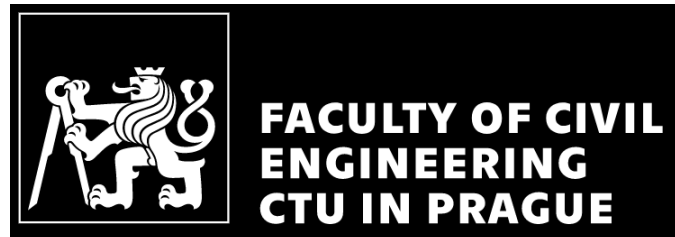


# Structural Steel Virtual Excursion

Design, manufacturing, erecting and full physical test of a simple portal frame of structure

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# Structural Steel Virtual Excursion

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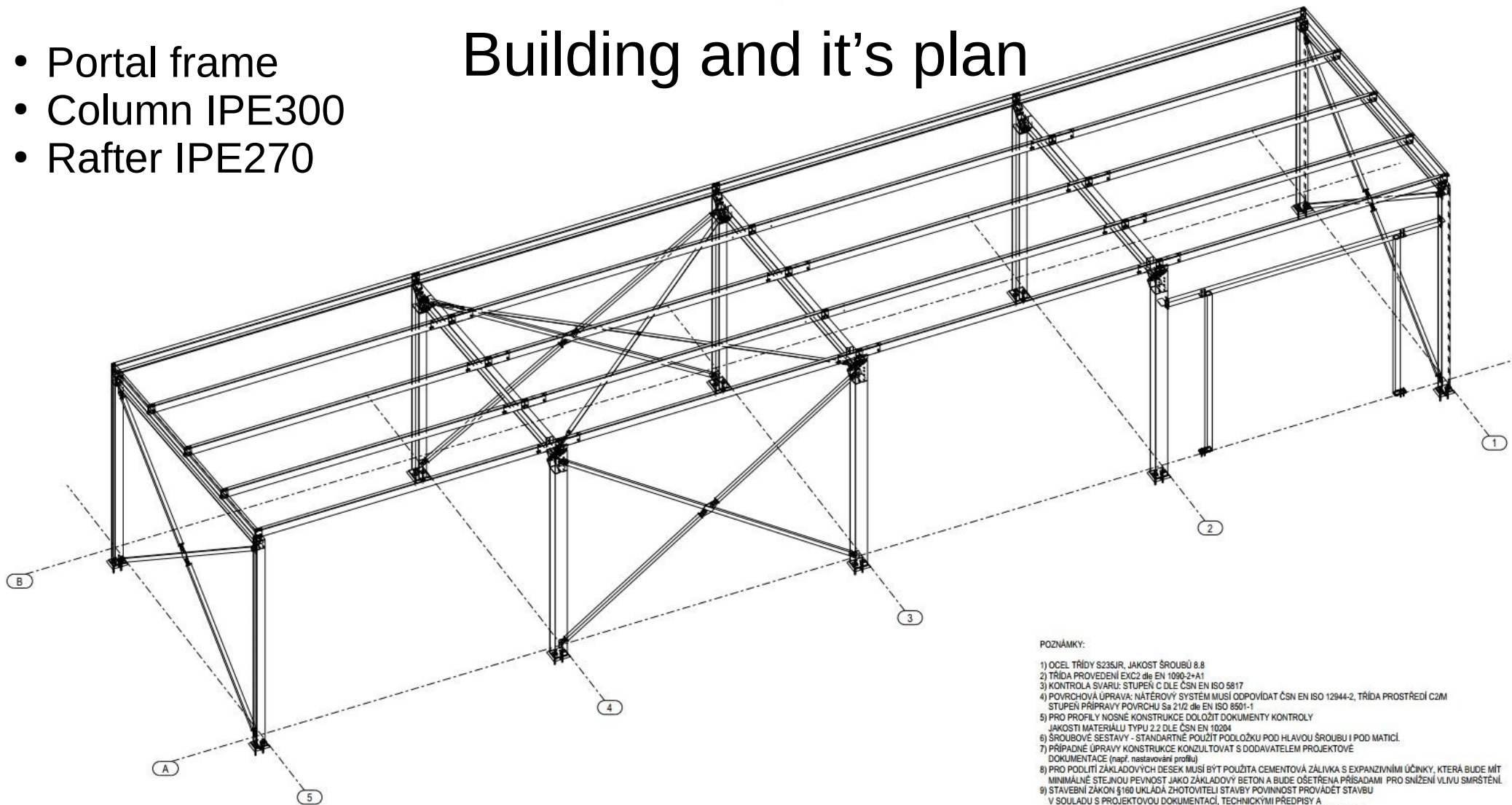


# Structural Steel Virtual Excursion

- **Objectives:**
- Build portal frame type of building (5.6 m structural span, 4.3 m structural height and 23.5 m building length),
- Perform full scale physical test on building with and without roof cladding (to test the effect of cladding on overall stiffness of the building),
- Do not damage building during the test! We will be checking just response to the side horizontal load at serviceability limit state,
- Some damage may occur to cladding connections. Check this damage.
- Investigate the contribution of roof cladding to the stiffness of the building,
- Shot video from manufacturing and building assembly,
- Record full scale test.

