

TASK 5: REINFORCED CONCRETE STAIRCASE1. Design of dimensions of reinforced concrete staircaseAssignment

- Height of the floor $h_f = 3700$ mm
- Depth of the main slab $h_s = 210$ mm
- Depth of floor structure $h_f = 150$ mm
- Thickness of cladding of the stair $h_c = 30$ mm

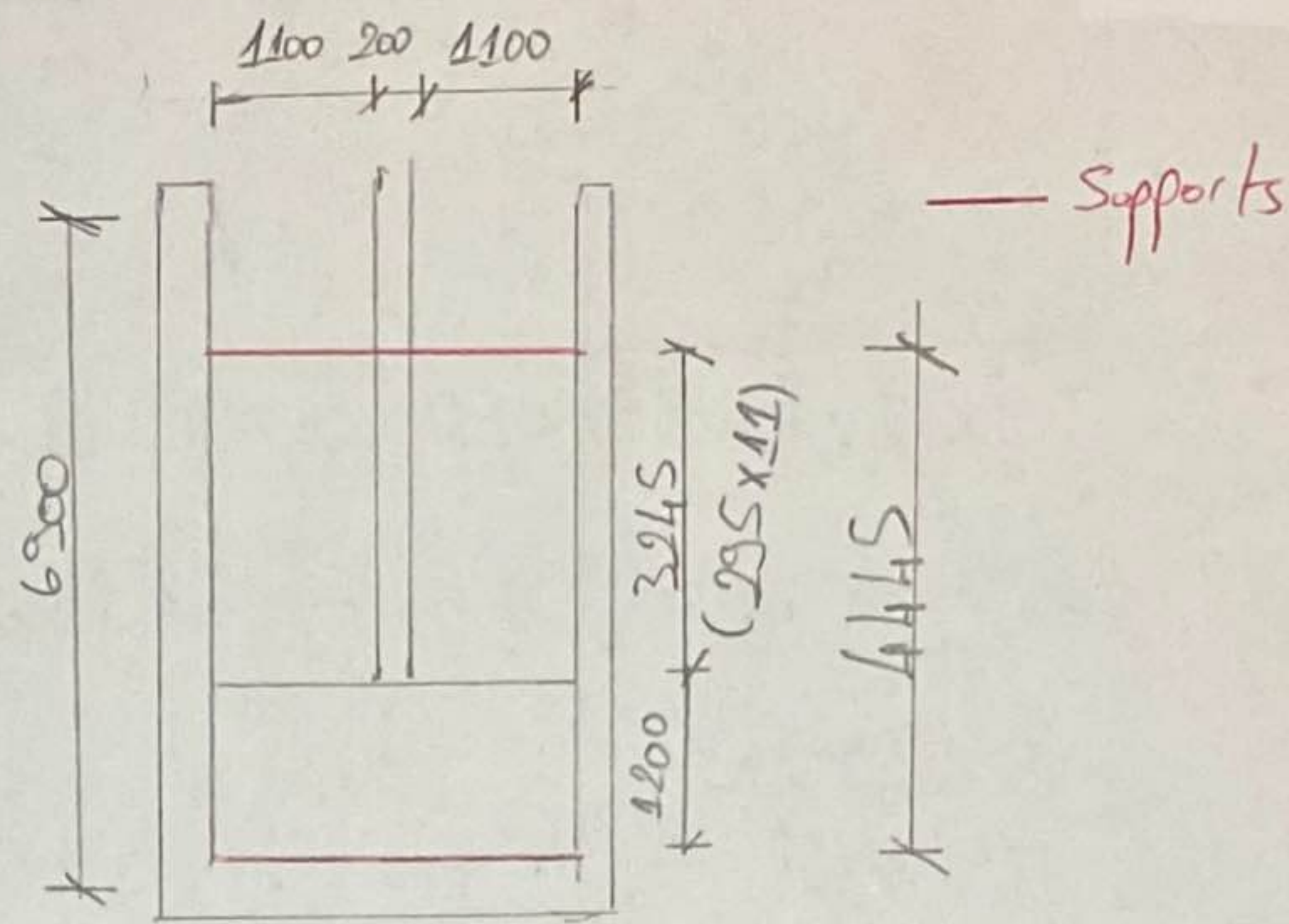
Dimensions of the staircase

- Ideal height of one step is 170 mm
- $3700/170 = 21,76 \rightarrow 22$ steps (2 flights with 11 steps)
- Height of one step $h = 3700/22 = 168$ mm
- Width of one step $b = 630 - 2h = 630 - 2 \times 168 = 294$ mm

⇒ DESIGN = Staircase with 168/295 mm steps, 2 flights, 11 steps in each flight

- Width of the flight - 1100 mm (in general, 1100 mm is the minimum width of the flight)
- Width of the gap between the flights - 200 mm (common value)
- Width of the landing - 1200 (should be at least "width of the flight + 100 mm")
- Width of the staircase is $1100 \times 2 + 200 = 2400$ mm
- Slope of the staircase is $\alpha = \arctan(168/295) \approx \underline{29,66^\circ}$

Scheme of the staircase



Preliminary check of the depth of the slab

