

Fire Dynamics Simulator

Wolfram Jahn Lulea, 13th–15th of March 2014



Developed by Kevin McGrattan at NIST for examining fire and smoke movement in enclosed spaces such as atria, exhibition halls, warehouses, tunnels, etc



Developed by Kevin McGrattan at NIST for examining fire and smoke movement in enclosed spaces such as atria, exhibition halls, warehouses, tunnels, etc

Navier-Stokes solver

FDS consists of -



Developed by Kevin McGrattan at NIST for examining fire and smoke movement in enclosed spaces such as atria, exhibition halls, warehouses, tunnels, etc

Navier-Stokes solver

Turbulence Model

FDS consists of -



Developed by Kevin McGrattan at NIST for examining fire and smoke movement in enclosed spaces such as atria, exhibition halls, warehouses, tunnels, etc

Navier-Stokes solver

Turbulence Model

FDS consists of { - Combustion Model



Developed by Kevin McGrattan at NIST for examining fire and smoke movement in enclosed spaces such as atria, exhibition halls, warehouses, tunnels, etc

Navier-Stokes solver

Turbulence Model

FDS consists of { - Combustion Model

- Radiation Model





Developed by Kevin McGrattan at NIST for examining fire and smoke movement in enclosed spaces such as atria, exhibition halls, warehouses, tunnels, etc

- Navier-Stokes solver
- Turbulence Model
- FDS consists of { Combustion Model
 - Radiation Model
 - Boundary heat transfer



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Change of mass in Control Volume



Navier-Stokes:

Mass Conservation $\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{u} = \dot{m}_{b}^{'''}$ Incoming/Outgoing mass





Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Produced mass



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{m}_{b}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho u) + \nabla \cdot \rho u u + \nabla \rho = \rho g + f_b + \nabla \cdot \tau_{ij}$

Change of momentum in Control Volume



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho u) + \nabla \cdot \rho u u + \nabla \rho = \rho g + f_b + \nabla \cdot \tau_{ij}$

Inertia



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho u) + \nabla \cdot \rho u u + \nabla \rho = \rho g + f_b + \nabla \cdot \tau_{ij}$

> Pressure difference (external force)



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho u) + \nabla \cdot \rho u u + \nabla \rho = \rho g + f_b + \nabla \cdot \tau_{ij}$

Gravity



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{m}_{b}^{\prime\prime\prime}$$

Momentum Conservation

$$\frac{\partial}{\partial t}(\rho \boldsymbol{u}) + \nabla \cdot \rho \boldsymbol{u} \boldsymbol{u} + \nabla \rho = \rho \boldsymbol{g} + \boldsymbol{f}_b + \nabla \cdot \boldsymbol{\tau}_{ij}$$

Some external force



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{b}^{\prime\prime\prime}$$

Momentum Conservation

$$\frac{\partial}{\partial t}(\rho \boldsymbol{u}) + \nabla \cdot \rho \boldsymbol{u} \boldsymbol{u} + \nabla \rho = \rho \boldsymbol{g} + \boldsymbol{f}_b + \nabla \cdot \boldsymbol{\tau}_{ij}$$

Shear forces



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho u) + \nabla \cdot \rho u u + \nabla \rho = \rho g + f_b + \nabla \cdot \tau_{ij}$

Energy Conservation

$$\frac{\partial}{\partial t}(\rho h) + \nabla \cdot \rho h u = \frac{Dp}{Dt} + \dot{q}''' - \nabla \cdot \dot{q}$$

Change of energy in Control Volume



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho \boldsymbol{u}) + \nabla \cdot \rho \boldsymbol{u} \boldsymbol{u} + \nabla \rho = \rho \boldsymbol{g} + \boldsymbol{f}_b + \nabla \cdot \boldsymbol{\tau}_{ij}$

Energy Conservation

$$\frac{\partial}{\partial t}(\rho h) + \nabla \cdot \rho h \mathbf{u} = \frac{Dp}{Dt} + \dot{q}''' - \nabla \cdot \dot{\mathbf{q}}$$