- Portal frame
- Column IPE300
- Rafter IPE270

# Building and it's plan

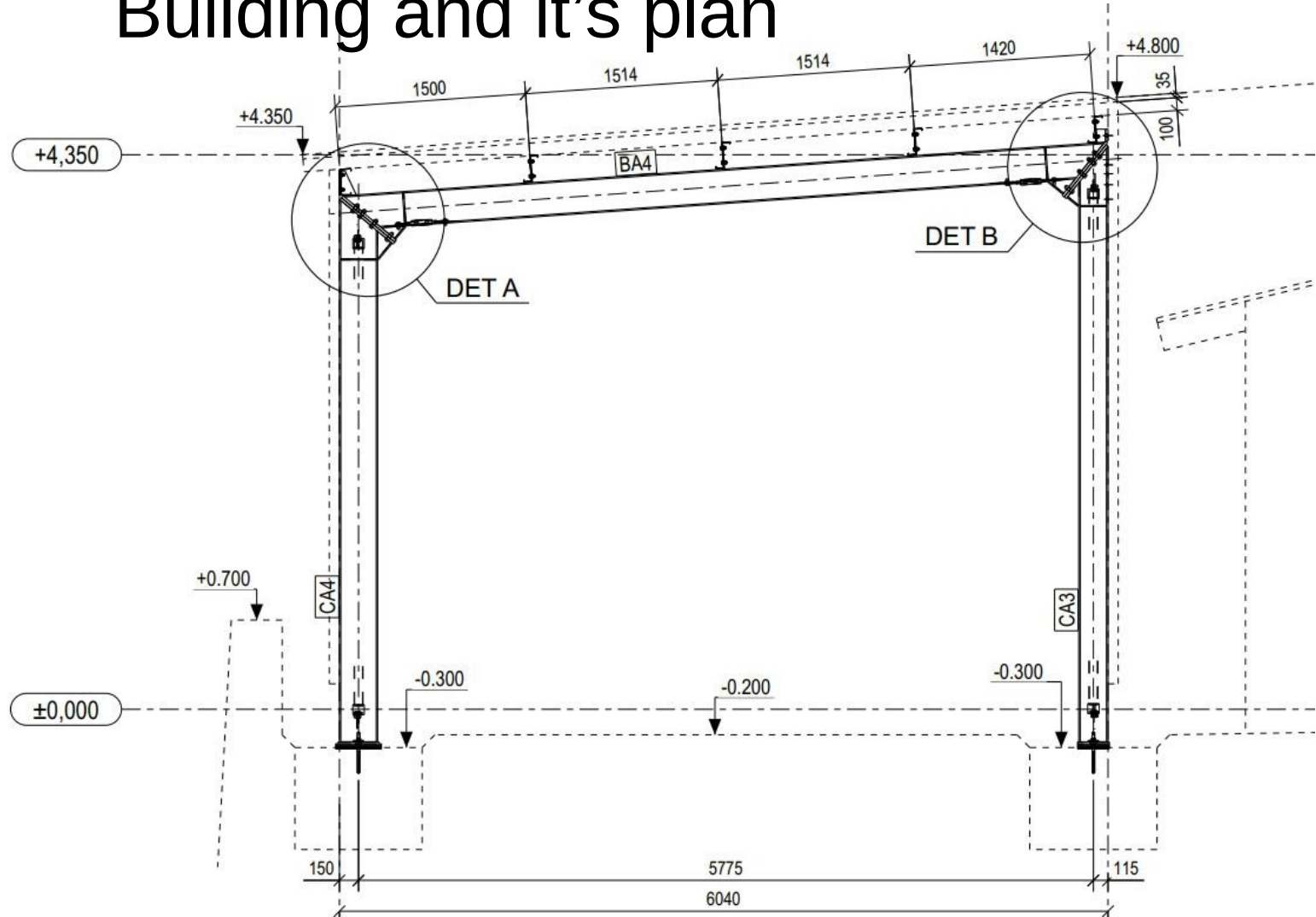


#### POZNÁMKY:

- 1) OCEL TŘÍDY S235JR, JAKOST ŠROUBŮ 8.8
- 2) TŘÍDA PROVEDENÍ EXC2 dle EN 1090-2+A1
- 3) KONTROLA SVARU: STUPĚN C DLE ČSN EN ISO 5817
- 4) POVRCHOVÁ ÚPRAVA: NÁTEROVÝ SYSTÉM MUSÍ ODPOVÍDAT ČSN EN ISO 12944-2, TŘÍDA PROSTŘEDÍ C2M STUPĚN PŘÍPRAVY POVRCHU Sa 2 1/2 dle EN ISO 8501-1
- 5) PRO PROFILY NOSNÉ KONSTRUKCE DOLŽIT DOKUMENTY KONTROLY JAKOSTI MATERIÁLU TYPU 2.2 DLE ČSN EN 10204
- 6) ŠROUBOVÉ SESTAVY - STANDARDNĚ POUŽÍT PODLOŽKU POD HLAVOU ŠROUBU I POD MATICI.
- 7) PŘÍPADNÉ ÚPRAVY KONSTRUKCE KONZULTOVAT S DODAVATELEM PROJEKTOVÉ DOKUMENTACE (např. nastavení profilu)
- 8) PRO PODLŽÍ ZÁKLADOVÝCH DESEK MUSÍ BÝT POUŽITA CEMENTOVÁ ZÁLIVKA S EXPANZIVNÍMI ÚČINKY, KTERÁ BUDE MÍT MINIMÁLNĚ STEJNOU PEVNOST JAKO ZÁKLADOVÝ BETON A BUDE OŠETŘENA PŘÍSDAVAMI PRO SNÍŽENÍ VLIVU SMRŠTĚNÍ.
- 9) STAVEBNÍ ZÁKON §160 UKLÁDÁ ZHOTOVITELI STAVBY POVINNOST PROVÁDĚT STAVBU V SOULADU S PROJEKTOVOU DOKUMENTACÍ, TECHNICKÝMI PŘEDPISY A TECHNICKÝMI NÓRMAMI. JAKEKOLIV ZMĚNY PROVEDENÉ OPROTÍ TETO VÝKRESOVĚ

# Building and it's plan

- Portal frame
- Column IPE300
- Rafter IPE270



# Manufacturing and assembly

- CNC cutting
- Manual welding
- Surface treatment
- Primer and final paint
- Assembly took 2 days
- Details in video



# Experiment

- Video
  - [https://odysee.com/@jxm:7/2021\\_experiment\\_hala\\_v01:4](https://odysee.com/@jxm:7/2021_experiment_hala_v01:4)

- Simple frame
- Hot rolled I-profiles (IPE 300 for column, IPE270 for rafter)
- Roof clad with composite panels (PUR)
- Test performed on UNCLAD building
- Another test on CLAD building (bare frame)
- Unit used by lab team when collecting experimental data, force and displacements shown on the photograph

# Experiment





# Experiment

- Forklift
  - Max. force about 50 kN (5 tons)
  - 30 kN was required and achieved during the test



# Experiment

- Detail of Z purlins, cladding by composite panels and column-rafter connection



# Experiment

- Detail of displacement sensors used during the experiment



# Experiment

- Column base, bracing plate and bracing connection



# Experiment

- Crossing of bracing diagonals



# Experiment

- Roof cross bracing



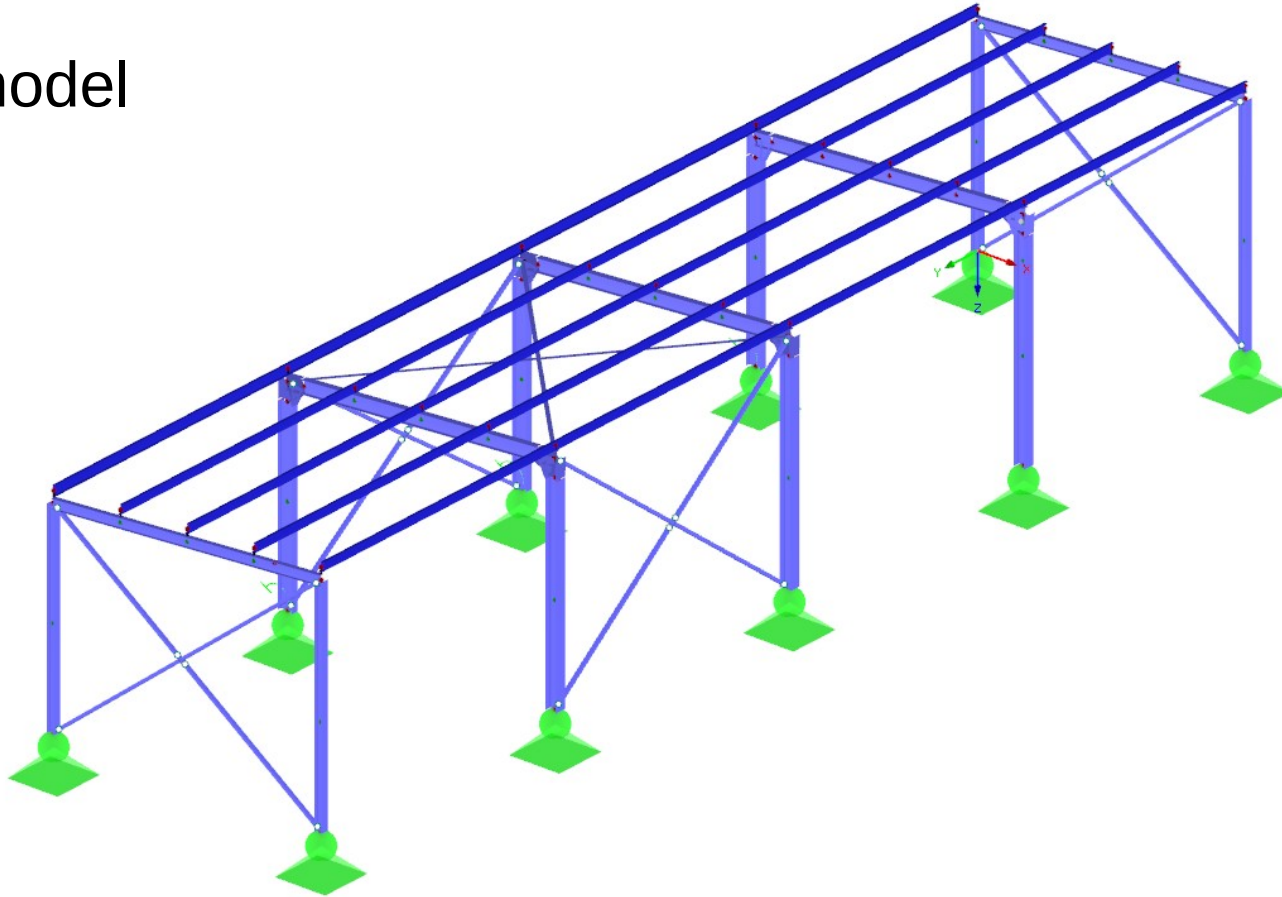
# Experiment

- Detail of cladding as well as fin plate used to connect dynamic rope to exert force by forklift



