

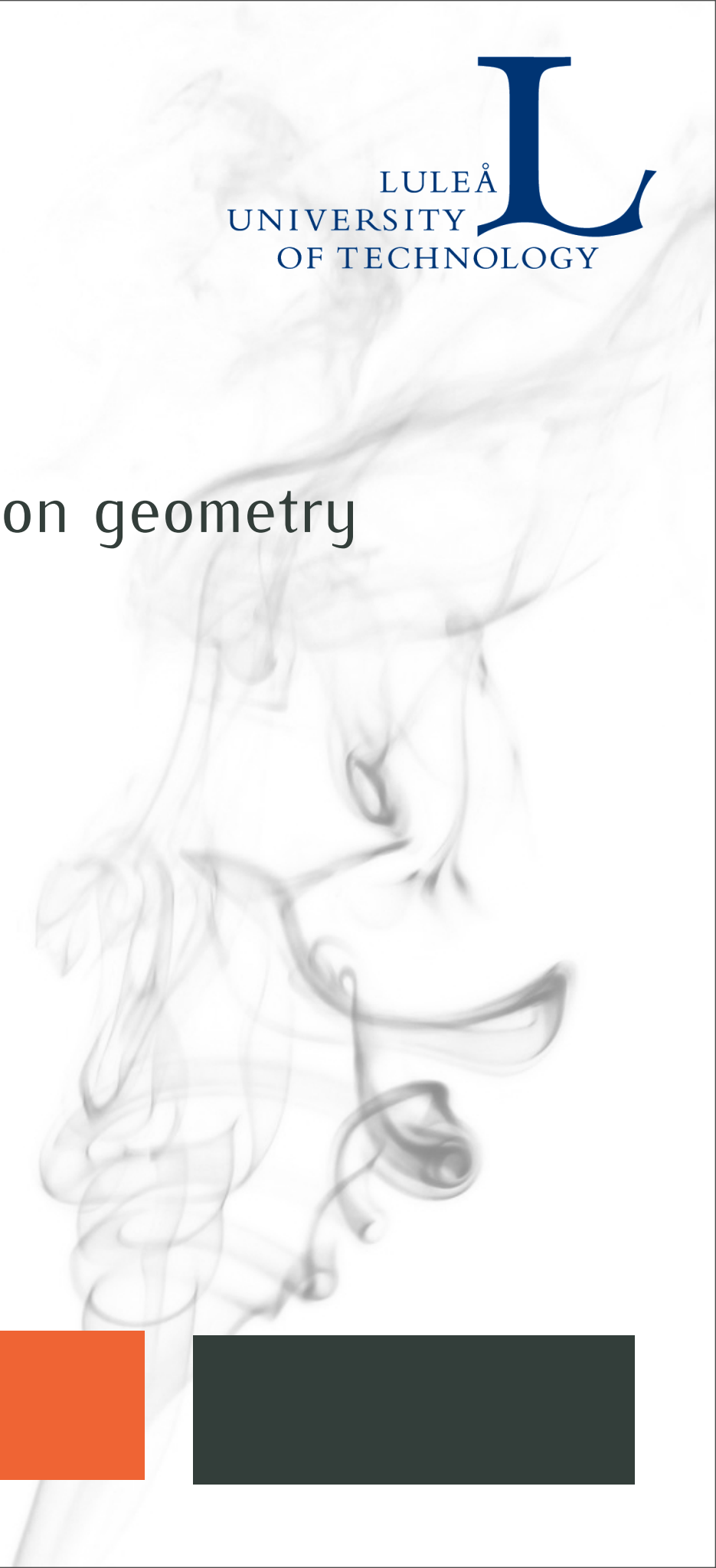
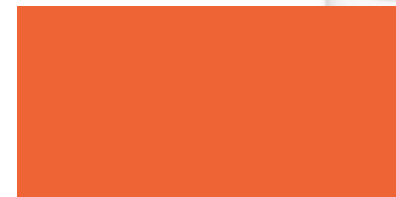
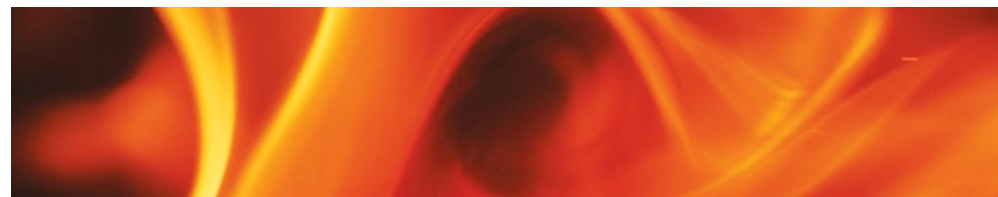
# Fire Modelling