Incoming/Outgoing energy by convection



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho \boldsymbol{u}) + \nabla \cdot \rho \boldsymbol{u} \boldsymbol{u} + \nabla \rho = \rho \boldsymbol{g} + \boldsymbol{f}_b + \nabla \cdot \boldsymbol{\tau}_{ij}$

Energy Conservation

$$\frac{\partial}{\partial t}(\rho h) + \nabla \cdot \rho h \boldsymbol{u} = \frac{D\rho}{Dt} + \dot{q}^{\prime\prime\prime} - \nabla \cdot \dot{\boldsymbol{q}}$$

Pressure changes



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho \boldsymbol{u}) + \nabla \cdot \rho \boldsymbol{u} \boldsymbol{u} + \nabla \rho = \rho \boldsymbol{g} + \boldsymbol{f}_b + \nabla \cdot \boldsymbol{\tau}_{ij}$

Energy Conservation

$$\frac{\partial}{\partial t}(\rho h) + \nabla \cdot \rho h \boldsymbol{u} = \frac{D\rho}{Dt} + \dot{\boldsymbol{q}}^{\prime\prime\prime} - \nabla \cdot \dot{\boldsymbol{q}}^{\prime\prime}$$

Energy production



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho u) + \nabla \cdot \rho u u + \nabla p = \rho g + f_b + \nabla \cdot \tau_{ij}$

Energy Conservation

$$\frac{\partial}{\partial t}(\rho h) + \nabla \cdot \rho h \mathbf{u} = \frac{Dp}{Dt} + \dot{q}''' - \nabla \cdot \dot{\mathbf{q}}''$$

Incoming/Outgoing energy by radiation



Navier-Stokes:

Mass Conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \boldsymbol{u} = \dot{\boldsymbol{m}}_{\boldsymbol{b}}^{\prime\prime\prime}$$

Momentum Conservation $\frac{\partial}{\partial t}(\rho u) + \nabla \cdot \rho u u + \nabla p = \rho g + f_b + \nabla \cdot \tau_{ij}$ Energy Conservation $\frac{\partial}{\partial t}(\rho h) + \nabla \cdot \rho h u = \frac{Dp}{Dt} + \dot{q}''' - \nabla \cdot \dot{q}''$ Gas Equation (for closure) $p = \rho \mathcal{R}_{\text{spec}} \mathcal{T}$



• FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.





- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.



- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.
- Large Eddy Simulation (or DNS if required) for turbulences:



- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.
- Large Eddy Simulation (or DNS if required) for turbulences: \rightarrow Large eddies are solved directly.



- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.
- Large Eddy Simulation (or DNS if required) for turbulences: \rightarrow Large eddies are solved directly.
 - \rightarrow Subscale eddies are approximated (Smagorinsky).



- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.
- Large Eddy Simulation (or DNS if required) for turbulences: \rightarrow Large eddies are solved directly.
 - \rightarrow Subscale eddies are approximated (Smagorinsky).
- Mixture fraction combustion model:



- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.
- Large Eddy Simulation (or DNS if required) for turbulences: \rightarrow Large eddies are solved directly.
 - \rightarrow Subscale eddies are approximated (Smagorinsky).
- Mixture fraction combustion model:
 - \rightarrow Infinite rate combustion.



- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.
- Large Eddy Simulation (or DNS if required) for turbulences: \rightarrow Large eddies are solved directly.
 - \rightarrow Subscale eddies are approximated (Smagorinsky).
- Mixture fraction combustion model:
 - \rightarrow Infinite rate combustion.
- Two approaches to model a fire:



- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.
- Large Eddy Simulation (or DNS if required) for turbulences: \rightarrow Large eddies are solved directly.
 - \rightarrow Subscale eddies are approximated (Smagorinsky).
- Mixture fraction combustion model:
 - \rightarrow Infinite rate combustion.
- Two approaches to model a fire: \rightarrow Prescribed HRR.



- FDS solves a simplified version of Navier-Stokes, appropriate for slow, buoyancy driven flows.
- Finite difference discretisation on a rectangular grid.
- Large Eddy Simulation (or DNS if required) for turbulences: \rightarrow Large eddies are solved directly.
 - \rightarrow Subscale eddies are approximated (Smagorinsky).
- Mixture fraction combustion model:
 - \rightarrow Infinite rate combustion.
- Two approaches to model a fire:
 - \rightarrow Prescribed HRR.
 - \rightarrow "Fire spread".