- The staircase is considered as one way slab with span of 4445 mm. The slab will be supported \Rightarrow the depth should be at least $4445/25 = 177,8$ mm
- The depth of landings is the same as the depth of the main slab 210 mm.
- The depth of flights: 199 mm
- $210 \text{ mm} > 177,8 \text{ mm}$ and $199 \text{ mm} > 177,8 \text{ mm}$ OK!

Perpendicular and head clearance of the staircase

Head clearance of the staircase should be more than $1500 + \frac{750}{\cos \alpha}$
 $= 1500 + \frac{750}{\cos(29,66)} \approx 2363 \text{ mm}$ and more than 2100 mm

Head clearance of our staircase is $h_1 = h_k - h_s - h_f - h$

$$\Rightarrow h_1 = 3700 - 210 - 150 - 168$$

$$3172 \text{ mm} > 2363 \text{ mm} \text{ OK!}$$

Perpendicular clearance of the staircase should be more than

$$750 + 1500 \times \cos \alpha = 750 + 1500 \times \cos(29,66) = 2053 \text{ mm} \text{ and more than } 1800 \text{ mm}$$

Perpendicular clearance of our staircase is $h_2 = h_1 \cos \alpha = 3172 \cdot \cos(29,66)$

$$= 2756 \text{ mm}$$

$$> 2053 \text{ mm} \text{ OK!}$$

2. Calculations of loads

Landing

Load	Char. value [kN/m ²]	γ_F	Design value [kN/m ²]
Slab	$0,21 \cdot 25 = 5,25$	1,35	7,09
Floor	1	1,35	1,35
Live load	3,5	1,50	5,25