Joakim Sandstrom  
Lulea, 13<sup>th</sup>-15<sup>th</sup> of March 2014



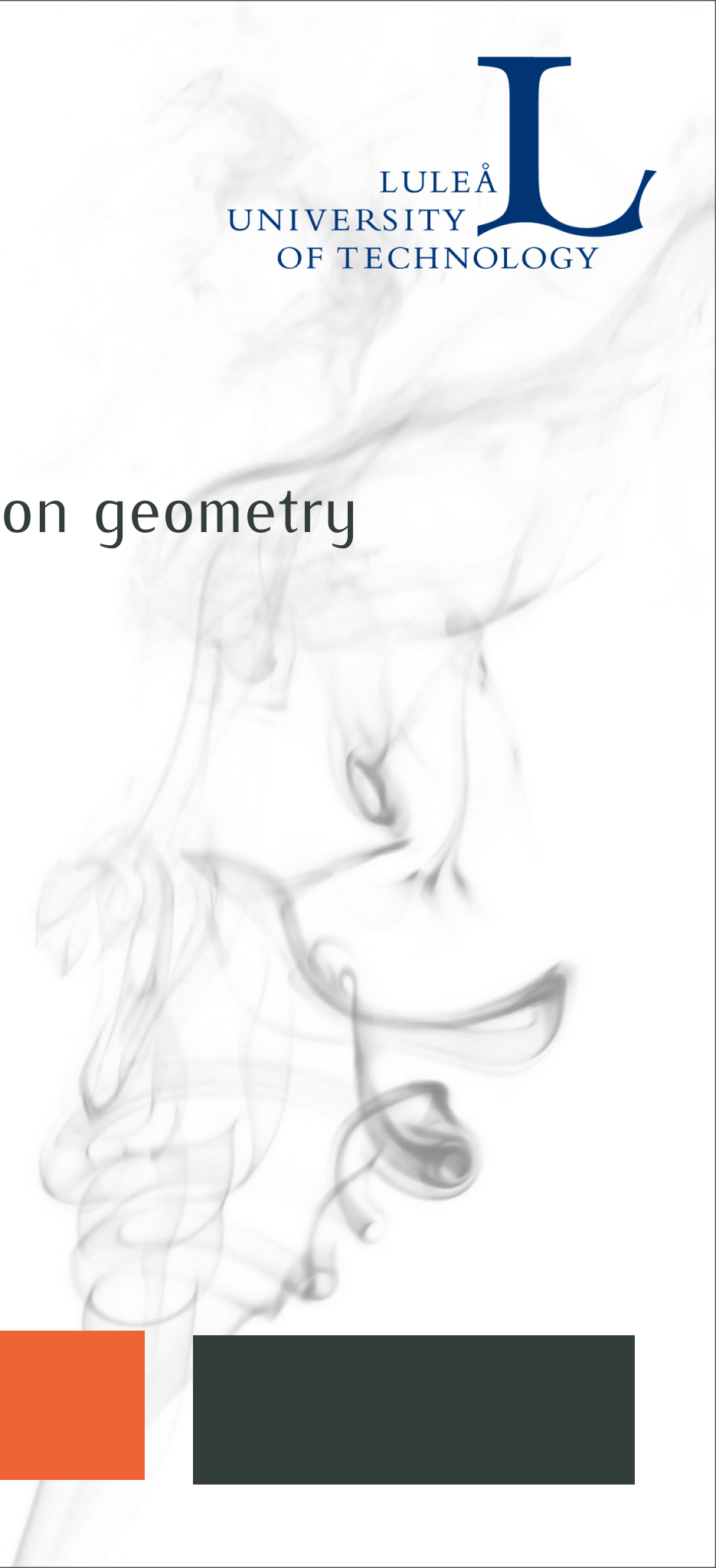
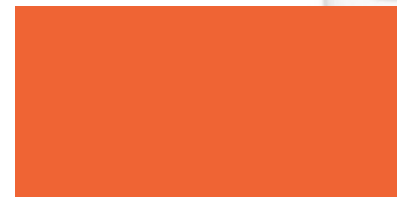
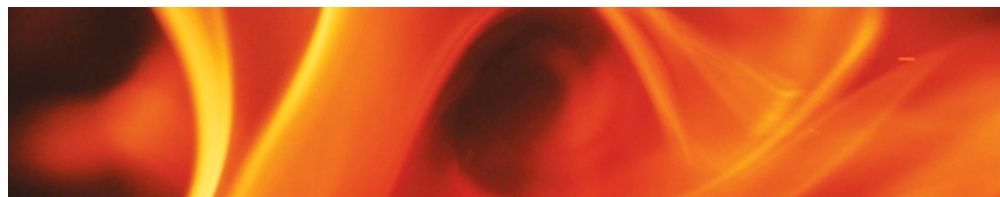
# Introduction