• Free (download it from https://code.google.com/p/fds-smv/).



- Free (download it from https://code.google.com/p/fds-smv/).
- Very easy to use (after this you'll be ready to go).



- Free (download it from https://code.google.com/p/fds-smv/).
- Very easy to use (after this you'll be ready to go).
- If used with caution, very powerful tool.



- Free (download it from https://code.google.com/p/fds-smv/).
- Very easy to use (after this you'll be ready to go).
- If used with caution, very powerful tool.
- But potentially dangerous if miss-used, or used without proper analysis of the results


About **FDS**

- Free (download it from https://code.google.com/p/fds-smv/).
- Very easy to use (after this you'll be ready to go).
- If used with caution, very powerful tool.
- But potentially dangerous if miss-used, or used without proper analysis of the results
 → e.g. Sprinkler - Fire interaction DOES NOT WORK!!



• Hundreds of parameters that can be adjusted.



- Hundreds of parameters that can be adjusted.
- Most of them require advanced knowledge of fire dynamics and numerical methods.



- Hundreds of parameters that can be adjusted.
- Most of them require advanced knowledge of fire dynamics and numerical methods.
- All of them come with a default.



- Hundreds of parameters that can be adjusted.
- Most of them require advanced knowledge of fire dynamics and numerical methods.
- All of them come with a default...so you don't have to adjust them.



- Hundreds of parameters that can be adjusted.
- Most of them require advanced knowledge of fire dynamics and numerical methods.
- All of them come with a default...so you don't have to adjust them.
- FDS offers many features that do not really work (fire spread, sprinklers).



- Hundreds of parameters that can be adjusted.
- Most of them require advanced knowledge of fire dynamics and numerical methods.
- All of them come with a default...so you don't have to adjust them.
- FDS offers many features that do not really work (fire spread, sprinklers).
- There is no general grid convergence!!



- Hundreds of parameters that can be adjusted.
- Most of them require advanced knowledge of fire dynamics and numerical methods.
- All of them come with a default...so you don't have to adjust them.
- FDS offers many features that do not really work (fire spread, sprinklers).
- There is no general grid convergence!!
- Non-physical phenomena are common, but are often not recognized.



- Hundreds of parameters that can be adjusted.
- Most of them require advanced knowledge of fire dynamics and numerical methods.
- All of them come with a default...so you don't have to adjust them.
- FDS offers many features that do not really work (fire spread, sprinklers).
- There is no general grid convergence!!
- Non-physical phenomena are common, but are often not recognized. \rightarrow Example: Burning at openings.



General Rule: GIGO!



General Rule: GIGO!

Garbage In – Garbage Out

















• Plain text file. Any text editor will do..





- Plain text file. Any text editor will do..
- Grid, geometry and boundary conditions are defined here.



- Plain text file. Any text editor will do..
- Grid, geometry and boundary conditions are defined here.
- Use an existing input file rather than creating a new one from scratch.



- Plain text file. Any text editor will do..
- Grid, geometry and boundary conditions are defined here.
- Use an existing input file rather than creating a new one from scratch.
- A valid line starts with an '&' any line without it will not be taken into account.



- Plain text file. Any text editor will do..
- Grid, geometry and boundary conditions are defined here.
- Use an existing input file rather than creating a new one from scratch.
- A valid line starts with an '&' any line without it will not be taken into account.
- A valid line has to finish with a '\'.



CHID – Naming the input file:

// Setup of FDS file
&HEAD CHID='First Example', TITLE='First Try'





The computational domain and grid:

```
// Setup of FDS file
&HEAD CHID='First Example', TITLE='First Try'
```

```
// Grid spacing
&MESH IJK=120,192,40, XB=0.0,12.0,0.0,19.0,0.0,4.0 /
```



The computational domain and grid:

```
// Setup of FDS file
&HEAD CHID='First Example', TITLE='First Try'
```

// Grid spacing &MESH IJK=120,192,40, XB=0.0,12.0,0.0,19.0,0.0,4.0 / $XB = x_i, x_f, y_i, y_f, z_i, z_f$



Simulation time:

```
// Setup of FDS file
&HEAD CHID='First Example', TITLE='First Try'
```

```
// Grid spacing
&MESH IJK=120,192,40, XB=0.0,12.0,0.0,19.0,0.0,4.0 /
```

// Simulation time
&TIME T_END=10. /



Simulation time:

```
// Setup of FDS file
&HEAD CHID='First Example', TITLE='First Try'
```

```
// Grid spacing
&MESH IJK=120,192,40, XB=0.0,12.0,0.0,19.0,0.0,4.0 /
```

// Simulation time
&TIME T_END=10. / if set to 0, only geometry is checked.