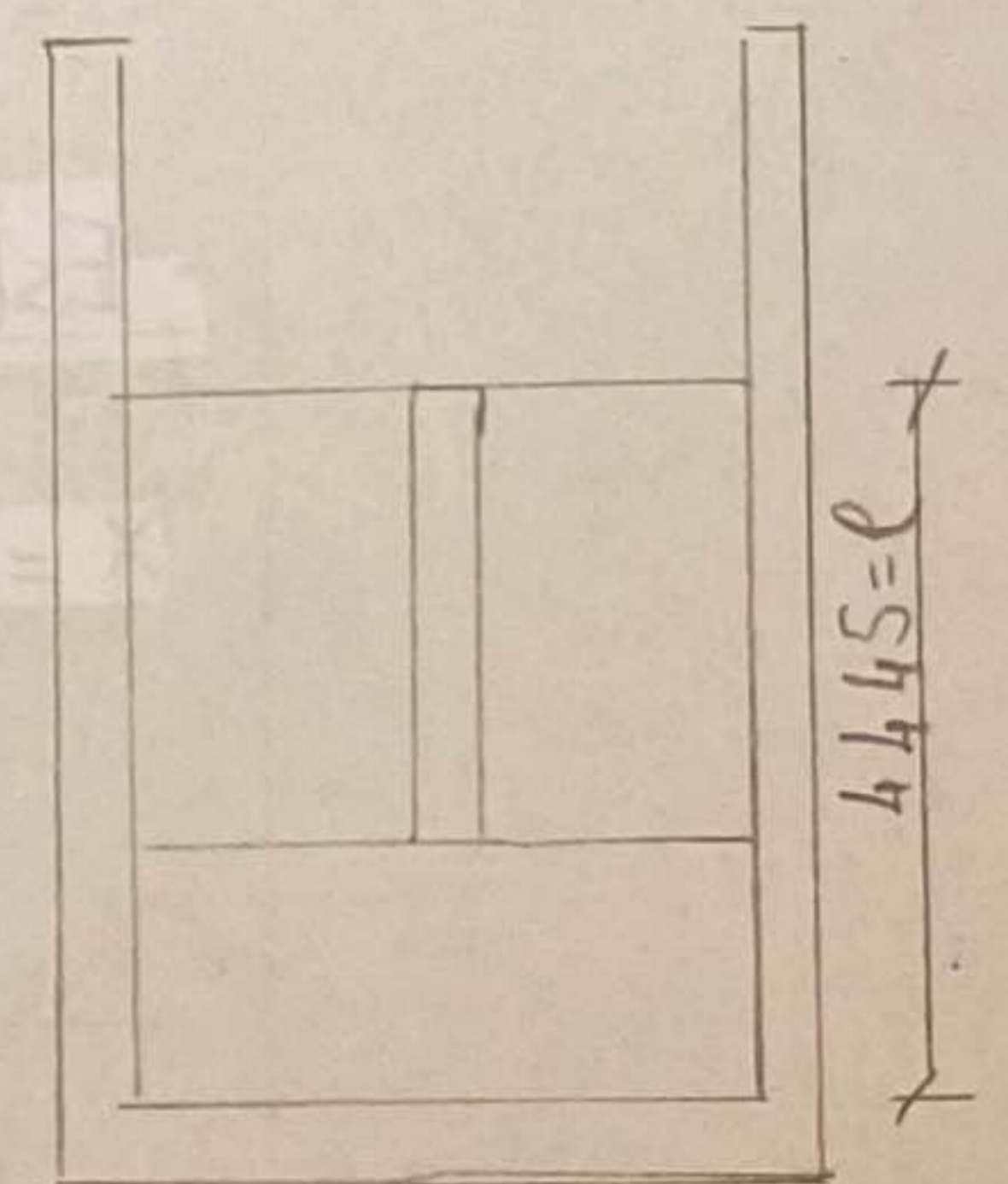