- Smoke management depends strongly on geometry



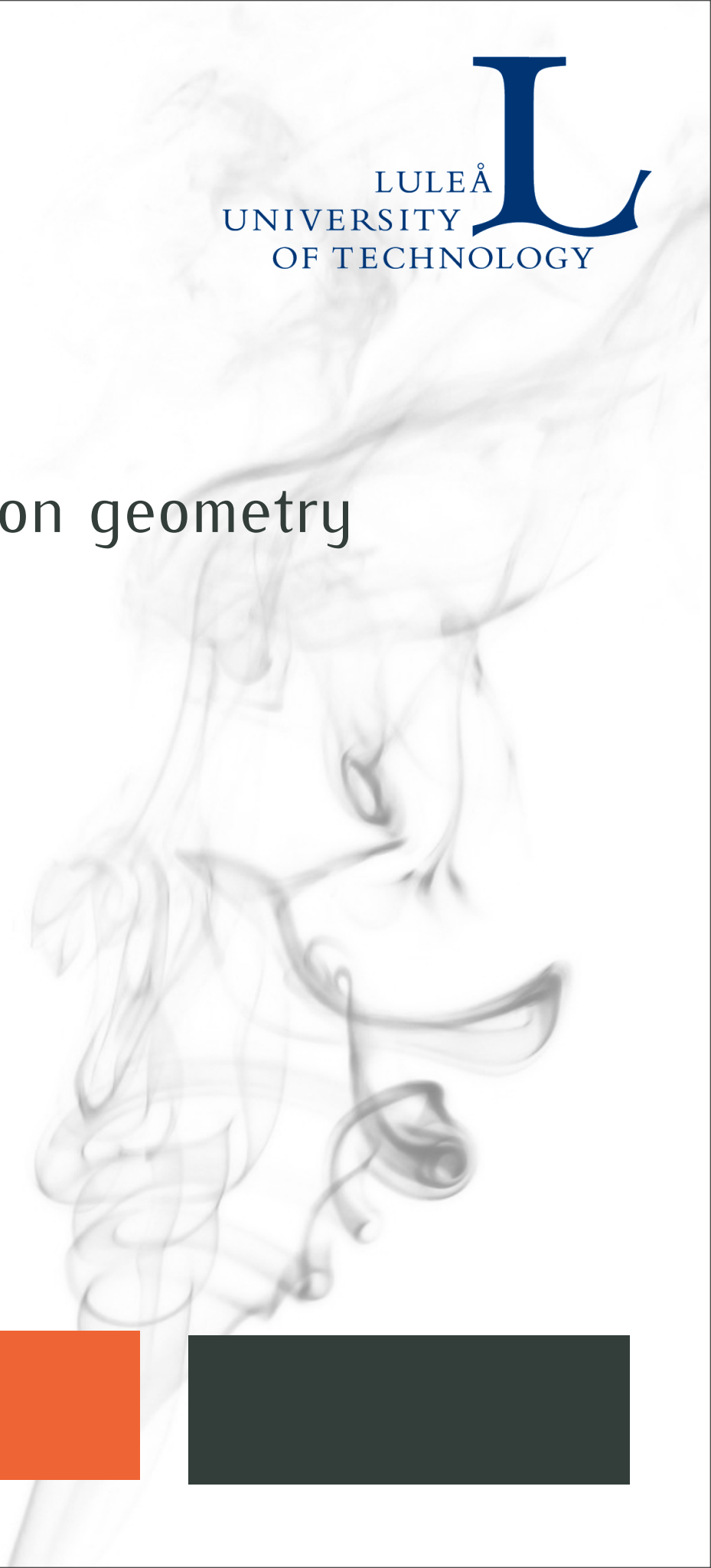
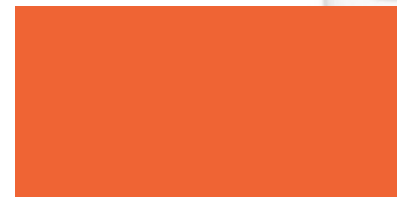
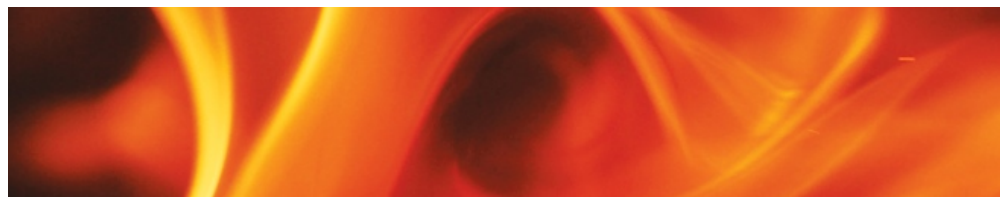
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→ hard to standardise