Miscellaneous:



<u>Control</u>:

// Control Parameters
&DUMP DT_RESTART=100.,NFRAMES=1800 /



<u>Control</u>:

// Control Parameters
&DUMP DT_RESTART=100.,DT_DEVC=5.,DT_SLCF=10.



<u>Obstacles</u>: Walls, furniture, doors etc. are all defined using rectangle blockages



<u>Obstacles</u>: Walls, furniture, doors etc. are all defined using rectangle blockages

// Creating obstacles
&OBST XB=6.2,6.4,1.6,6.6,0.0,2.4 /



<u>Obstacles</u>: Walls, furniture, doors etc. are all defined using rectangle blockages



<u>Obstacles</u>: Walls, furniture, doors etc. are all defined using rectangle blockages



<u>Obstacles</u>: Walls, furniture, doors etc. are all defined using rectangle blockages



RAINDANCE SCIENCE

Defining the Geometry



Boundary Conditions

• The obstruction is a boundary condition to the flow (free slip)


- The obstruction is a boundary condition to the flow (free slip)
- What about thermal boundary conditions (to calculate heat fluxes, wall temperatures)?



- The obstruction is a boundary condition to the flow (free slip)
- What about thermal boundary conditions (to calculate heat fluxes, wall temperatures)?

Surfaces and Materials

&SURF ID='Wall',MATL_ID='Paper','Concrete', THICKNESS=0.001,0.3,BACKING='EXPOSED'/



- The obstruction is a boundary condition to the flow (free slip)
- What about thermal boundary conditions (to calculate heat fluxes, wall temperatures)?

Surfaces and Materials



- The obstruction is a boundary condition to the flow (free slip)
- What about thermal boundary conditions (to calculate heat fluxes, wall temperatures)?

Surfaces and Materials

&SURF ID='Wall',MATL_ID='Paper','Concrete', THICKNESS=0.001,0.3,BACKING='EXPOSED'/ &MATL ID='Paper',CONDUCTIVITY=0.12, SPECIFIC_HEAT=1.172,DENSITY=128./ &MATL ID='Concrete',CONDUCTIVITY=1.7, SPECIFIC_HEAT=0.75,DENSITY=2400./



• SI units.



- SI units.
- Every Surface needs an ID associated to it.



- SI units.
- Every Surface needs an ID associated to it.
- Can be applied directly to an obstacle (all surfaces have same ID).



- SI units.
- Every Surface needs an ID associated to it.
- Can be applied directly to an obstacle (all surfaces have same ID).
- Or to a certain part of surface:
 - → &VENT XB=6.2,6.2,1.6,6.6,0.0,2.4,SURF_ID='WOOD'\



- SI units.
- Every Surface needs an ID associated to it.
- Can be applied directly to an obstacle (all surfaces have same ID).
- Or to a certain part of surface:
 - → &VENT XB=6.2,6.2,1.6,6.6,0.0,2.4,SURF_ID='WOOD'\
- The BCs of the Computational domain have to defined:



- SI units.
- Every Surface needs an ID associated to it.
- Can be applied directly to an obstacle (all surfaces have same ID).
- Or to a certain part of surface:
 - → &VENT XB=6.2,6.2,1.6,6.6,0.0,2.4,SURF_ID='WOOD'



• Special case of Boundary Condition





• Special case of Boundary Condition

↓ SURF ID





• Special case of Boundary Condition

SURF ID

 HRRPUA, RAMP &SURF ID='MyFire', HRRPUA=700, RAMP_Q='MyRamp'\



• Special case of Boundary Condition

SURF ID

 HRRPUA, RAMP &SURF ID='MyFire', HRRPUA=700, RAMP_Q='MyRamp'\

```
&RAMP ID='MyRamp',T=0,F=0.0/
```



