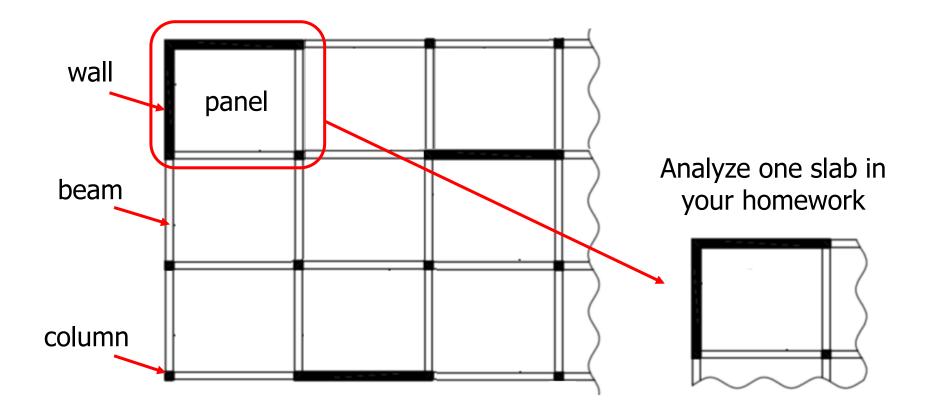
■ Beam (frame) – ■ beton4life Task 1

Task 2 – Assignment



beton4life

Task 2 – Assignment



Task 2 – Assignment goals

Our goal will be to:

1) Calculate **bending moments**:

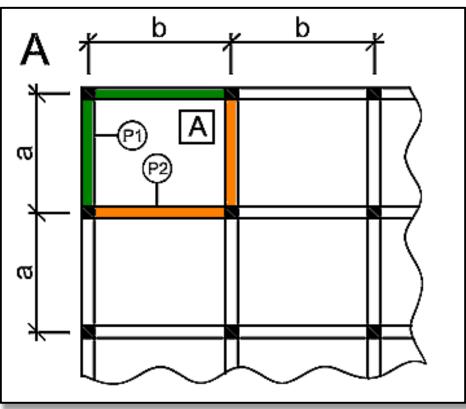
- using calculation based on linear analysis,
- using precalculated tables based on the theory of plasticity.
- 2) Preliminarily check the slab depth*.
- 3) Calculate loading of a supporting element (beam or wall).

Supports and static schemes

Supports

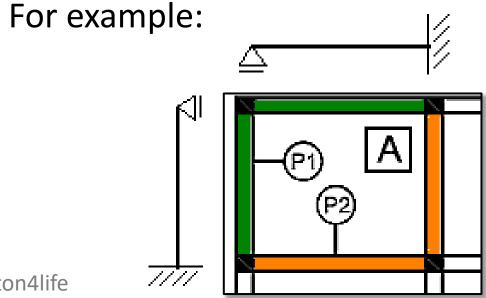
Based on the real supports of the slab, we must identify support types:

- fixed support for wall and inner beam,
- hinged (point) support for outer beam.



Static schemes

Based on the support types, we can determine static scheme in each direction: ~ 1 $\langle \cdot |$



Loading of the slab

Loading of the slab

Before any calculations, we must first **calculate the total area load** on the slab. The slab is loaded by:

- self-weight,
- other dead loads,
- live loads.

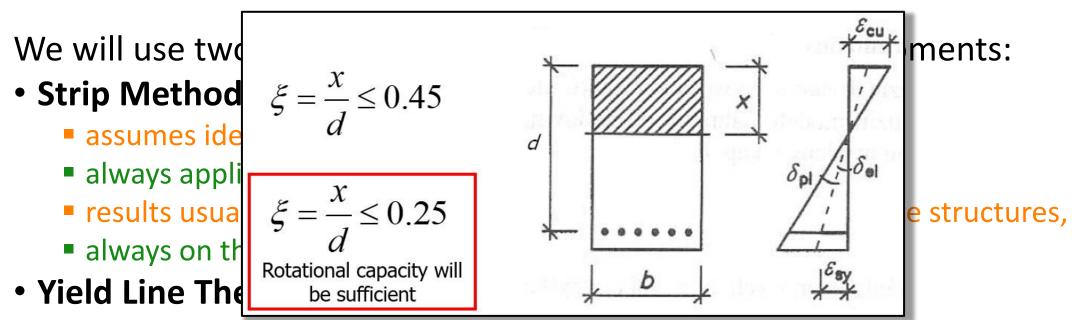
Do the calculation in a table!