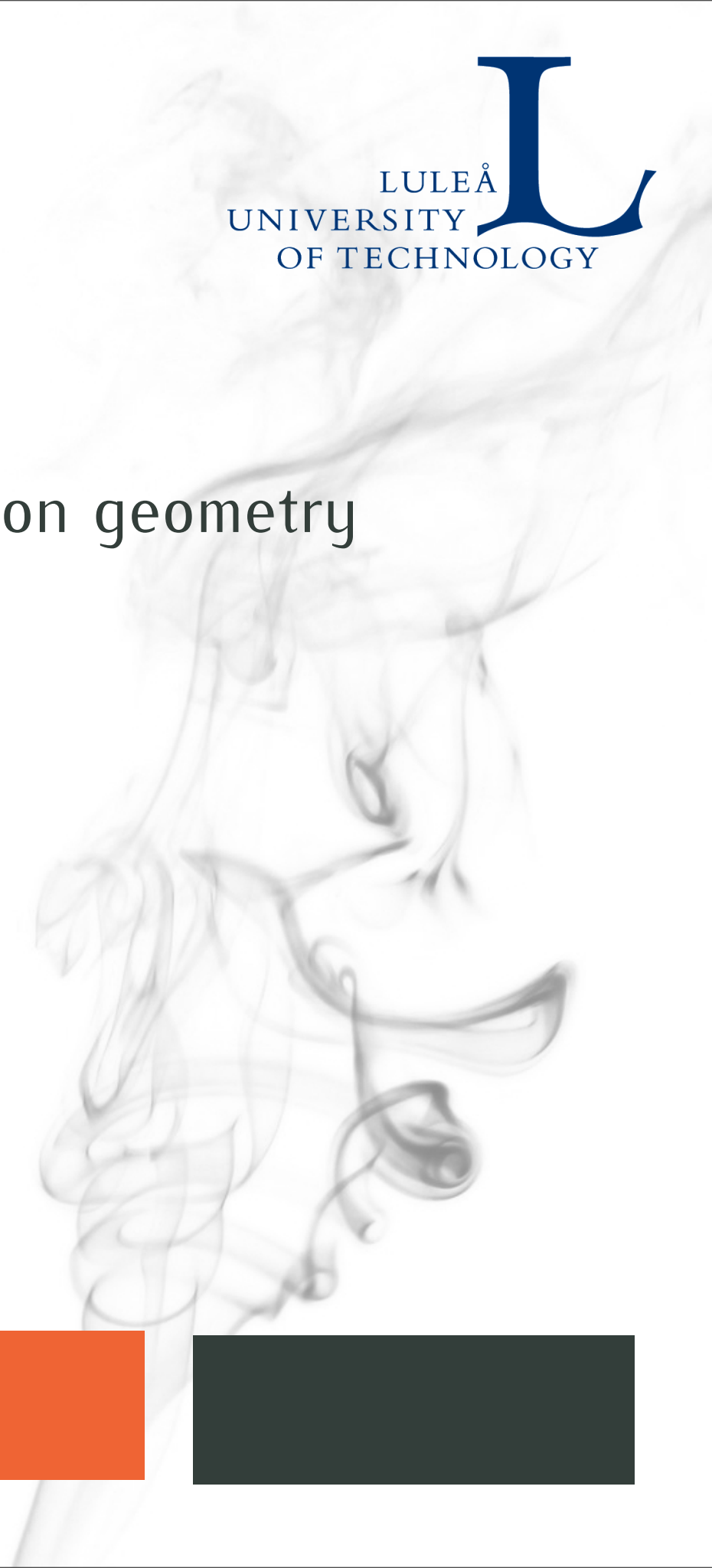
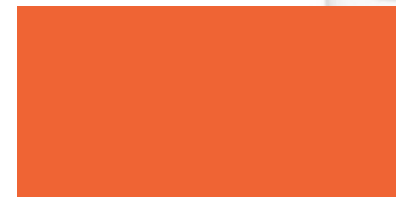
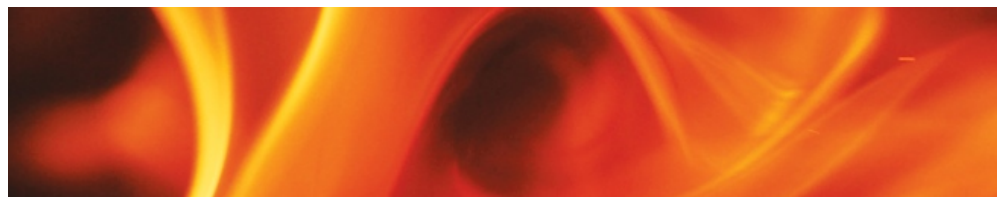
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  - hard to standardise
  - Prescriptive design often impossible



