

Drawing reinforcementWiden of envelope curve:

$$\text{Section 1: } a_{l_1} = \frac{z}{2} \cot \theta = \frac{51,36}{2} \cdot 1,5 \approx \underline{38,5 \text{ cm}}$$

$$\text{Section 2: } a_{l_2} = \frac{z}{2} \cot \theta = \frac{55,3}{2} \cdot 1,5 \approx \underline{41,5 \text{ cm}}$$

$$\text{Section 3: } a_{l_3} = \frac{z}{2} \cot \theta = \frac{48,4}{2} \cdot 1,5 \approx \underline{36,3 \text{ cm}}$$

Anchorage length

$$l_{b, reqd} = \frac{\phi}{4} \cdot \frac{\sigma_{sd}}{f_{bd}}$$

$$\sigma_{sd} = f_{yd} = 435 \text{ MPa}$$

$$f_{ctd} = \frac{f_{ct, k, 0,05}}{1,5}$$

$$\text{For } \sigma_{30/37} \quad f_{ct, k, 0,05} = \underline{2 \text{ MPa}}$$

$$f_{ctd} = \frac{2}{1,5} \approx 1,33 \text{ MPa}$$

$$f_{bd} = 2,25 \cdot 21 \cdot 22 \cdot f_{ctd} \\ = 2,25 \cdot 1 \cdot 1 \cdot 1,33 \\ \approx \underline{3,00 \text{ MPa}}$$

For  $\phi = 20 \text{ mm}$

$$l_{b, reqd} = \frac{20}{4} \cdot \frac{435}{3} = \underline{725 \text{ mm}} ; \quad l_{bd} = \overbrace{\alpha_1 \alpha_2 \alpha_3 \alpha_4 \alpha_5}^{=1} \cdot l_{b, reqd} \\ = \underline{725 \text{ mm}}$$

$$l_{b, min} = \max(0,3 l_{b, reqd} ; 10\phi ; 100 \text{ mm}) \\ = \max(0,3 \times 725 ; 10 \times 20 ; 100 \text{ mm}) = \underline{217,5 \text{ mm}}$$



For  $\phi 18$  mm

$$l_{b, reqd} = \frac{\phi}{4} \cdot \frac{\sigma_{sd}}{f_{bd}} = \frac{18}{4} \cdot \frac{435}{3} = \underline{\underline{652,5 \text{ mm}}}$$

$$l_{bd} = 625,5 \text{ mm}$$

$$l_{b, min} = \max(0,3 \cdot l_{b, reqd}; 10\phi; 100 \text{ mm}) = \underline{\underline{187,65 \text{ mm}}}$$