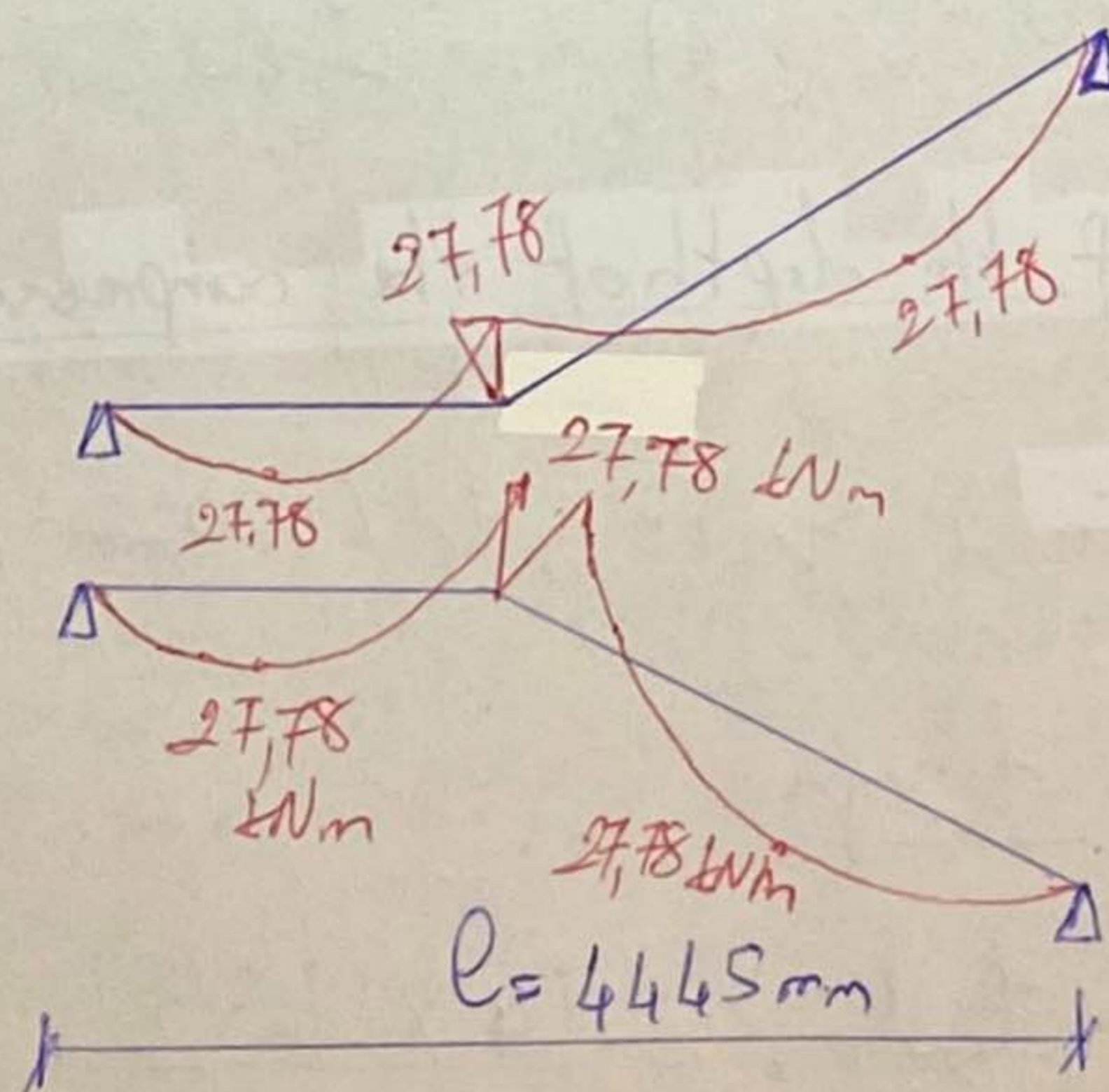
$$f_{dl} = 13,69 \text{ kN/m}^2$$