We will use two methods for the calculation of bending moments:

- Strip Method (based on elastic theory)
 - assumes ideally linear behaviour of materials,
 - always applicable,
 - results usually not close to real behaviour of reinforced-concrete structures,
 - always on the safe side.

• Yield Line Theory (based on plastic theory)

- assumes ideally plastic behaviour of materials,
- NOT always applicable (sufficient plastic hinge rotational capacity is necessary),
- results close to real behaviour of reinforced-concrete structures,
- NOT always on the safe side.



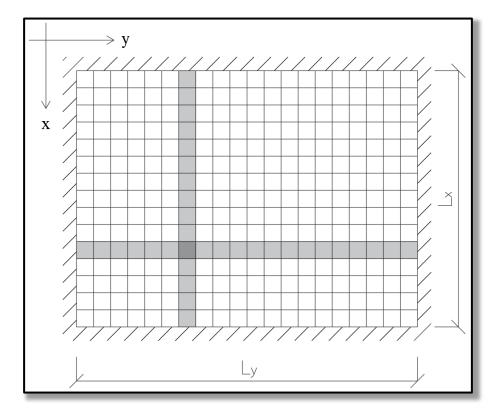
- assumes ideally plastic behaviour of materials,
- NOT always applicable (sufficient plastic hinge rotational capacity is necessary),
- results close to real behaviour of reinforced-concrete structures,
- NOT always on the safe side.

Bending moments – Strip Method

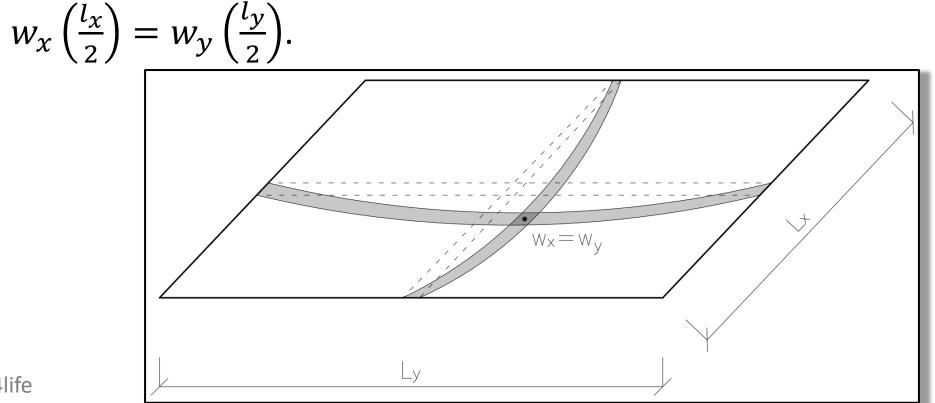


Strip Method (elastic)

In this method, we assume that the slabs consists of **two perpendicular sets of strips**, and we calculate the **loading and moments in the two directions individually**.



First, we must calculate the value of load in each direction (f_x and f_y). We calculate these values using the assumption that the deflection of the slab in both directions must be the same



Using the equation for deflection in the middle of a beam

$$w = k \frac{f l^4}{EI},$$

we can derive:

$$w_{x}\left(\frac{l_{x}}{2}\right) = w_{y}\left(\frac{l_{y}}{2}\right)$$
$$k_{x}\frac{f_{x}l_{x}^{4}}{EI} = k_{y}\frac{f_{y}l_{y}^{4}}{EI},$$
$$f_{y} = f_{x}\frac{k_{x}l_{x}^{4}}{k_{y}l_{y}^{4}}.$$

$$k = \frac{1}{384}$$

$$k = \frac{2}{384}$$

$$k = \frac{5}{384}$$

As the sum of the loads in both directions must be equal to total area load

$$f = f_x + f_y.$$

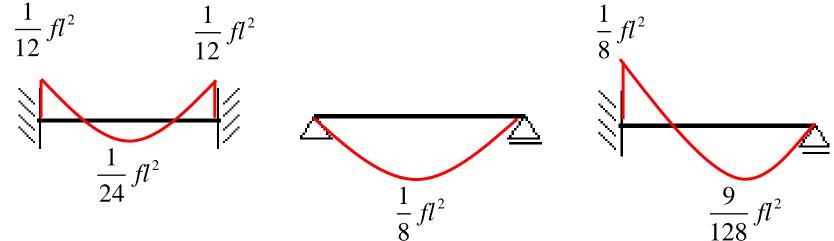
we can derive

$$f = f_x + f_x \frac{k_x l_x^4}{k_y l_y^4},$$
$$f_x = \frac{f}{1 + \frac{k_x l_x^4}{k_y l_y^4}}.$$