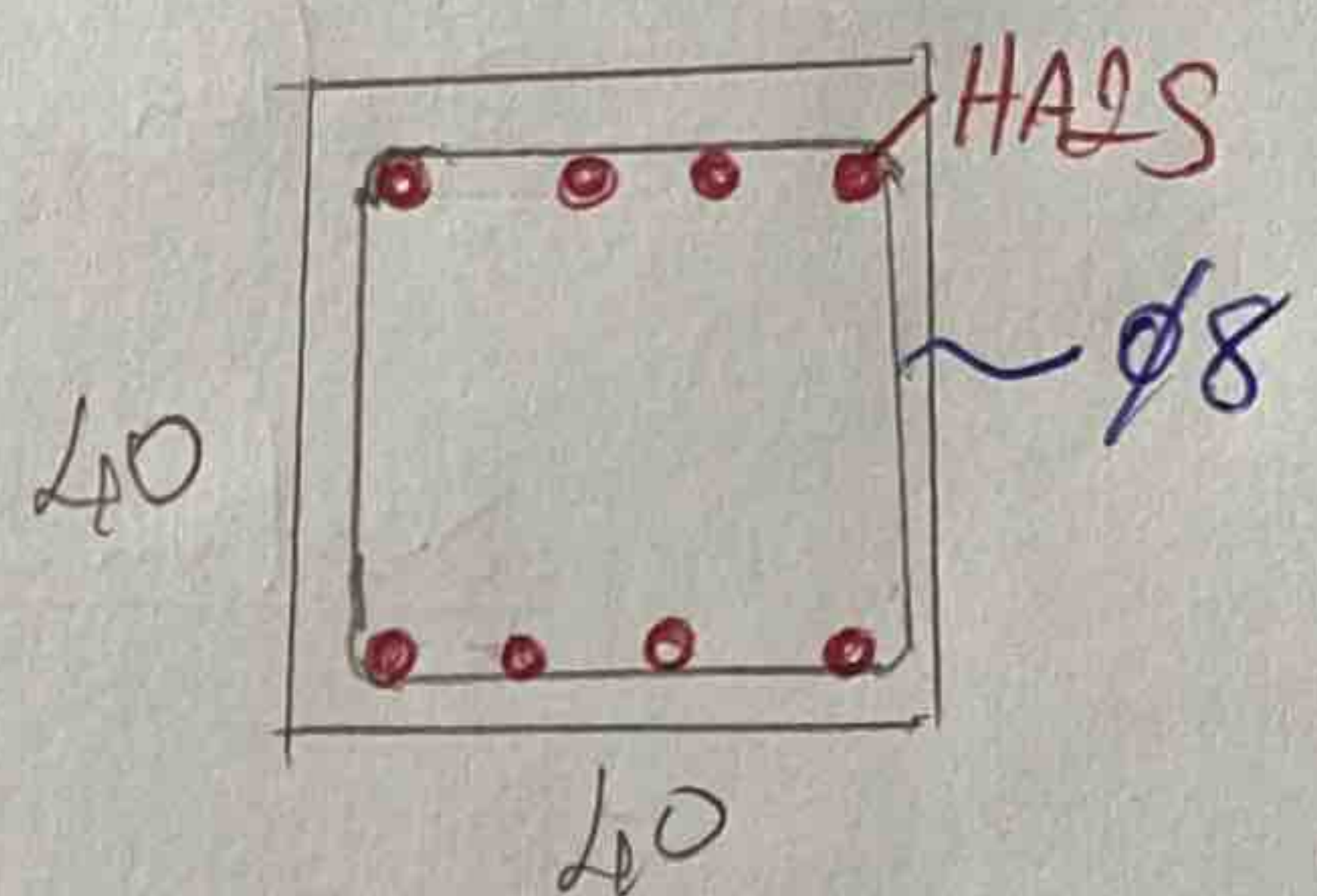
For  $\phi 16$  mm

$$l_{b, reqd} = \frac{16}{4} \cdot \frac{435}{3} = 580 \text{ mm}; \quad \underline{\underline{l_{bd} = 580 \text{ mm}}}$$

$$l_{b, min} = \max(174; 460; 100) = \underline{\underline{176 \text{ mm}}}$$

Design of column ties

Diameter estimation



$$\phi_{tie} \geq \max\left(\frac{\phi_s}{4}; 6 \text{ mm}\right)$$

$$\phi_{tie} \geq \max\left(\frac{25}{4}; 6 \text{ mm}\right) = \max(6,25; 6 \text{ mm}) = \underline{\underline{7 \text{ mm}}}$$

So, we can use  $\phi 8$  mm for stirrups

Basic spacing

$$s_1 \leq \min(20\phi_s; \min(l_{col}; h_{col}); 600 \text{ mm})$$

$$s_1 \leq \min(20 \cdot 25; 400; 600 \text{ mm}) = \underline{\underline{400 \text{ mm}}}$$