Flight

Load	Char. Value [kN/m ²]	γ_F	Design Value [kN/m ²]
Slab	$\frac{0,189}{\cos(29,66)} \times 25$	1,35	7,73
Cladding	$0,5 \cdot \frac{168 + 295}{295}$	1,35	1,06
Steps	$\frac{0,168}{2} \cdot 25$	1,35	2,83
Live load	3,5	1,5	5,25

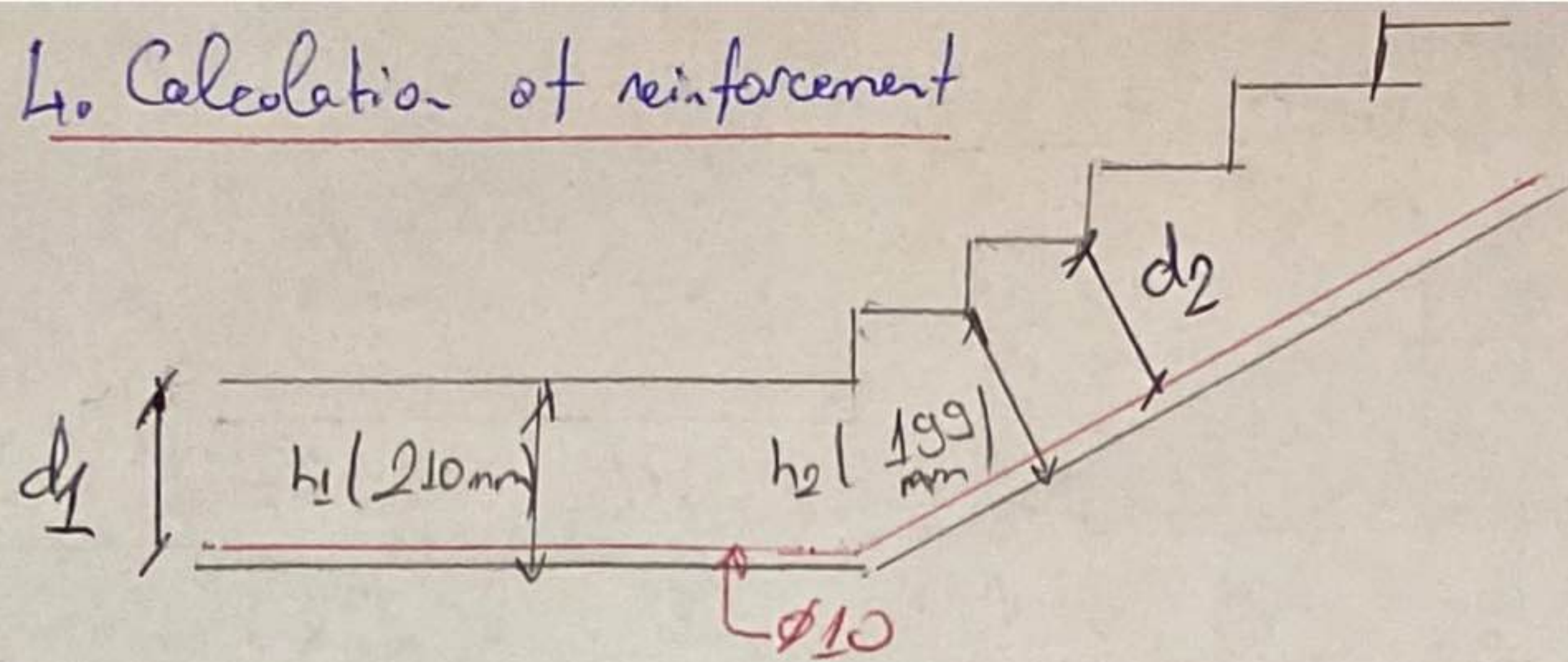
$$f_{df} = 16,87 \text{ kN/m}^2$$

3. Design bending moment



$$M_{Ed} = \frac{1}{12} f_{df} \cdot l^2 = \frac{1}{12} \times 16,87 \times 4,445^2 = 27,78 \text{ kNm}$$

4. Calculation of reinforcement



$$d_1 = h_1 - c - \frac{\phi}{2} = 210 - 25 - \frac{10}{2} = 180 \text{ mm}$$

$$d_2 = h_2 - c - \frac{\phi}{2} = 199 - 25 - \frac{10}{2} = 169 \text{ mm}$$

We keep the smallest effective depth $d = 169 \text{ mm}$. Because we use the same reinforcement for the landing and flight. The smallest effective depth allows us to be conservative although it's not economic.

$$a_{s, reqd} = \frac{M_{Ed, max}}{0,9 \cdot d \cdot f_{yd}} = \left(\frac{27,78 \times 10^3}{0,9 \cdot 0,169 \times 435 \times 10^6} \right) \times 10^4 \approx \underline{4,20 \text{ cm}^2}$$

$$a_{s, min} = \max \left(0,26 \frac{f_{ctm}}{f_{yk}} \cdot b_s \cdot d_s, 0,0013 \cdot 1,1 \cdot 0,169 \right) \times 10^4$$
$$= \max \left(0,26 \frac{2,9}{500} \cdot 1,1 \cdot 0,169; 0,0013 \cdot 1,1 \cdot 0,169 \right) \times 10^4$$
$$= \max(2,80; 2,42) = 2,80 \text{ cm}^2 < a_{s, reqd} \text{ OK!}$$