The final equations for loads in each direction are:

$$f_x = \frac{f}{1 + \frac{k_x l_x^4}{k_y l_y^4}}$$
$$f_y = f - f_x$$

Using the loads in individual directions (f_x and f_y), we can calculate bending moments in each direction using these values for given static scheme.



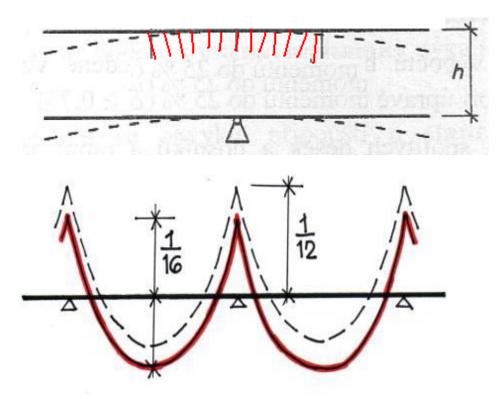
We calculate the moments on strips of 1 m width. The load is therefore: $f_{lin} [kN/m] = f_{area} \cdot 1 \text{ m}$

Bending moments – Yield Line Theory



Yield Line Theory

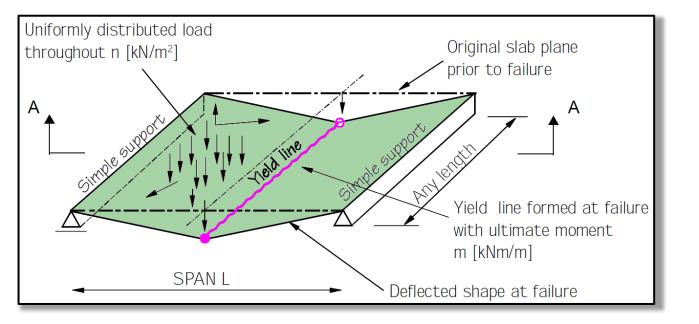
Yield Line Theory considers: **cracks** in the structure \rightarrow changes in **bending stiffness** \rightarrow **redistribution** of internal forces \rightarrow real behaviour.

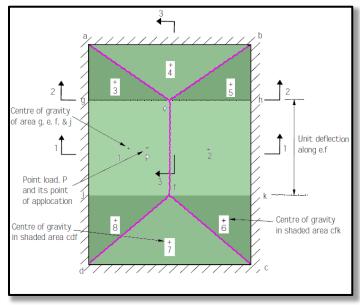


In order to use Yield Line Theory, multiple conditions must be satisfied:

- slab must have constant depth,
- supports must be rigid,
- corners must be prevented from lifting,
- adjacent panels must have same loads,
- adjacent panels must have same spans,
- reinforcement must have sufficient ductility (steel class B, C),
- rotational capacity must be sufficient ($x/d \le 0.25$).

The Yield Line Theory is based on the assumption that **local parts are** ideally plastic (like hinges) and the rest of the slab is ideally rigid.



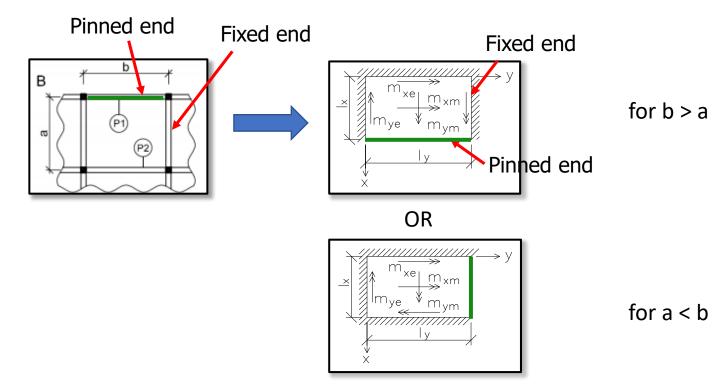


The theory is very complicated, and thus, we use tables generated using this theory.