# Behaviour

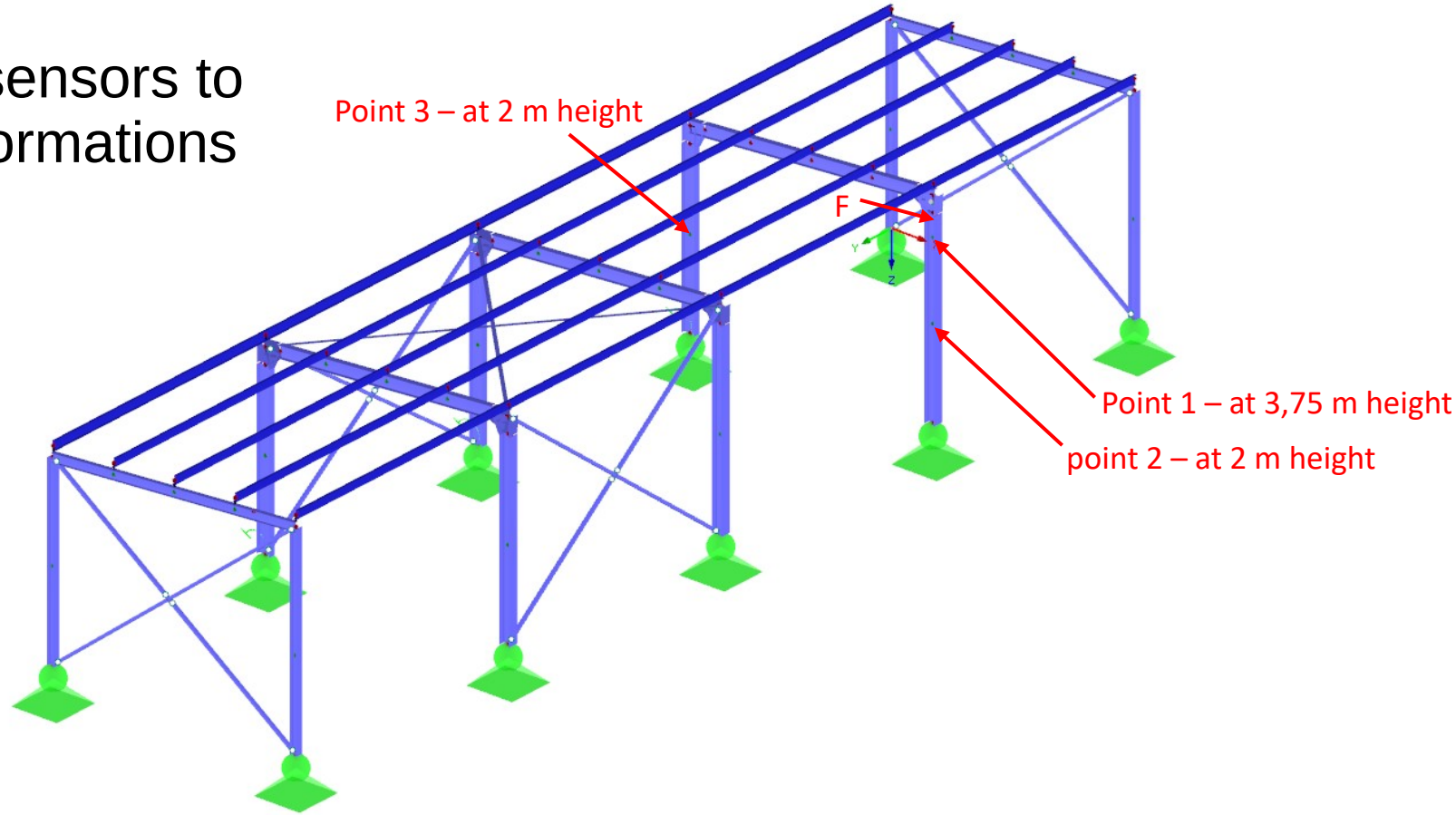
- Analysis model





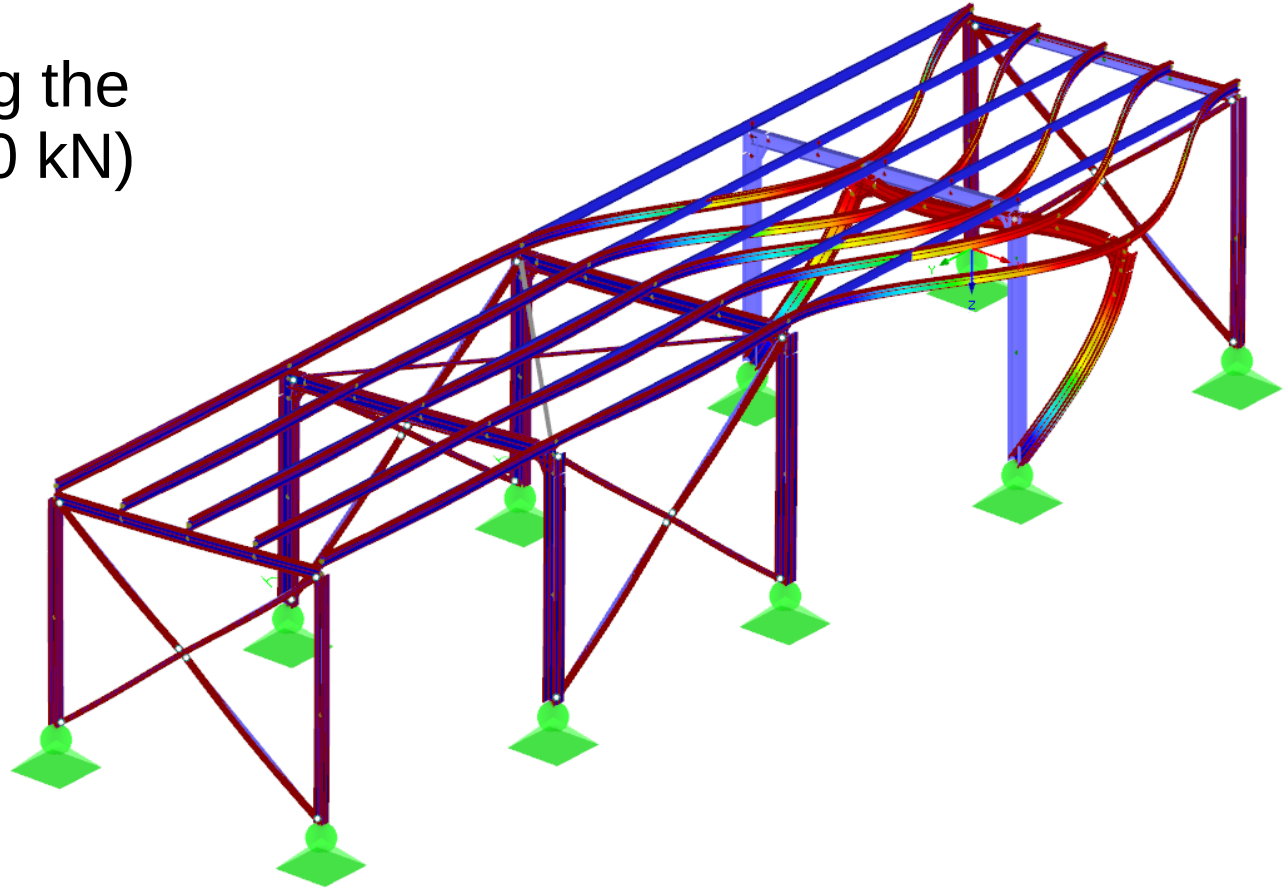
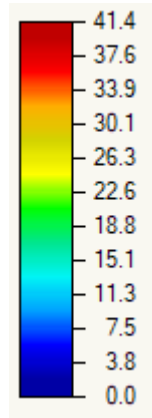
# Behaviour

- Positions of sensors to measure deformations



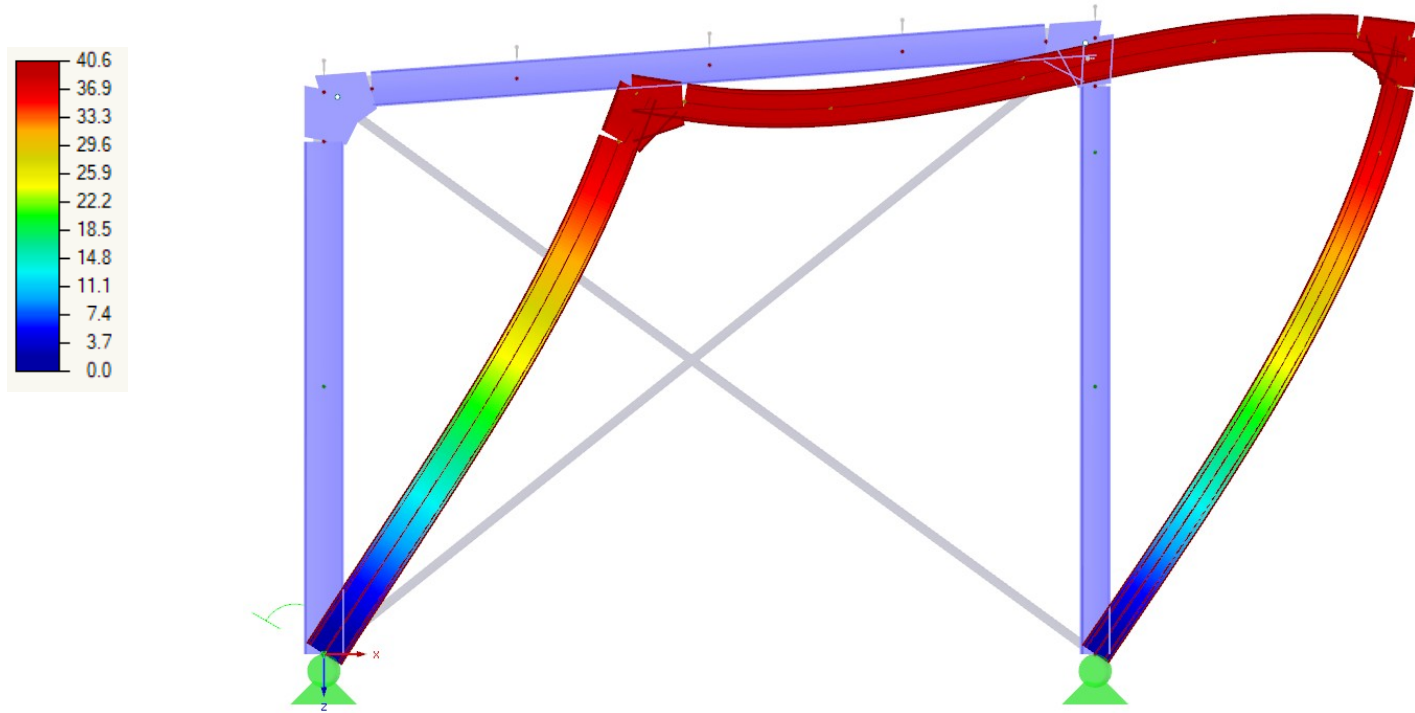
# Behaviour

- Deformation during the experiment ( $F = 30$  kN)