• Special case of Boundary Condition

SURF ID

 HRRPUA, RAMP &SURF ID='MyFire', HRRPUA=700, RAMP_Q='MyRamp'\

&RAMP ID='MyRamp',T=0,F=0.0/
&RAMP ID='MyRamp',T=80,F=0.2/



• Special case of Boundary Condition

SURF ID

- HRRPUA, RAMP &SURF ID='MyFire', HRRPUA=700, RAMP_Q='MyRamp'\
 - &RAMP ID='MyRamp',T=0,F=0.0/
 &RAMP ID='MyRamp',T=80,F=0.2/
 &RAMP ID='MyRamp',T=120,F=0.5/





• Special case of Boundary Condition

SURF ID

- HRRPUA, RAMP &SURF ID='MyFire', HRRPUA=700, RAMP_Q='MyRamp'\
 - &RAMP ID='MyRamp',T=0,F=0.0/ &RAMP ID='MyRamp',T=80,F=0.2/ &RAMP ID='MyRamp',T=120,F=0.5/ &RAMP ID='MyRamp',T=150,F=1.0/





RAINDANCE SCIENCE

The Fire

• Fuel is injected at such rate that, if burnt, produces HRRPUA.



- Fuel is injected at such rate that, if burnt, produces HRRPUA
- Adding HRRPUA and TMPIGN to any surface converts it into a fire when TMPIGN is reached.



- Fuel is injected at such rate that, if burnt, produces HRRPUA
- Adding HRRPUA and TMPIGN to any surface converts it into a fire when TMPIGN is reached.→Carful with that!



- Fuel is injected at such rate that, if burnt, produces HRRPUA
- Adding HRRPUA and TMPIGN to any surface converts it into a fire when TMPIGN is reached.→Carful with that!
- Alternatively you can prescribe MLRPUA. This will produce injection of gas at a rate of MLRPUA, which will burn if it finds adequate conditions.



- Fuel is injected at such rate that, if burnt, produces HRRPUA
- Adding HRRPUA and TMPIGN to any surface converts it into a fire when TMPIGN is reached.→Carful with that!
- Alternatively you can prescribe MLRPUA. This will produce injection of gas at a rate of MLRPUA, which will burn if it finds adequate conditions.
- A radially spreading fire can be prescribed by: &VENT XB=0.0,5.0,1.5,9.5,0.0,0.0,SURF_ID='FIRE', XYZ=1.5,4.0,0.0,SPREAD_RATE=0.03/



- Fuel is injected at such rate that, if burnt, produces HRRPUA
- Adding HRRPUA and TMPIGN to any surface converts it into a fire when TMPIGN is reached.→Carful with that!
- Alternatively you can prescribe MLRPUA. This will produce injection of gas at a rate of MLRPUA, which will burn if it finds adequate conditions.
- A radially spreading fire can be prescribed by: &VENT XB=0.0,5.0,1.5,9.5,0.0,0.0,SURF_ID='FIRE', XYZ=1.5,4.0,0.0,SPREAD_RATE=0.03/
- You can also define pyrolysis parameters and get FDS to mimic a "real" fire.



- Fuel is injected at such rate that, if burnt, produces HRRPUA
- Adding HRRPUA and TMPIGN to any surface converts it into a fire when TMPIGN is reached.→Carful with that!
- Alternatively you can prescribe MLRPUA. This will produce injection of gas at a rate of MLRPUA, which will burn if it finds adequate conditions.
- A radially spreading fire can be prescribed by: &VENT XB=0.0,5.0,1.5,9.5,0.0,0.0,SURF_ID='FIRE', XYZ=1.5,4.0,0.0,SPREAD_RATE=0.03/
- You can also define pyrolysis parameters and get FDS to mimic a "real" fire.→VERY Carful with that!

• Mechanical ventilation (i.e. fancoils) can be modelled as air-flow coming into or leaving the domain.





- Mechanical ventilation (i.e. fancoils) can be modelled as air-flow coming into or leaving the domain.
- The flow "disappears" ("appears") at the boundary.