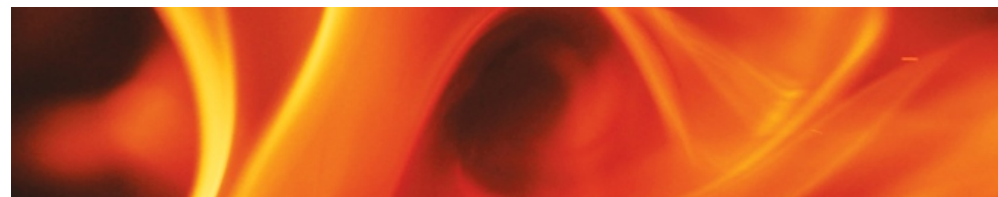
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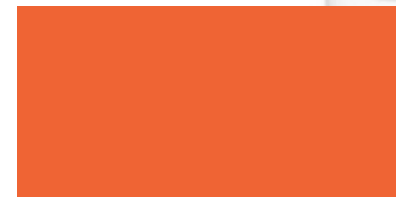
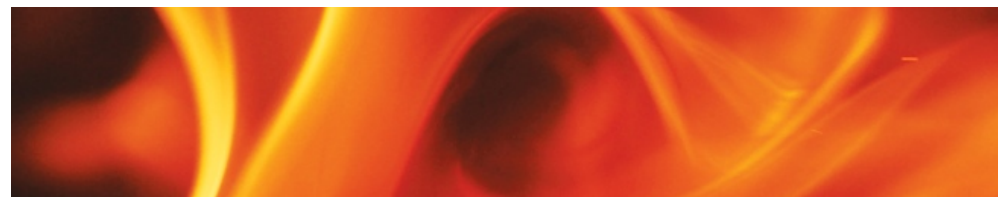
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- This is where Fire Modelling comes into play



# Decisions to be made

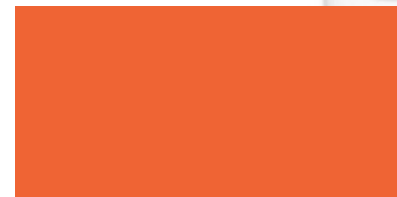
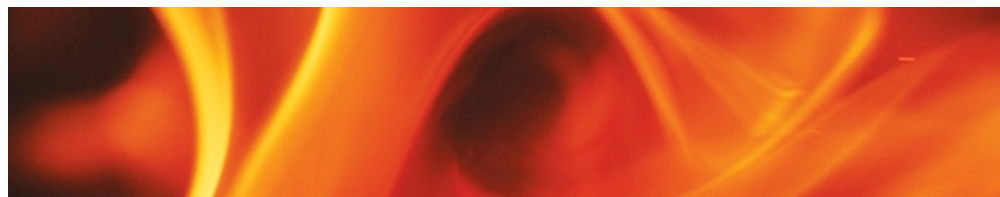
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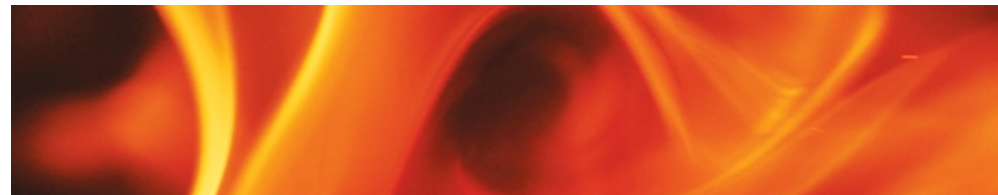
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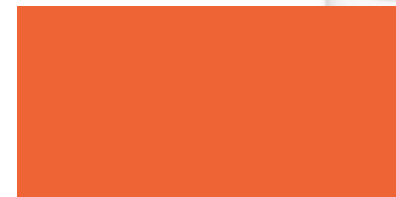
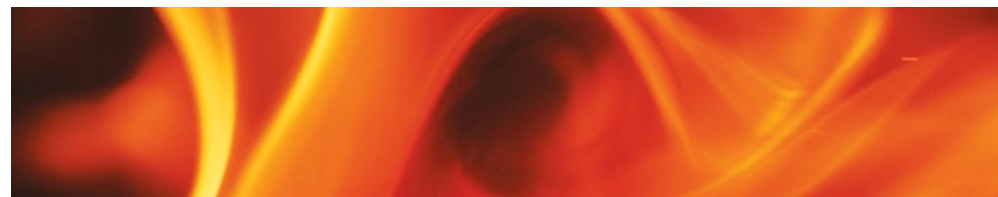
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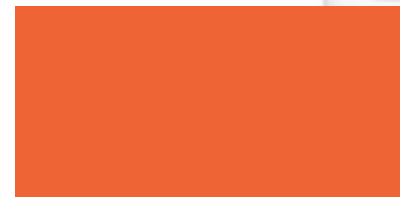
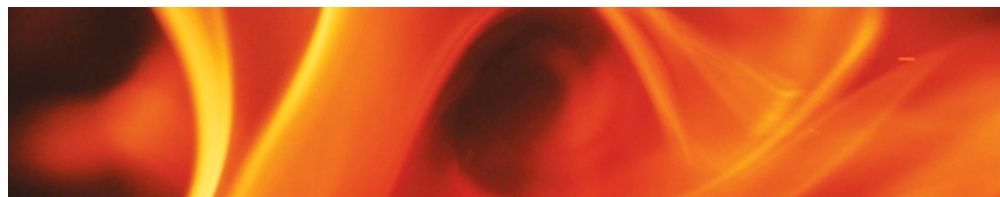
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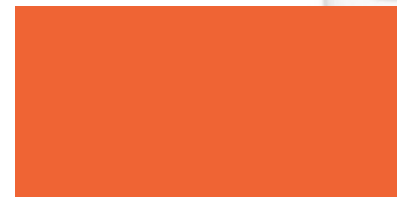
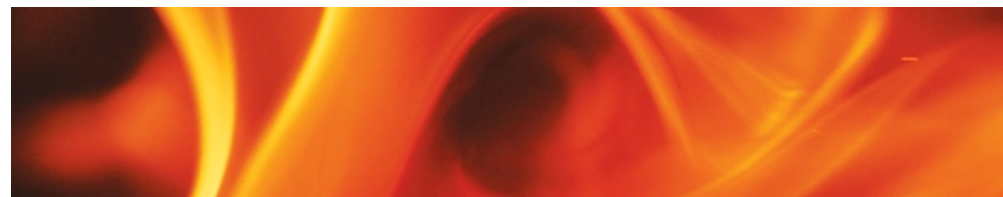
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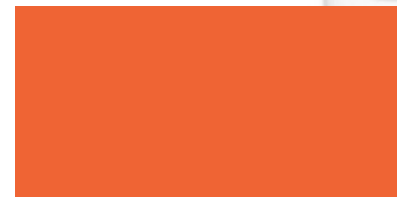
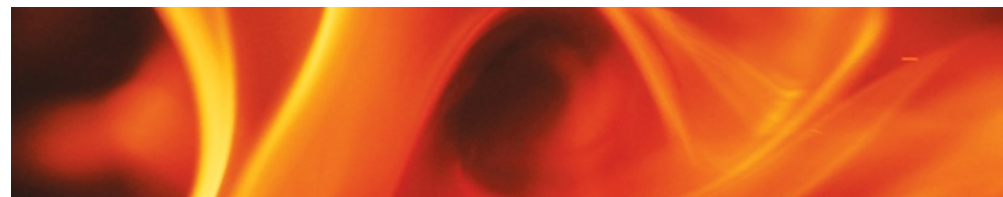