| | | ly/lx | | | | | | | | | | |
|---|-----------|--------|--------|--------|--------|--------|-----------------|--------|--------|--------|--------|--------|
| Typ podepření | | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.6 | 1.7 | 1.8 | 1.9 | 2.0 |
| → y | βxe | -0.032 | -0.038 | -0.043 | -0.047 | -0.051 | -0.053 | -0.057 | -0.058 | -0.060 | -0.062 | -0.064 |
| | βxm | 0.024 | 0.028 | 0.032 | 0.035 | 0.038 | 0.040 | 0.042 | 0.044 | 0.045 | 0.047 | 0.048 |
| I ^{III} ye * mym * | βуе | | | | | | -0.032 | | | | | |
| <u>}</u> | βym | 0.024 | | | | | | | | | | |
| × | | | | | | | | | | | | |
| y | βxe | -0.038 | -0.044 | -0.048 | -0.052 | -0.055 | -0.058 | -0.060 | -0.062 | -0.064 | -0.066 | -0.067 |
| | βxm | 0.029 | 0.033 | 0.036 | 0.039 | 0.041 | 0.043 | 0.045 | 0.047 | 0.048 | 0.049 | 0.051 |
| | βуе | | | | | | -0.038 | | | | | |
| | βym 0.029 | | | | | | | | | | | |
| × | | | | | | | | | | | | |
| x mxe mye mymye x x x x x x x y y y y y y y y y y y y y | βxe | -0.038 | -0.048 | -0.056 | -0.062 | -0.068 | -0.072 | -0.077 | -0.080 | -0.083 | -0.087 | -0.090 |
| | βxm | 0.029 | 0.036 | 0.042 | 0.046 | 0.051 | 0.054 | 0.058 | 0.060 | 0.063 | 0.065 | 0.067 |
| | βye | | | | | | -0.038 | | | | | _ |
| Å ∧ ∧ | βym | | | | | | 0.029 | | | | | |
| | 0 | 0.047 | 0.055 | 0.052 | 0.000 | 0.074 | 0.070 | 0.000 | 0.005 | 0.000 | 0.001 | 0.004 |
| $\begin{array}{c} \downarrow \\ x \\$ | βxe | -0.047 | -0.055 | -0.063 | -0.069 | -0.074 | -0.078 | -0.083 | -0.085 | -0.088 | -0.091 | -0.094 |
| | βxm | 0.035 | 0.042 | 0.047 | 0.051 | 0.056 | 0.058 | 0.062 | 0.064 | 0.066 | 0.068 | 0.070 |
| | βуе 0 | | | | | | -0.047 0.035 | | | | | |
| × | βym | | | | | | 0.055 | | | | | _ |
| $\begin{array}{c} \xrightarrow{m_{xe_1} m_{xm}} & y \\ \xrightarrow{m_{xe_1} m_{xm}} & \xrightarrow{y} \\ \xrightarrow{w_{m_{ym}}} & y \\ \xrightarrow{w_{m_{ym}}} & y \\ y \\ \xrightarrow{y} & y \end{array}$ | βxe | -0.046 | -0.051 | -0.055 | -0.058 | -0.061 | -0.063 | -0.065 | -0.067 | -0.068 | -0.070 | -0.071 |
| | βxm | 0.035 | 0.038 | 0.033 | 0.030 | 0.045 | 0.047 | 0.005 | 0.007 | 0.051 | 0.052 | 0.053 |
| | βуе | 0.055 | 0.030 | 0.041 | 0.045 | 0.045 | 0.047 | 0.045 | 0.050 | 0.051 | 0.052 | 0.055 |
| | βym | | | | | | 0.035 | | | | | _ |
| x | P7 | | | | | | | | | | | _ |
| Y Y | βxe | | | | | | 0 | | | | | _ |
| × | βxm | 0.035 | 0.046 | 0.057 | 0.065 | 0.073 | 0.079 | 0.085 | 0.089 | 0.093 | 0.097 | 0.101 |
| lmye * mym * | βye | | | | | | -0.046 | | | | | |
| | βym | | | | | | 0.035 | | | | | |
| x | | | | | | | | | | | | |
| × mxe mxm * mym | βxe | -0.058 | -0.066 | -0.072 | -0.077 | -0.082 | -0.085 | -0.090 | -0.092 | -0.095 | -0.097 | -0.100 |
| | βxm | 0.044 | 0.049 | 0.054 | 0.058 | 0.062 | 0.064 | 0.067 | 0.069 | 0.071 | 0.073 | 0.075 |
| | βуе | | | | | | 0 | | | | | |
| | βym | | | | | | 0.044 | | | | | |
| X | | | | | | | | | | | | |
| x mye ¥mym | βxe | | | | | | 0 | | | | | |
| | βxm | 0.044 | 0.055 | 0.065 | 0.072 | 0.080 | 0.085 | 0.091 | 0.095 | 0.099 | 0.102 | 0.106 |
| | βуе | | | | | | -0.058 | | | | | |
| ly ly | βym | | | | | | 0.044 | | | | | |
| × | <u> </u> | | | | | | | | | | | |
| × mxm * mym | βxe | | | | | | 0 | | | | | |
| | βxm | 0.056 | 0.066 | 0.075 | 0.082 | 0.089 | 0.093 | 0.099 | 0.102 | 0.106 | 0.109 | 0.113 |
| | βye | | | | | | 0 | | | | | |
| y ly | βym | | | | | | 0.056 | | | | | |
| 3 | | | _ | _ | _ | _ | | _ | _ | _ | _ | |