# Behaviour

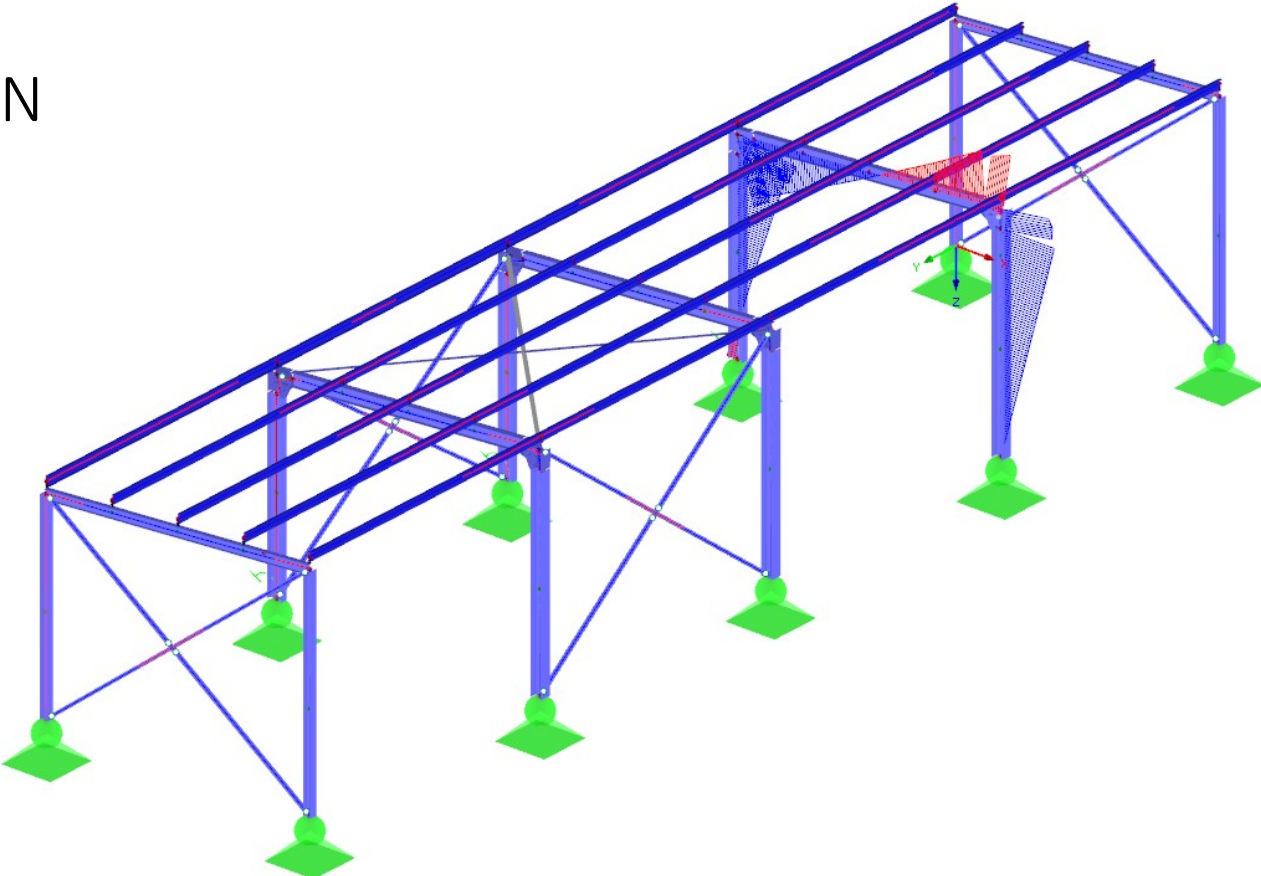
Horizontal deformation of bare frame for  $F = 30$  kN





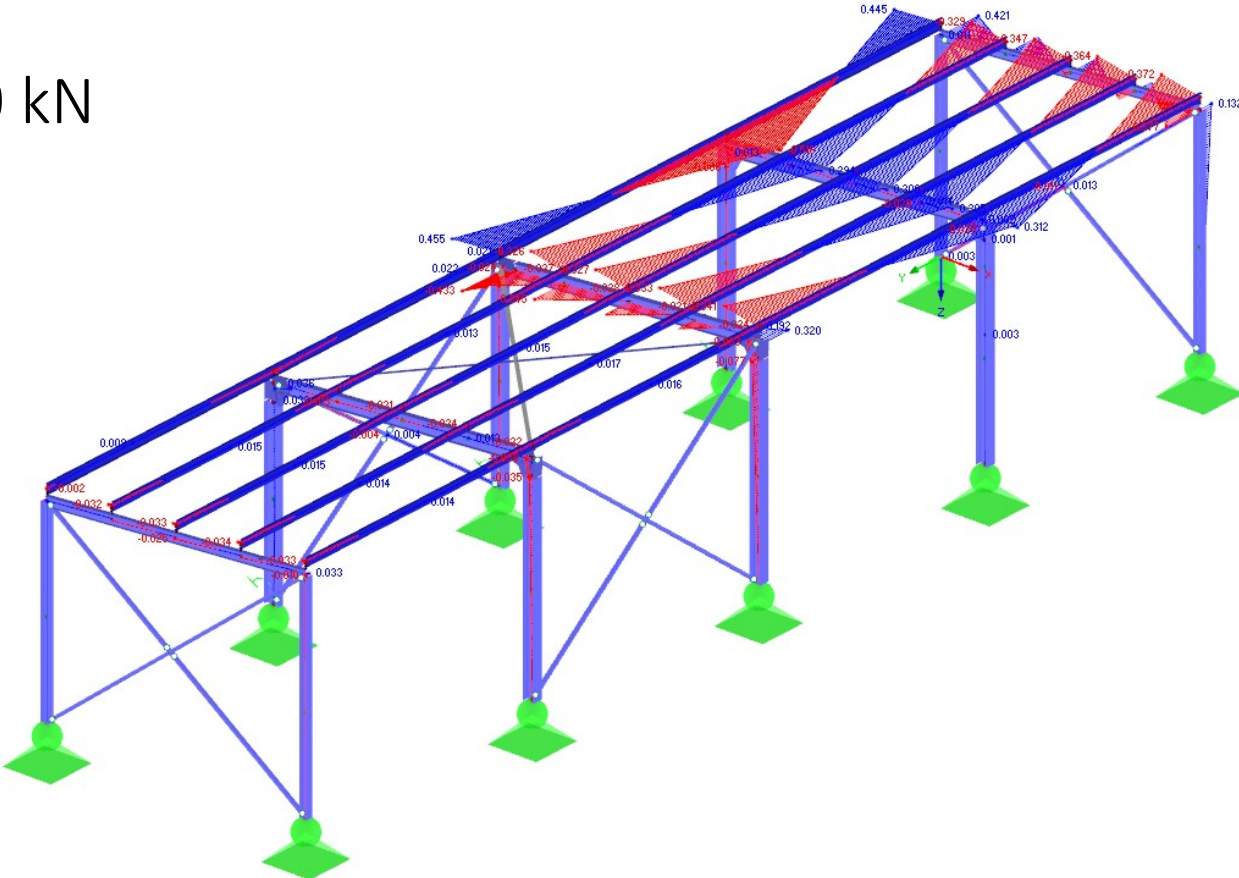
# Behaviour

$M_y$  for  $F = 30 \text{ kN}$



# Behaviour

$M_z$  for  $F = 30 \text{ kN}$



# Behaviour - observations

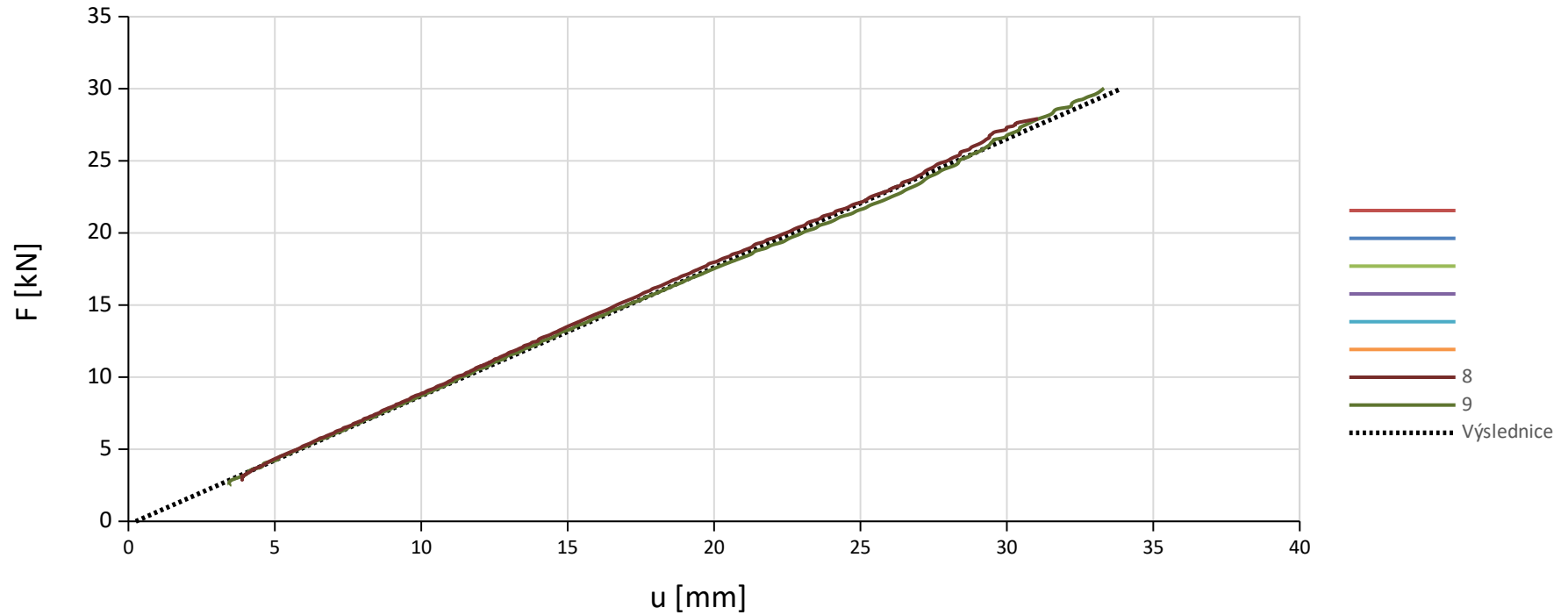
Distortion of Zed roof purlin during the test