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- What fire?
  - Design fire based on use, geometry and fire load

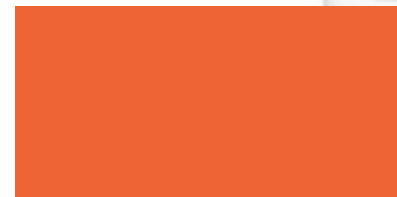
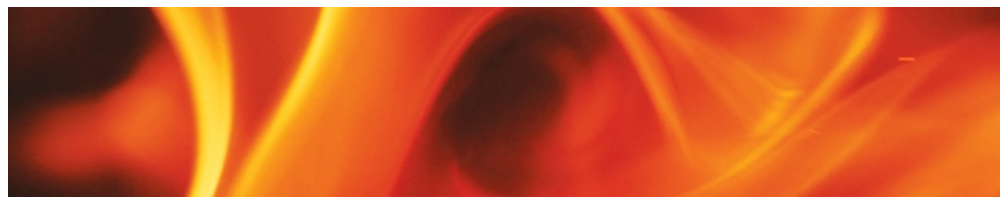


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The choice of Fire Model is not necessarily exclusive. You might need to use CFD and still use correlations.

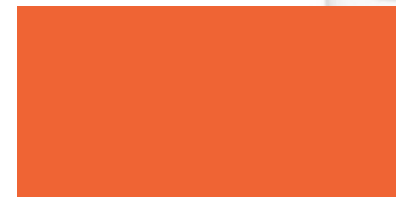
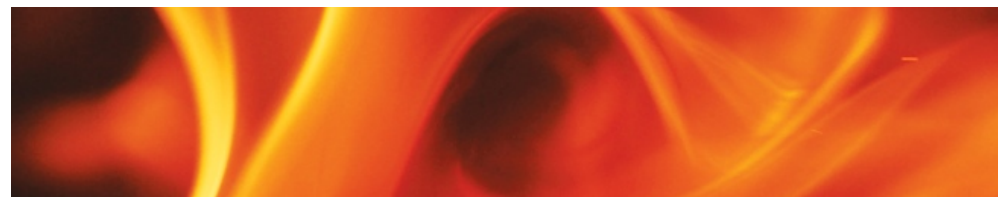