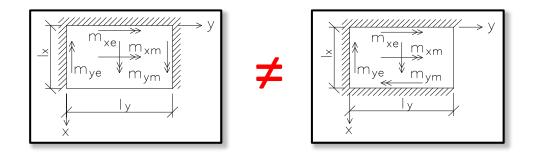


When using the tables, we first select the type of the panel based on the assigned panel.



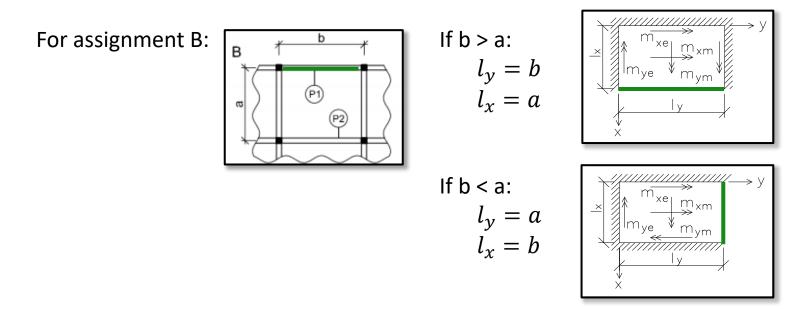
When using the tables, we first select the type of the panel based on the assigned panel.

Be careful when selecting the type of the panel!



Then we calculate ratio of spans (l_y/l_x) .

Be careful assigning a and b to l_x and l_y ! For all panel types, l_x is the shorter span.

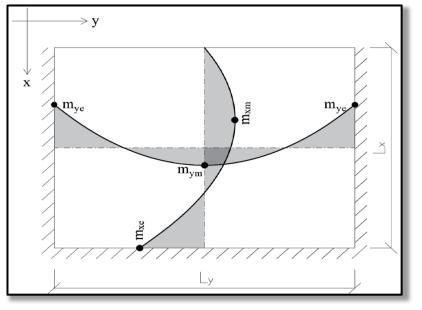


Using the selected type of panel and calculated ratio of spans, we lookup β_{ii} coefficients in the table. (Use linear interpolation to calculate β_{xi} coefficients.)