Damage and ovalization of holes in composite roof panel



# Behaviour

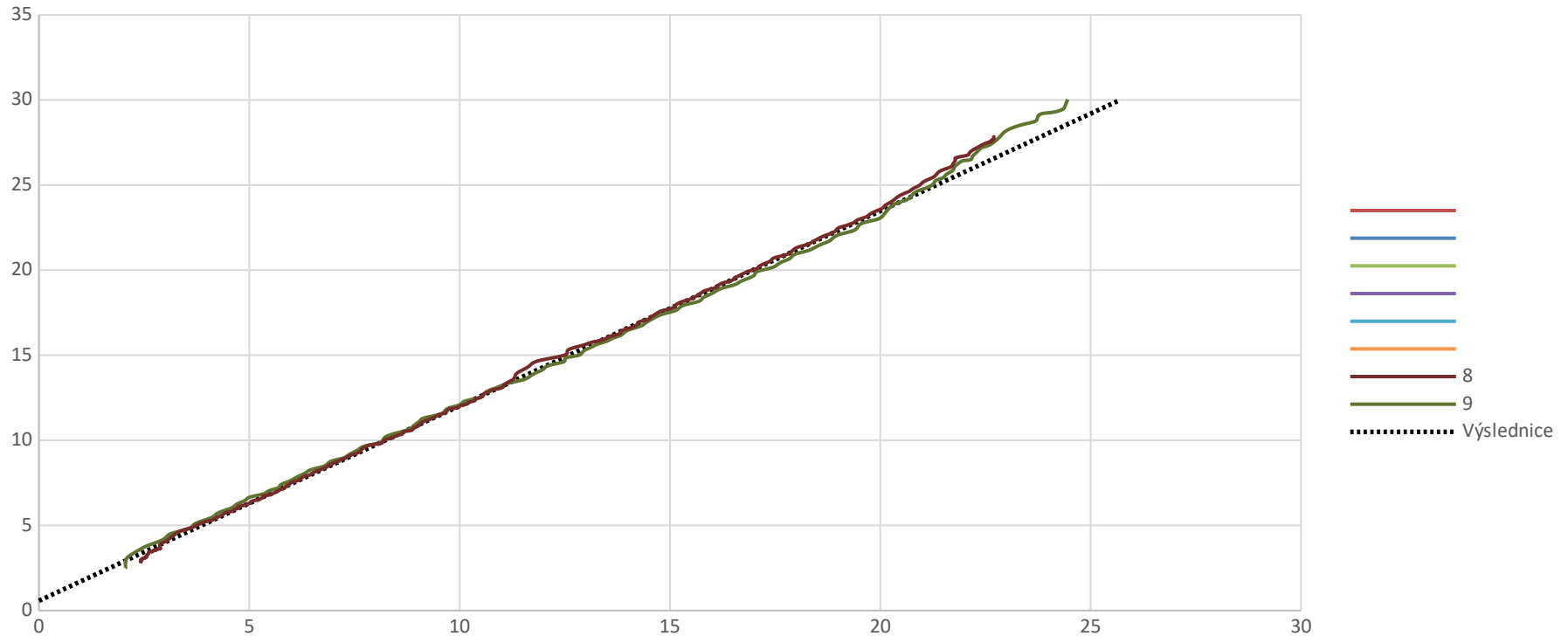
Point #1, F-u diagram, bare steel frame





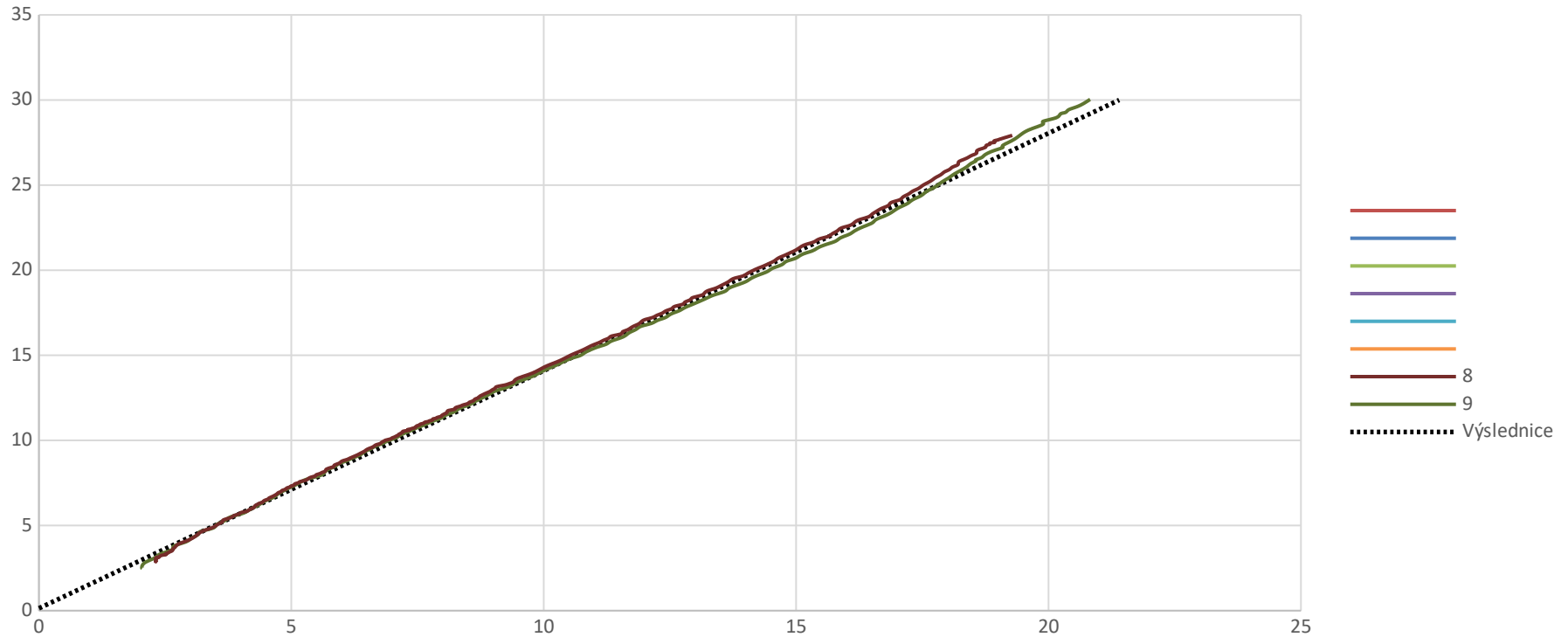
# Behaviour

Point #2, F-u diagram, bare steel frame



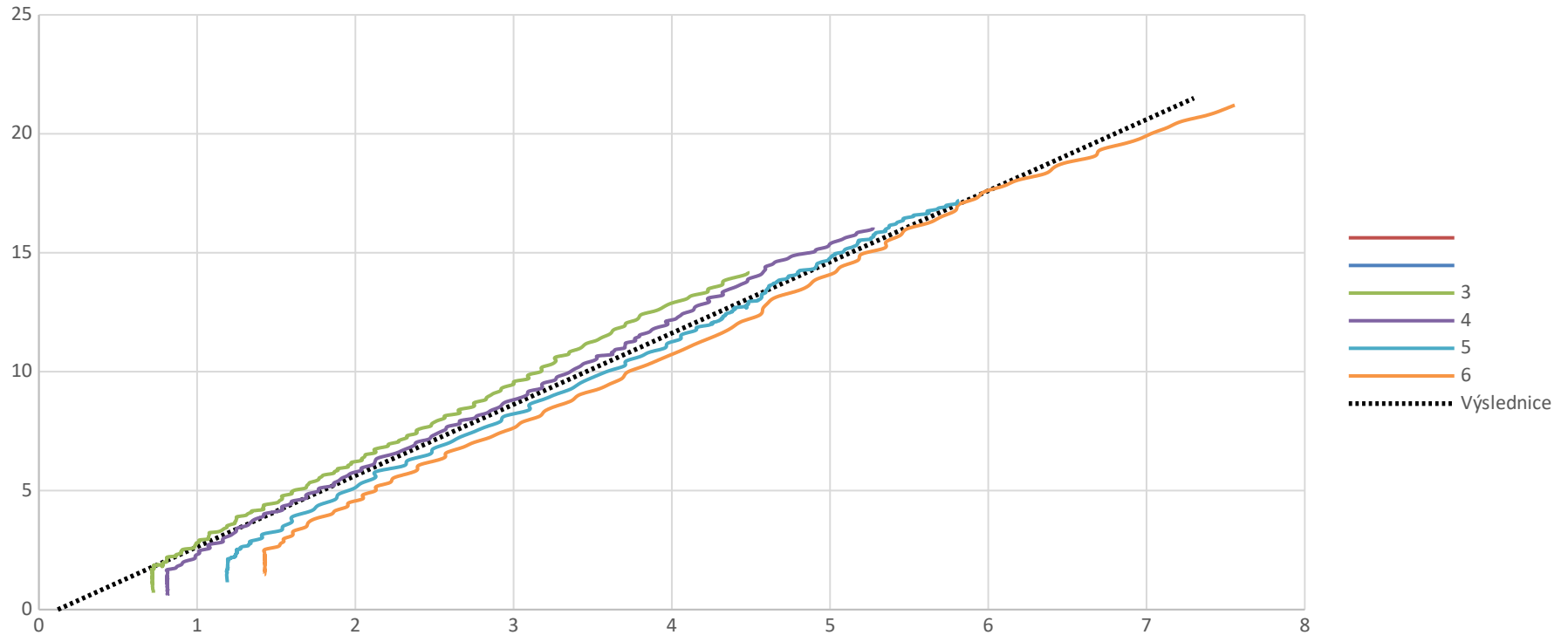
# Behaviour

Point #3, F-u diagram, bare steel frame



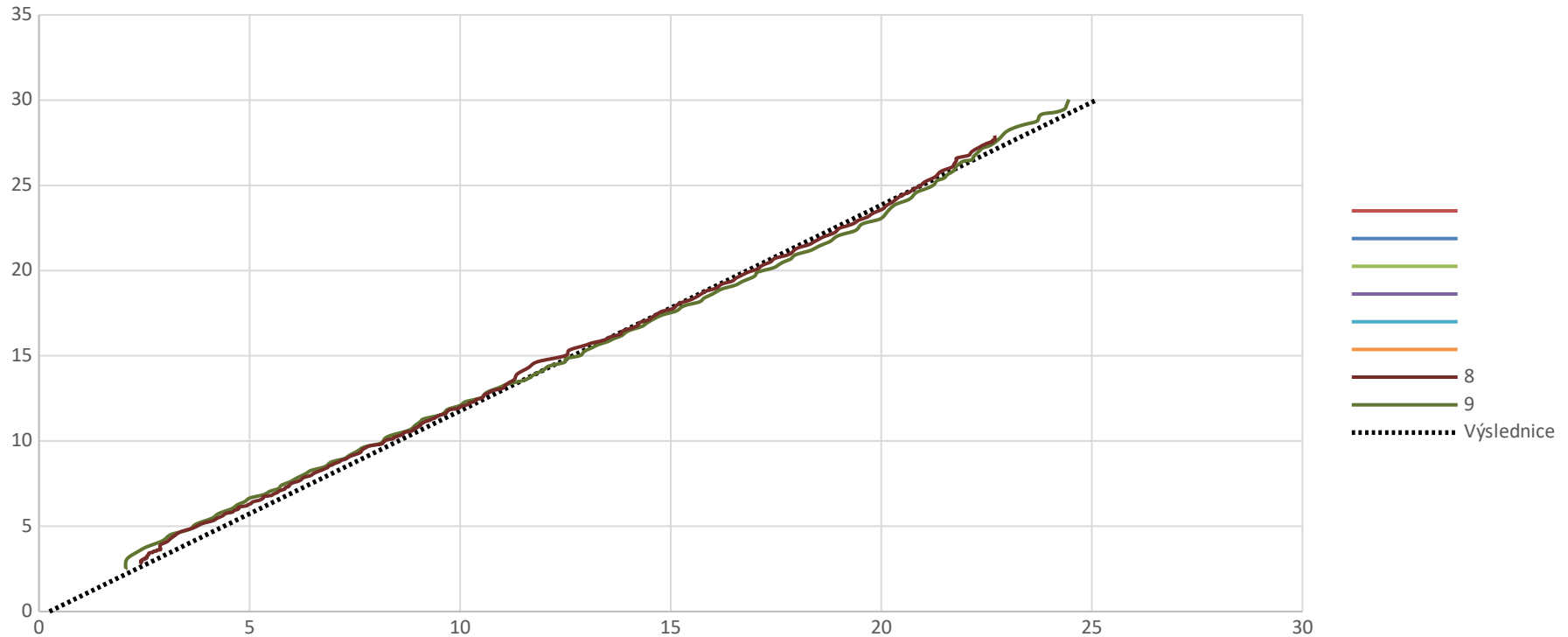
# Behaviour

Point #1, F-u diagram, Frame with roof cladding



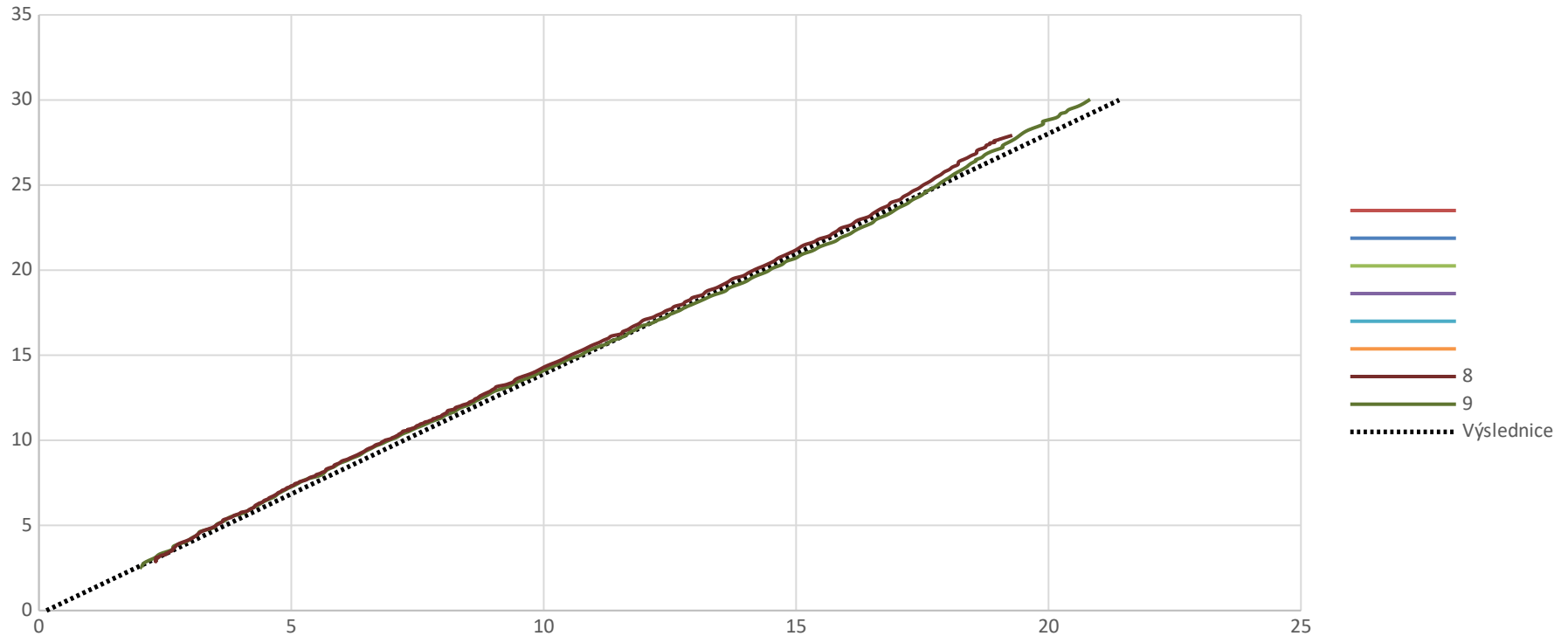
# Behaviour

Point #2, F-u diagram, Frame with roof cladding



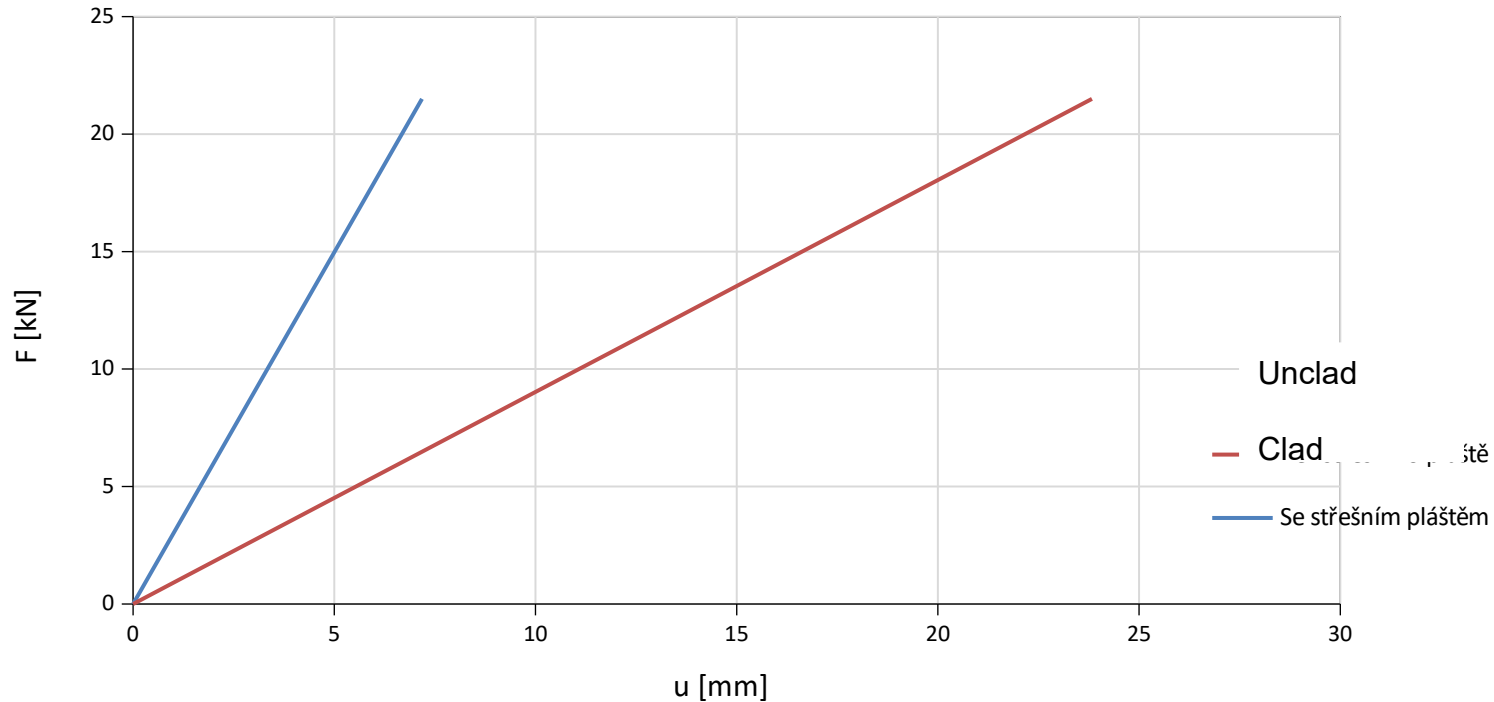
# Behaviour

Point #3, F-u diagram, Frame with roof cladding



# Behaviour

Comparison of horizontal deformations of clad and unclad building for Point 1