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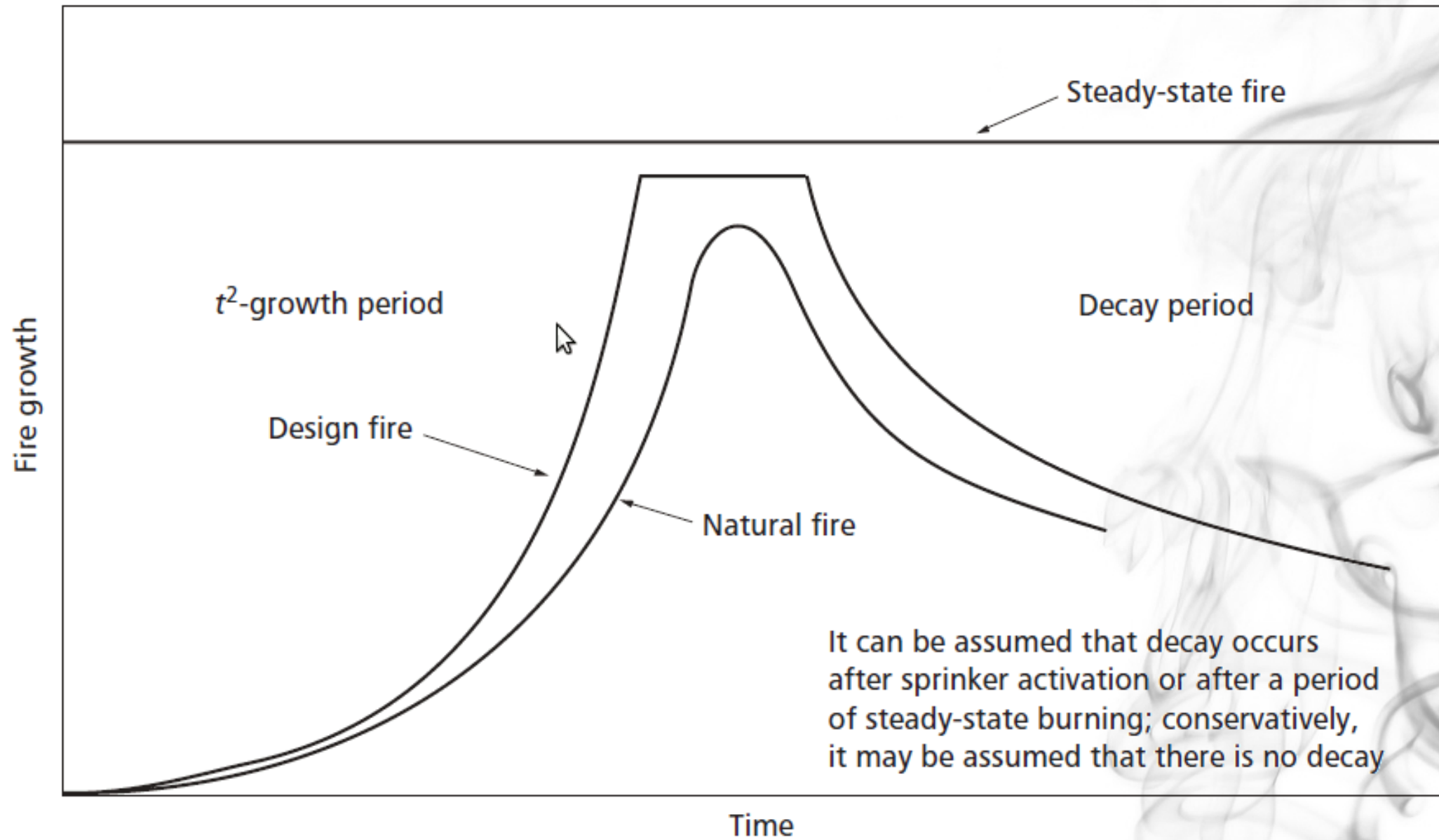
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Design fire need engineering judgement!  
→ There is no single solution..

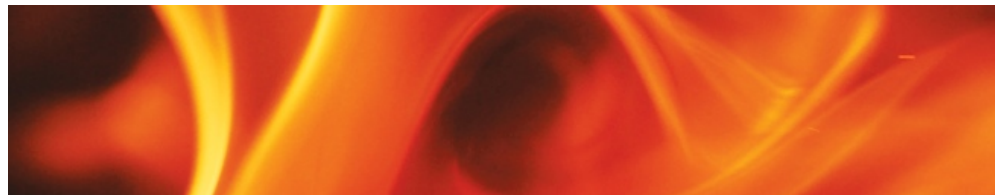




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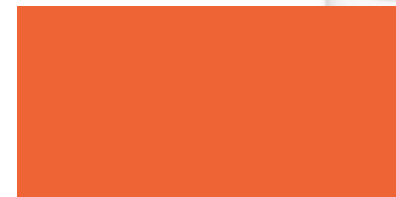
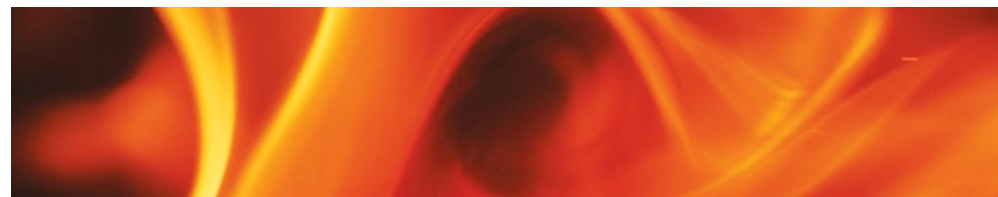