| | | ly/lx | | | | | | | | | | |
|---|-----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Typ podepření | | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.6 | 1.7 | 1.8 | 1.9 | 2.0 |
| $ \begin{array}{c} & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & $ | βxe | -0.032 | -0.038 | -0.043 | -0.047 | -0.051 | -0.053 | -0.057 | -0.058 | -0.060 | -0.062 | -0.064 |
| | βxm | 0.024 | 0.028 | 0.032 | 0.035 | 0.038 | 0.040 | 0.042 | 0.044 | 0.045 | 0.047 | 0.048 |
| | βye | | | | | | -0.032 | | | | | |
| | βym | | | | | | 0.024 | | | | | |
| × | | | | | | | | | | | | |
| $\xrightarrow{x} \xrightarrow{m_{xe}} \xrightarrow{m_{xm}} \xrightarrow{y}$ | βхе | -0.038 | -0.044 | -0.048 | -0.052 | -0.055 | -0.058 | -0.060 | -0.062 | -0.064 | -0.066 | -0.067 |
| | βxm | 0.029 | 0.033 | 0.036 | 0.039 | 0.041 | 0.043 | 0.045 | 0.047 | 0.048 | 0.049 | 0.051 |
| | βуе | | | | | | -0.038 | | | | | |
| | βym | | | | | | 0.029 | | | | | |
| x | | | | | | | | | | | | |
| $\xrightarrow{\mathbf{m}} \begin{array}{c} m_{\mathbf{x}e_{\mathbf{x}e_{\mathbf{y}}}} \\ m_{\mathbf{y}e_{x}e_{y}e_{x}e_{x}e_{x}e_{x}e_{x}e_{x}e_{x}e_{x$ | βxe | -0.038 | -0.048 | -0.056 | -0.062 | -0.068 | -0.072 | -0.077 | -0.080 | -0.083 | -0.087 | -0.090 |
| | βxm | 0.029 | 0.036 | 0.042 | 0.046 | 0.051 | 0.054 | 0.058 | 0.060 | 0.063 | 0.065 | 0.067 |
| | βye | -0.038 | | | | | | | | | | |
| | βym | 0.029 | | | | | | | | | | |
| × | | | | | | | | | | | | |

Calculate the bending moments using the following equations.

 $m_{\rm xe} = \beta_{\rm xe} m_0$ $m_{\rm xm} = \beta_{\rm xm} m_0$ $m_{\rm ye} = \beta_{\rm ye} m_0$ $m_{\rm ym} = \beta_{\rm ym} m_0$ $m_0 = f_{\rm d} \cdot l_{\rm x}^2$ Basic value of bending moment.



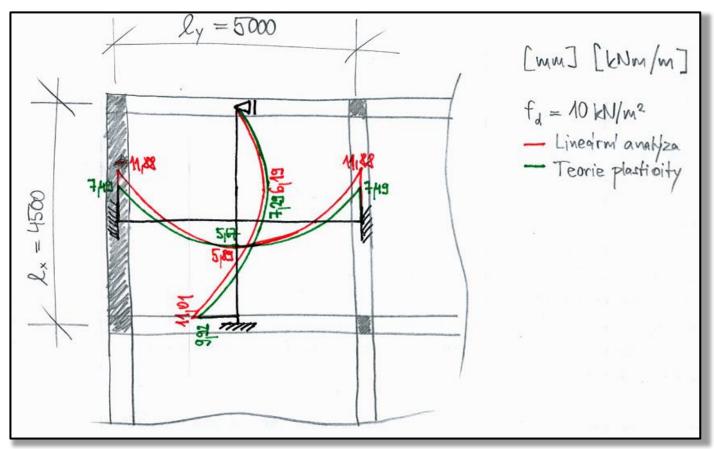
Indices:

- x, y directions of a moments (m_x is the moment in the direction of $I_{\rm v}$)
- m midspan moment
- e support (edge) moment ٠

Bending moments – schemes

Bending moments – schemes

Compare elastic (Strip Method) and plastic (Yield Line Theory) moments in one scheme.



Design of reinforcement

Design of reinforcement

In the homework, you **DO NOT HAVE TO design the reinforcement**.

Just remember, that the procedure of design of bending reinforcement for two-way slabs is almost identical to beams (see HW3).

The only difference is that you design the **reinforcement in 2 directions** and that the **width of the cross-section is taken as b = 1 m**.

Preliminarily check of the slab depth

Preliminarily check of the slab depth

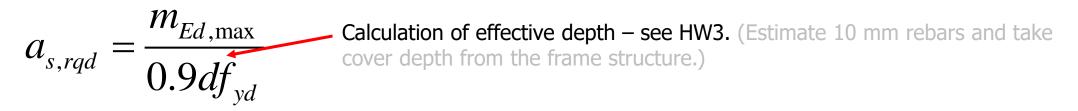
Check the given value of h_s for the **biggest moment from plastic analysis** (which we will denote as $m_{Ed,max}$).

We will check the slab from the point of view of:

- estimated area of reinforcement (can the slab be reinforced?),
- estimated compressed zone (is the rotational capacity sufficient?),
- span / depth ratio (will deflections be ok?).