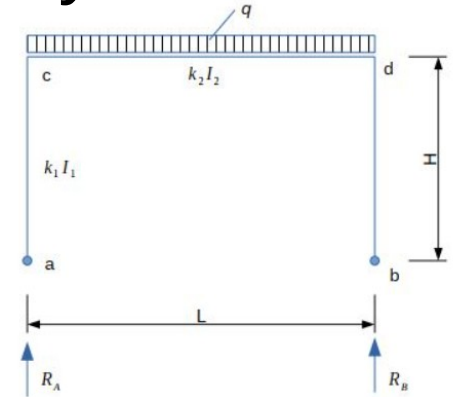


# Example of a simplified analysis

- **Objectives:**
- Analysis of internal forces and displacements based on frame equations (no need for software)
- Investigate sensitivity of frame to sway imperfections
  - Calculate horizontal deformations and internal forces
  - Check  $\alpha_{cr}$
  - Check limiting vertical loading at which sway imperfections need to be considered
- Ultimate Limit State of column, check:
  - Lateral torsional buckling of column
  - Interaction of axial force and bending moment

# Example of a simplified analysis

- Python based code developed in Jupyter notebook
- Procedure:
  - Internal forces and deformations based on equations (sketches)
  - Level of loading is hardcoded (can be adjusted as appropriate)
  - Check frame imperfections
  - Check  $\alpha_{cr}$  and it's limits
  - Check if sway imperfections need to be considered
  - Check interaction of axial compression (flexural buckling, flexural torsional buckling) and lateral torsional buckling (Table NB.3.1 of CSN EN 1993-1-1)



$$k_1 = \frac{I_1}{H}$$
$$k_2 = \frac{I_2}{L}$$
$$M_s = \frac{qL^2}{8}$$
$$M_{ca} = -M_{cb} = \frac{qL^2}{4} * \frac{k_1}{3k_1 + 2k_2}$$
$$M_{max} = \frac{qL^2}{8} - M_{ca}$$
$$R_A = R_B = \frac{qL}{2}$$

In [145]:

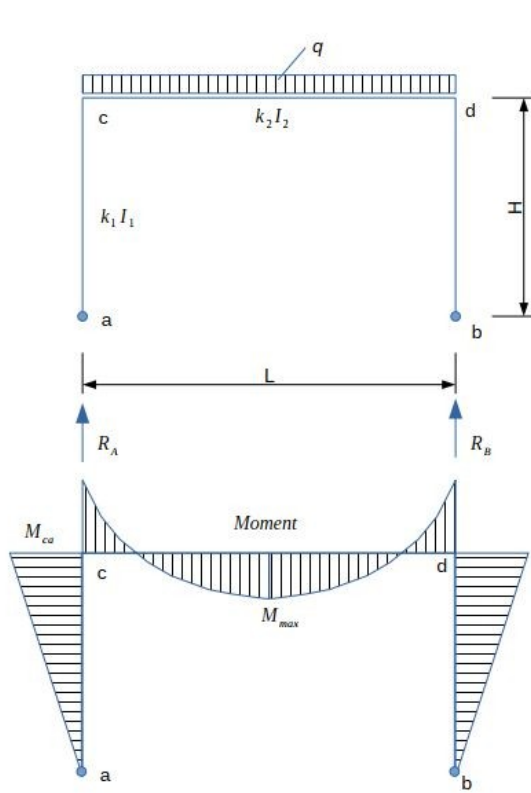
```
1 # Loading
2 # Total factored UDL on rafter
3 qd = 20 #[kN/m]
4 Fd = 20 #[kN]
```