$$s_2 \leq 0,6 s_1$$

$$s_2 \leq 0,6 \times 400 = \underline{\underline{240 \text{ mm}}}$$



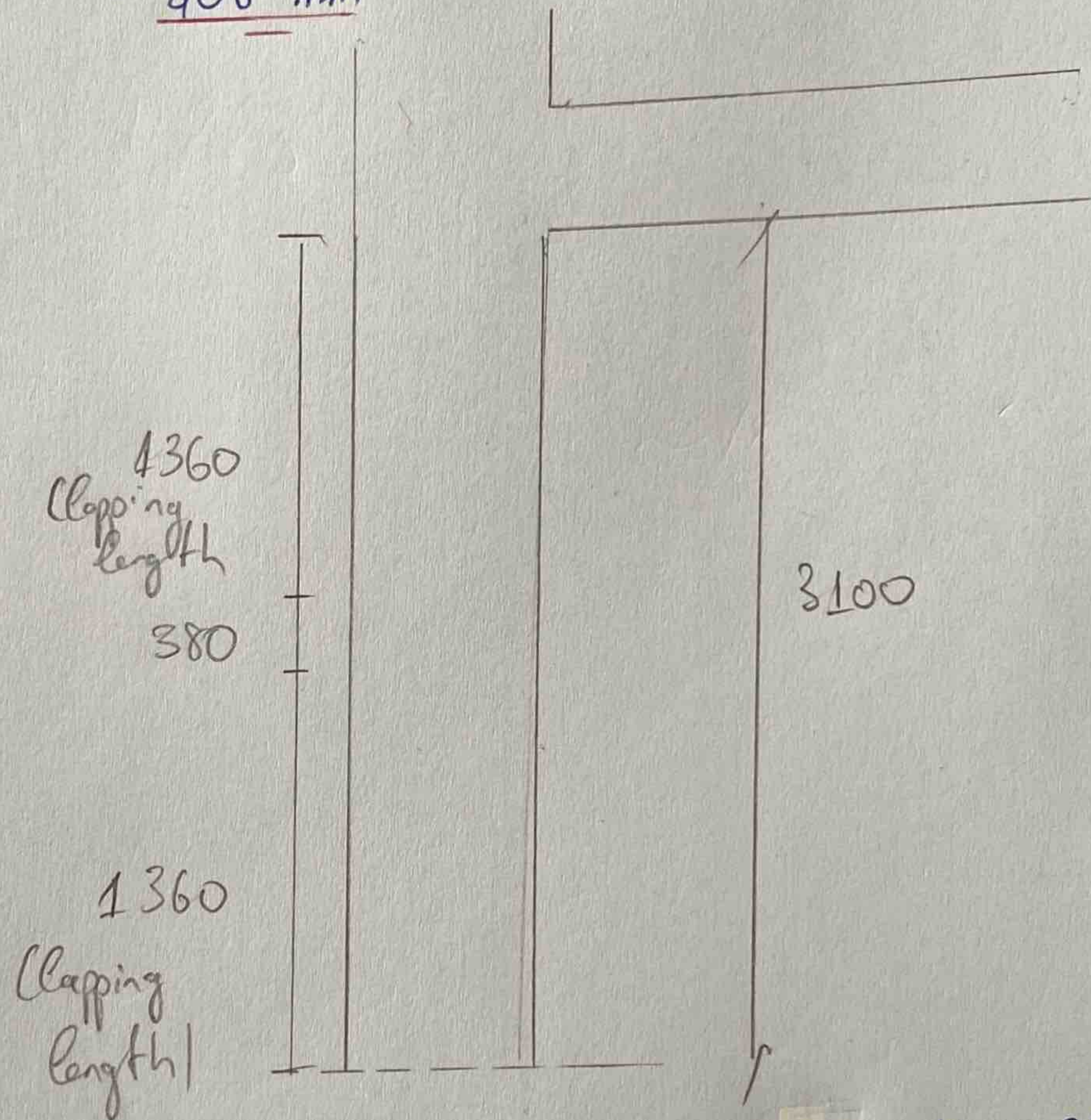
## Lapping length

$$l_{o,d} = \sqrt[4]{l_1 \cdot l_2 \cdot l_3 \cdot l_4 \cdot l_5 \cdot l_6} \cdot l_{b,reqd}$$
$$= 1,5 \cdot 906,25$$
$$\approx \underline{1360 \text{ mm}}$$

$$l_{b,reqd} = \frac{\sigma}{4} \cdot \frac{\sigma_{sd}}{f_b \phi}$$
$$= \frac{25}{4} \cdot \frac{435}{3}$$
$$= 906,25 \text{ mm}$$

## Minimum lapping

$$l_{o,min} = \max(0,3 \cdot l_{b,reqd}; 1,5 \phi; 200 \text{ mm})$$
$$= \max(0,3 \cdot 1,5 \cdot 906,25; 1,5 \cdot 25; 200 \text{ mm})$$
$$\approx \underline{408 \text{ mm}}$$



The basic spacing  $s_1$  (400) is more than 380 mm. Consequently, we don't have any other choice than using only one spacing  $s_2$  (240 mm) for the column.