- Mechanical ventilation (i.e. fancoils) can be modelled as air-flow coming into or leaving the domain.
- The flow "disappears" ("appears") at the boundary.

Air supply:

&SURF ID='SUPPLY', VEL=-1.2, COLOR='BLUE' /
&VENT XB=5.0,5.0,1.0,1.4,2.0,2.4, SURF_ID='SUPPLY' /



- Mechanical ventilation (i.e. fancoils) can be modelled as air-flow coming into or leaving the domain.
- The flow "disappears" ("appears") at the boundary.

Air supply:

&SURF ID='SUPPLY', VEL=-1.2, COLOR='BLUE' /
&VENT XB=5.0,5.0,1.0,1.4,2.0,2.4, SURF_ID='SUPPLY' /

Exhaust:

&SURF ID='EXHAUST', VEL=1.2, COLOR='RED' /
&VENT XB=5.0,5.0,1.8,3.3,2.0,2.4, SURF_ID='EXHAUST' /



• Point "measurements" are obtained by adding "measuring" Devices:





● Point "measurements" are obtained by adding "measuring" Devices:
 → &DEVC XYZ=2.0,6.4,0.0,QUANTITY='TEMPERATURE'/



- Point "measurements" are obtained by adding "measuring" Devices:
 - \rightarrow &DEVC XYZ=2.0,6.4,0.0,QUANTITY='TEMPERATURE'/
 - \rightarrow If a volume is given instead of a point, an integrated quantity is recorded (HRR, Average Temperature)



- Point "measurements" are obtained by adding "measuring" Devices:
 - \rightarrow &DEVC XYZ=2.0,6.4,0.0,QUANTITY='TEMPERATURE'/
 - \rightarrow If a volume is given instead of a point, an integrated quantity is recorded (HRR, Average Temperature)
- Point "measurements" are recorded in spreadsheet format (CHID_devc.csv)



- Point "measurements" are obtained by adding "measuring" Devices:
 - \rightarrow &DEVC XYZ=2.0,6.4,0.0,QUANTITY='TEMPERATURE'/
 - \rightarrow If a volume is given instead of a point, an integrated quantity is recorded (HRR, Average Temperature)
- Point "measurements" are recorded in spreadsheet format (CHID_devc.csv)
- Devices (DEVC) can also be used to control actions:



- Point "measurements" are obtained by adding "measuring" Devices:
 PDEVG_XXZ=2_0_6_4_0_0_0ULANTITY= TEMPERATURE 1 (
 - \rightarrow &DEVC XYZ=2.0,6.4,0.0,QUANTITY='TEMPERATURE'/ \rightarrow If a volume is given instead of a point an integrated quant
 - \rightarrow If a volume is given instead of a point, an integrated quantity is recorded (HRR, Average Temperature)
- Point "measurements" are recorded in spreadsheet format (CHID_devc.csv)
- Devices (DEVC) can also be used to control actions: \rightarrow Smoke detectors, Sprinklers etc.



- - \rightarrow &DEVC XYZ=2.0,6.4,0.0,QUANTITY='TEMPERATURE'/ \rightarrow If a volume is given instead of a point, an integrated quantity is
 - recorded (HRR, Average Temperature)
- Point "measurements" are recorded in spreadsheet format (CHID_devc.csv)
- Devices (DEVC) can also be used to control actions: \rightarrow Smoke detectors, Sprinklers etc.
- Add SETPOINT to DEVC line:



- Point "measurements" are obtained by adding "measuring" Devices:
 - \rightarrow &DEVC XYZ=2.0,6.4,0.0,QUANTITY='TEMPERATURE'/
 - \rightarrow If a volume is given instead of a point, an integrated quantity is recorded (HRR, Average Temperature)
- Point "measurements" are recorded in spreadsheet format (CHID_devc.csv)
- Devices (DEVC) can also be used to control actions: \rightarrow Smoke detectors, Sprinklers etc.
- Add SETPOINT to DEVC line:

```
&DEVC XYZ=0,0,0,ID='Clock',QUANTITY='TIME',SETPOINT=30.,INITIAL_STATE=.TRUE./
```