# Example of a simplified analysis

- Code could be found at:  
<https://github.com/maresjiri/Simple-portal-frame>

- Frame equations



$$k_1 = \frac{I_1}{H}$$

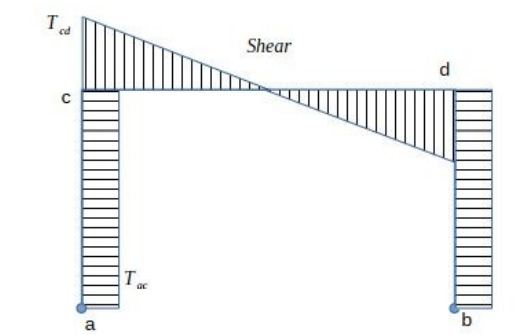
$$k_2 = \frac{I_2}{L}$$

$$M_s = \frac{qL^2}{8}$$

$$M_{ca} = -M_{cd} = \frac{qL^2}{4} * \frac{k_1}{3k_1 + 2k_2}$$

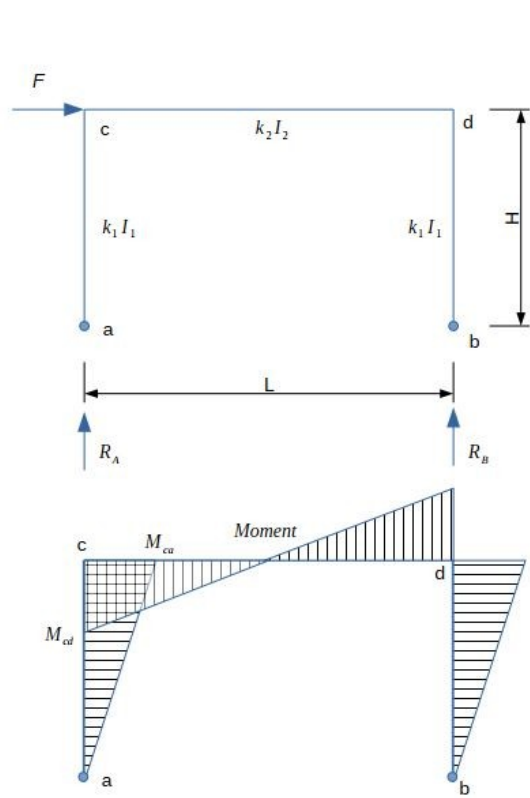
$$M_{max} = \frac{qL^2}{8} - M_{cd}$$

$$R_A = R_B = \frac{ql}{2}$$



$$T_{ac} = \frac{-M_{ca}}{H}$$

$$T_{cd} = R_A = \frac{ql}{2}$$

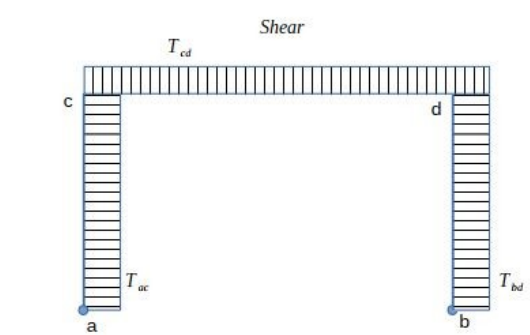


$$k_1 = \frac{I_1}{H}$$

$$k_2 = \frac{I_2}{L}$$

$$\phi_c = \frac{FH}{6k_2}$$

$$\psi = \frac{FH}{6} * \frac{k_1 + 2k_2}{k_1 k_2}$$



$$\Delta = \frac{\psi H}{2E}$$

$$M_{ca} = -M_{cd} = \frac{-FH}{2}$$

$$T_{ac} = \frac{-M_{ca}}{H} = \frac{F}{2}$$

$$T_{cd} = \frac{-FH}{L} = \frac{2M_{cd}}{L}$$

$$T_{bd} = T_{ac} = \frac{-M_{ca}}{H} = \frac{F}{2}$$

$$R_A = T_{cd}$$

$$R_B = -R_A$$

# Example of a simplified analysis

- Profiles and material

```
1 # Profiles
2 # Column
3 # IPE 300
4 Ac = 5381 #[mm^2], cross-sectional area
5 Iyc = 83560000 #[mm^4]
6 Wyc = 557000 #[mm^3]
7 Izc = 6038000 #[mm^4]
8 Itc = 201200
9 Iwc = 125900000000
10 zg = 0 #[m]
11 zj = 0 #[m]
12
13
14 # Rafter
15 # IPE 270
16 Ar = 4594 #[mm], cross-sectional area
17 Iyr = 57900000 #[mm^4]
18 Wyr = 429000 #[mm^3]
19 Izr = 4199000 #[mm^4]
20
21
22 # Material
23 E = 210000000 #[kPa]
24 G = 80700000 #[kPa]
25 fy = 275000
26 gammaM1 = 1
```

# Example of a simplified analysis

- Loading and frame imperfections

```
1 # Loading
2 # Total factored UDL on rafter
3 qd = 20 #[kN/m]
4 Fd = 20 #[kN]
```

```
1 # Frame imperfections
2 alpha_h = 2 / math.sqrt(H)
3 m = 2
4 alpha_m = math.sqrt(0.5 * (1 + 1/m))
5 phi0 = 1 / 200
6 phi = phi0 * alpha_h * alpha_m
7
8 # Equivalent horizontal force
9 EHF = qd * L * phi
10 k1 = Iyc * 10**(-12) / H
11 k2 = Iyr * 10**(-12) / L
12 psi_EHF = (EHF * H / 6) * ((k1 + 2*k2) / k1 / k2)
13 DELTA_EHF = psi_EHF * H / 2 / E
```

# Example of a simplified analysis

- $\alpha_{cr}$  and amplification factor
- Here,  $\alpha_{cr} \gg 10$  therefore linear analysis ignoring sway imperfections is acceptable
- When loading on rafter is increased  $\alpha_{cr}$  gets reduced and imperfections need to be accounted for in analysis
- Re-running the code with increased qd shows sensitivity of the frame to the imperfections

```
1 Hd = Fd + EHF
2 Vd = qd * L
3 alpha_cr = (Hd / Vd) * (H / DELTA)
```

```
alpha_cr = 26.21 [-]
```

```
1 # Amplification factor
2 amp = 1 / (1 - 1 / alpha_cr)
```

```
1 errmsg = "Method is adequate."
2 if alpha_cr < 3:
3     errmsg = "ERROR: alpha_cr out of limits."
4 if alpha_cr > 10:
5     errmsg = "Linear elastic analysis is adequate."
6     amp = 1
7
8 print(errmsg)
```

```
Linear elastic analysis is adequate.
```

```
amp = 1.000 [-]
```

# Example of a simplified analysis

- Buckling curves and critical buckling moment  $M_{cr}$

```
1 PHI_y = 0.5*(1 + alpha_y *(lambda_dash_y - 0.2) + lambda_dash_y**2)
2 PHI_z = 0.5*(1 + alpha_z *(lambda_dash_z - 0.2) + lambda_dash_z**2)
3 chi_y = min(1 / (PHI_y + math.sqrt(PHI_y**2 - lambda_dash_y**2)),1)
4 chi_z = min(1 / (PHI_z + math.sqrt(PHI_z**2 - lambda_dash_z**2)),1)
```

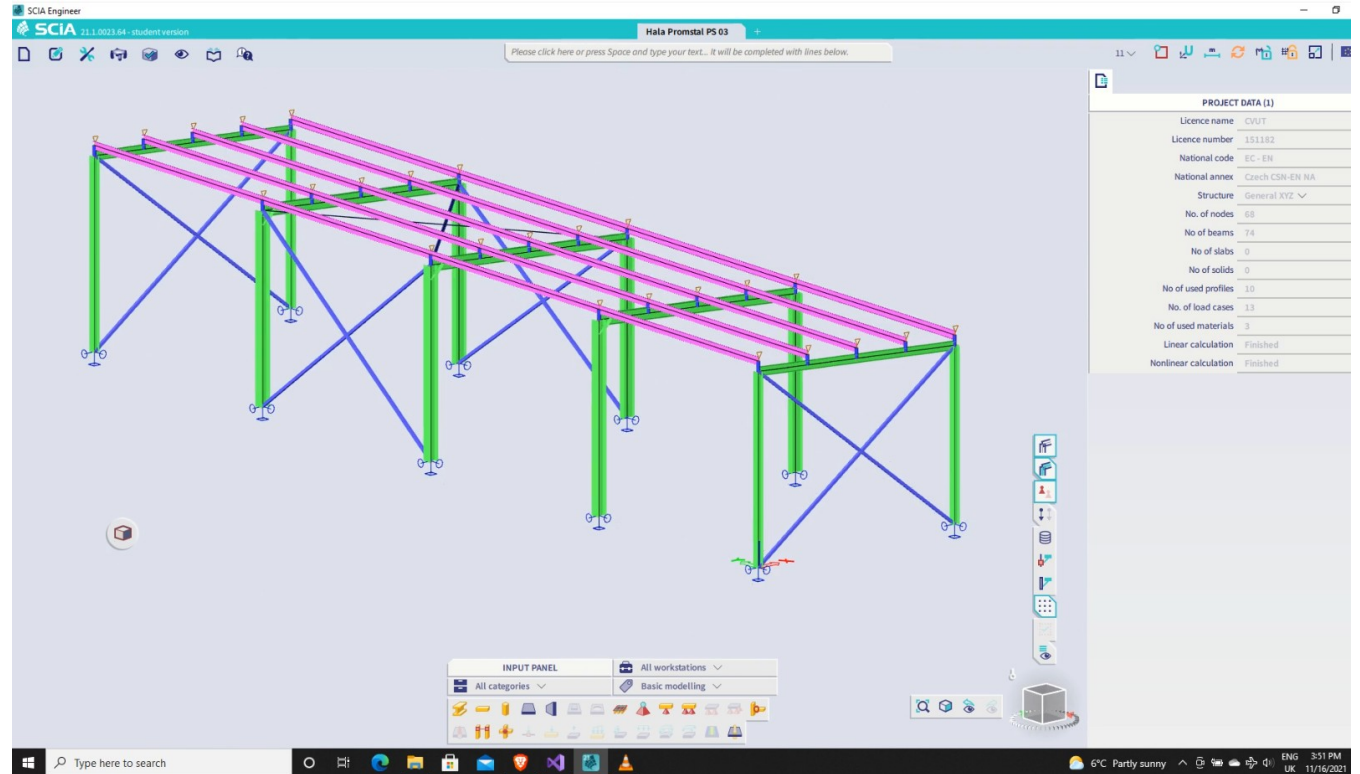
- Table NB.3.1 of CSN EN 1993-1-1 or use an alternative solution specific to your NAD
- Interaction of axial force and bending moment

```
1 UF1 = NEd * gammaM1 / chi_y / NRk + kyy * MEd * gammaM1 / chi_LT / MyRk
2 UF2 = NEd * gammaM1 / chi_z / NRk + kzy * MEd * gammaM1 / chi_LT / MyRk
```

```
UF1 = 0.641 [-]
UF2 = 0.712 [-]
```

# Analysis using commercial software

- Modelled in SCIA Engineer
- Model can be downloaded from project site



# Conclusions

- Cladding contributes to the stiffness of building but the analysis needs to assure that it does not get damaged,
- Contribution of cladding to the overall stiffness of building will depend on quality and frequency of it's connection to the framework,
- Certain permanent damage occurs in composite panel at the serviceability limit state,
- Distortional stiffness/flexibility of roof purlins also contributes to this deformation,
- Simple analysis shows as the sensitivity of imperfect frame to vertical loading, the level of loading at experiment is fairly below these limits.