DESIGN: $\phi 10$ with spacing of 183 mm (6 x $\phi 10$)

$$a_{s, prov} = 474 \text{ mm}^2 > a_{s, reqd} (420 \text{ mm}^2) \text{ OK!}$$

Check of the design

$$x = \frac{a_{s, prov} \cdot f_{yd}}{0,8 \cdot b_s \cdot f_{cd}} = \frac{474 \times 435}{0,8 \cdot 1,1 \times 20 \times 10^6} \times 10^3 \approx \underline{11,71 \text{ mm}}$$

$$z = d_s - 0,4x$$
$$= 169 - 0,4 \cdot 11,71 = 164,32$$

$$M_{Rd} = a_{s, prov} \cdot f_{yd} \cdot z = (474 \times 435 \times 0,16432) \times 10^{-3}$$

$$33,88 > M_{Ed} (27,78 \text{ kNm}) \text{ OK!}$$

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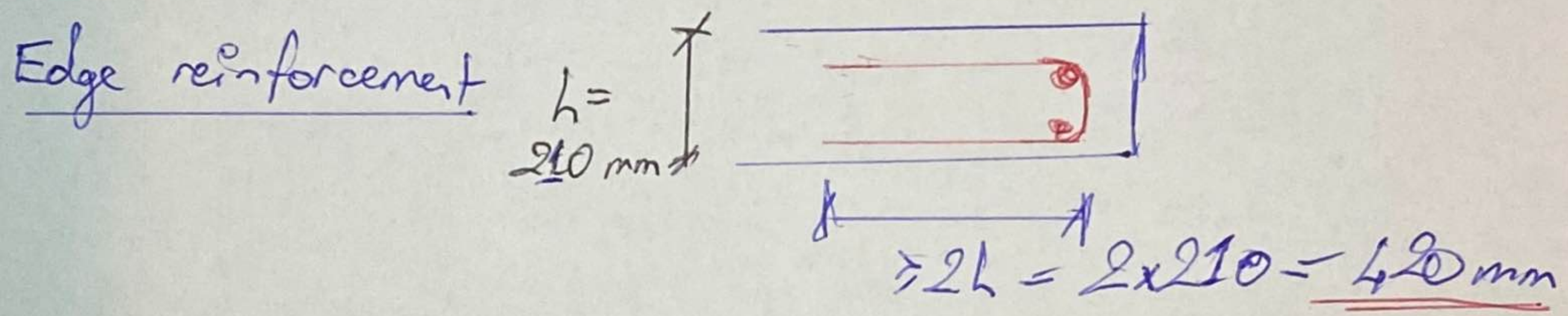
5. Detailing rules

$$\xi = \frac{x}{d} = \frac{11,71}{169} = 0,069 < 0,45 \text{ OK!}$$

Spacing of rebars

$$s_{\min}(2h; 250 \text{ mm}) \\ s_{\min}(2 \times 189; 250 \text{ mm}) = 250 \text{ mm} > 483 \text{ mm OK!}$$

6. Sketch of reinforcement



Transverse reinforcement

$$a_{s, tr} \geq 0,25 \cdot a_{s, \text{main}} \\ \geq 0,25 \times 474 \approx \underline{119 \text{ mm}^2/\text{m}}$$

$s_{tr} \leq \min(3h; 600 \text{ mm}) \\ \leq \min(3 \times 210; 600 \text{ mm}) = \underline{600 \text{ mm}}$

DESIGN! $\phi 8$ with spacing of 600 mm

$$a_{s, \text{prov}_{tr}} = \frac{1000}{4} \times 50 \text{ mm}^2 = 125 \text{ mm}^2 > a_{s, tr} (119 \text{ mm}^2/\text{m})$$

OK!