- Point "measurements" are obtained by adding "measuring" Devices:
 - \rightarrow &DEVC XYZ=2.0,6.4,0.0,QUANTITY='TEMPERATURE'/
 - \rightarrow If a volume is given instead of a point, an integrated quantity is recorded (HRR, Average Temperature)
- Point "measurements" are recorded in spreadsheet format (CHID_devc.csv)
- Devices (DEVC) can also be used to control actions: \rightarrow Smoke detectors, Sprinklers etc.
- Add SETPOINT to DEVC line and link it to other item: &DEVC XYZ=0,0,0,ID='Clock',QUANTITY='TIME',SETPOINT=30.,INITIAL_STATE=.TRUE./ &OBST XB=...,SURF_ID='...',DEVC_ID='Clock'/



• Slice Files:







- Slice Files:
 - → &SLCF PBZ=0.45, QUANTITY='TEMPERATURE', VECTOR=.TRUE./

Plane parallel to z = 0.45





- Slice Files:
 - \rightarrow &SLCF PBZ=0.45,QUANTITY='TEMPERATURE',VECTOR=.TRUE./



- Slice Files:
 - \rightarrow &SLCF <code>PBZ=0.45,QUANTITY='TEMPERATURE',VECTOR=.TRUE./</code>
- Boundary Files:



- Slice Files:
 - \rightarrow &SLCF <code>PBZ=0.45,QUANTITY='TEMPERATURE',VECTOR=.TRUE./</code>
- Boundary Files:
 - \rightarrow &BNDF QUANTITY='TEMPERATURE'/



- Slice Files:
 - \rightarrow &SLCF PBZ=0.45,QUANTITY='TEMPERATURE',VECTOR=.TRUE./
- Boundary Files:
 - \rightarrow &BNDF QUANTITY='TEMPERATURE'/
 - → Define BNDF_DEFAULT=.FALSE. on the MISC line in order to avoid innecessary output.



- Slice Files:
 - \rightarrow &SLCF PBZ=0.45,QUANTITY='TEMPERATURE',VECTOR=.TRUE./
- Boundary Files:
 - \rightarrow &BNDF QUANTITY='TEMPERATURE'/
 - → Define BNDF_DEFAULT=.FALSE. on the MISC line in order to avoid innecessary output.
 - \rightarrow Define BNDF_OBST=.TRUE. on an OBST line you want to see.



- Slice Files:
 - \rightarrow &SLCF PBZ=0.45,QUANTITY='TEMPERATURE',VECTOR=.TRUE./
- Boundary Files:
 - \rightarrow &BNDF QUANTITY='TEMPERATURE'/
 - → Define BNDF_DEFAULT=.FALSE. on the MISC line in order to avoid innecessary output.
 - \rightarrow Define BNDF_OBST=.TRUE. on an OBST line you want to see.
- Information contained in the slice files can be exported into spreadsheet format if required (using fds2ascii, which can be downloaded from the FDS website).



Finally...

• The last line in an FDSv5 input file is '&TAIL/':





Finally...

• The last line in an FDSv5 input file is '&TAIL/':

&OBST XB=5.6,6.2,5.8,6.6,0.0,2.0,SURF_ID='WALL'/ &OBST XB=5.4,6.2,1.6,5.8,0.0,2.0,SURF_ID='WALL'/

&SURF ID='WALL', MATL_ID='...'

&MATL ID='...'.../
&SLCF PBZ=0.45,QUANTITY='TEMPERATURE',VECTOR=.TRUE./

&TAIL/



• If you run OS X or GNU/Linux, open a terminal.



- If you run OS X or GNU/Linux, open a terminal.
- If you run Windows, open cmd window.



- If you run OS X or GNU/Linux, open a terminal.
- If you run Windows, open cmd window.
- Change directory to where your input file is (cd /to/your/fds/example/path)



- If you run OS X or GNU/Linux, open a terminal.
- If you run Windows, open cmd window.
- Change directory to where your input file is (cd /to/your/fds/example/path)
- Once in your working directory run FDS by typing:



- If you run OS X or GNU/Linux, open a terminal.
- If you run Windows, open cmd window.
- Change directory to where your input file is (cd /to/your/fds/example/path)
- Once in your working directory run FDS by typing:

fds5 inputfile.fds





Let's try...