Check of the slab depth – area of reinforcement

First, calculate the **required cross-sectional area of reinforcement**:



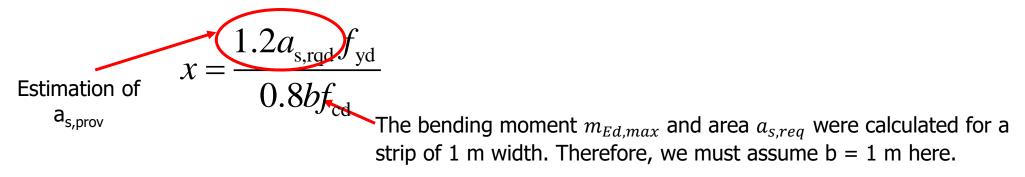
Then, calculate the **minimal and maximal area of reinforcement** ($a_{s,min}$ and $a_{s,max}$) – see HW3.

Finally, **check the condition** for the area of reinforcement:

 $a_{s,max} \ge a_{s,req} \ge a_{s,min}$

Check of the slab depth – compressed zone

First, estimate the **depth of the compressed zone**:



Then, check the condition for the relative depth of the compressed zone:

$$\frac{x}{d} \le 0.45.$$

Check of the slab depth – span/depth

Check the span/depth ratio (deflection control) – see HW1.

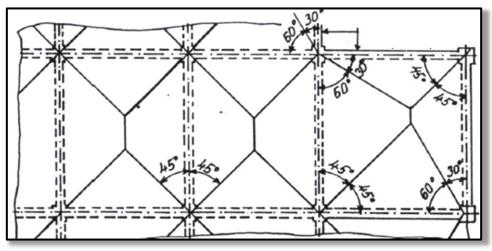
$$\begin{split} \lambda &\leq \lambda_d \\ \frac{l}{d} &\leq \kappa_{c1} \kappa_{c2} \kappa_{c3} \lambda_{d,tab} \end{split}$$

Check of the slab depth

If all of the conditions are satisfied, the assigned slab depth is suitable.

If some of the conditions are not checked, propose a solution (just describe it, don't calculate anything).

Draw tributary areas of all the supporting elements.

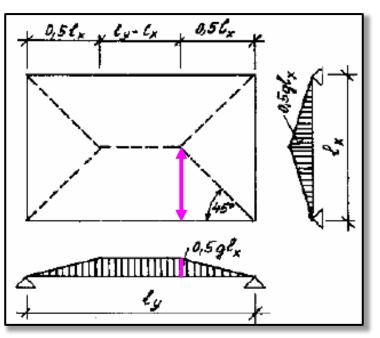


The angle between **identical supports** (fixed/fixed, pinned/pinned) is **45°**. The angle between **fixed and pinned support** is 60°.

For your given supporting element (wall or beam), draw load diagram and calculate the load.

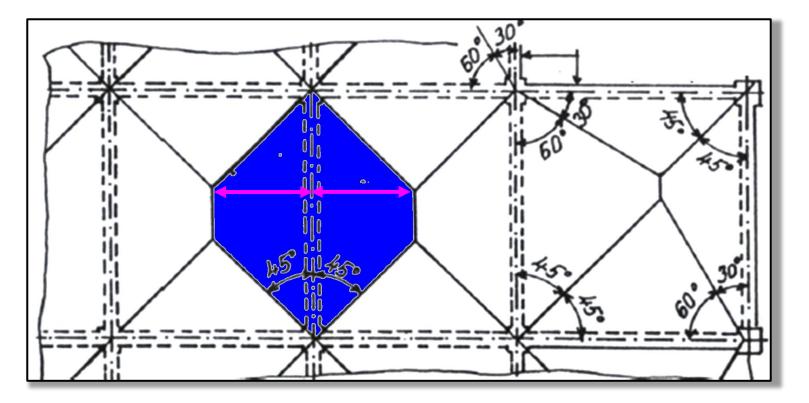
The load in each point is:

total load of the slab $(f_d) \times$ width of the tributary area





Be aware that inner walls and beams are loaded by 2 adjacent panels!



thank you for your attention



Recognitions

I thank **Assoc. Prof. Petr Bílý** for his original seminar presentation and other supporting materials from which this presentation was created.