CIBSE Guide E



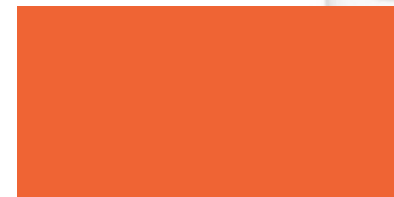
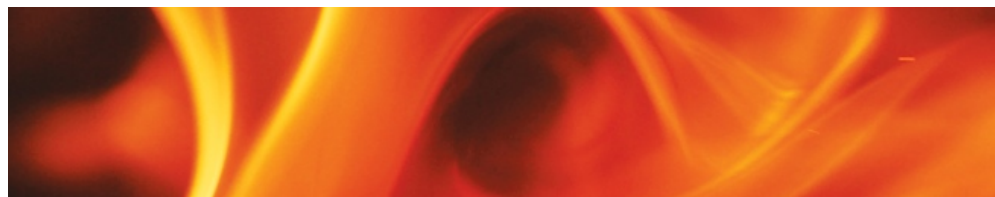
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- Most accepted growth model:  $t^2$ -fire



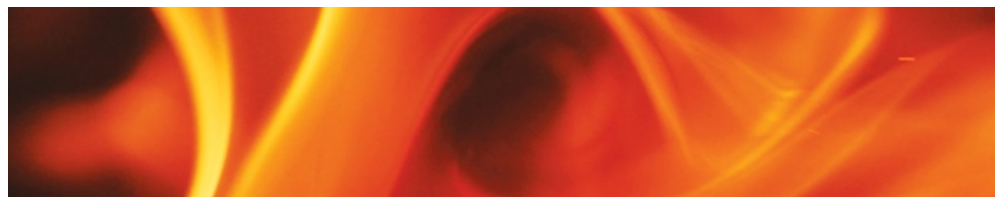
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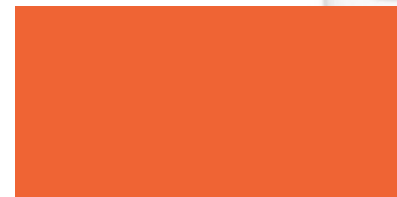
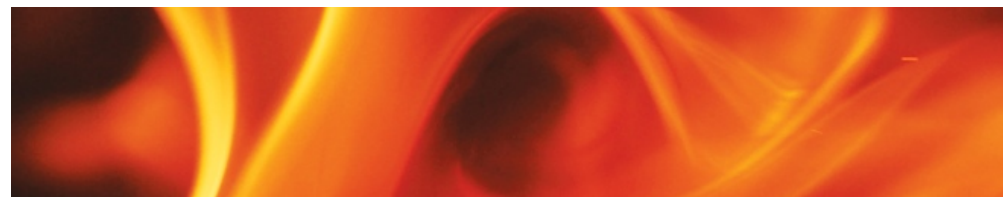


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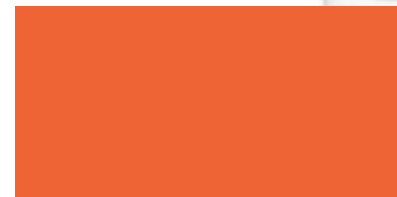
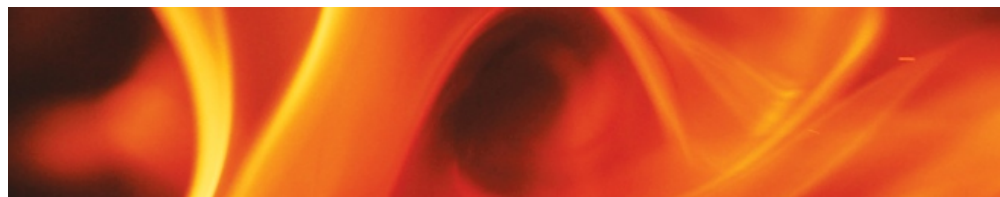


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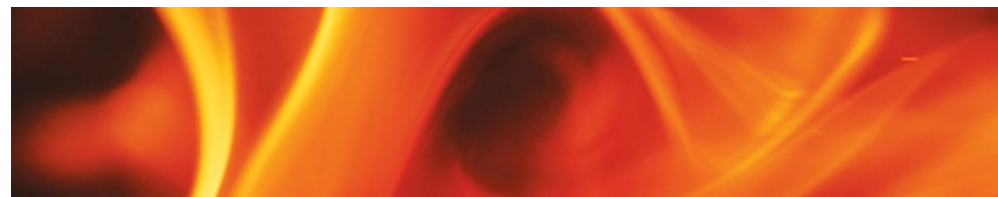


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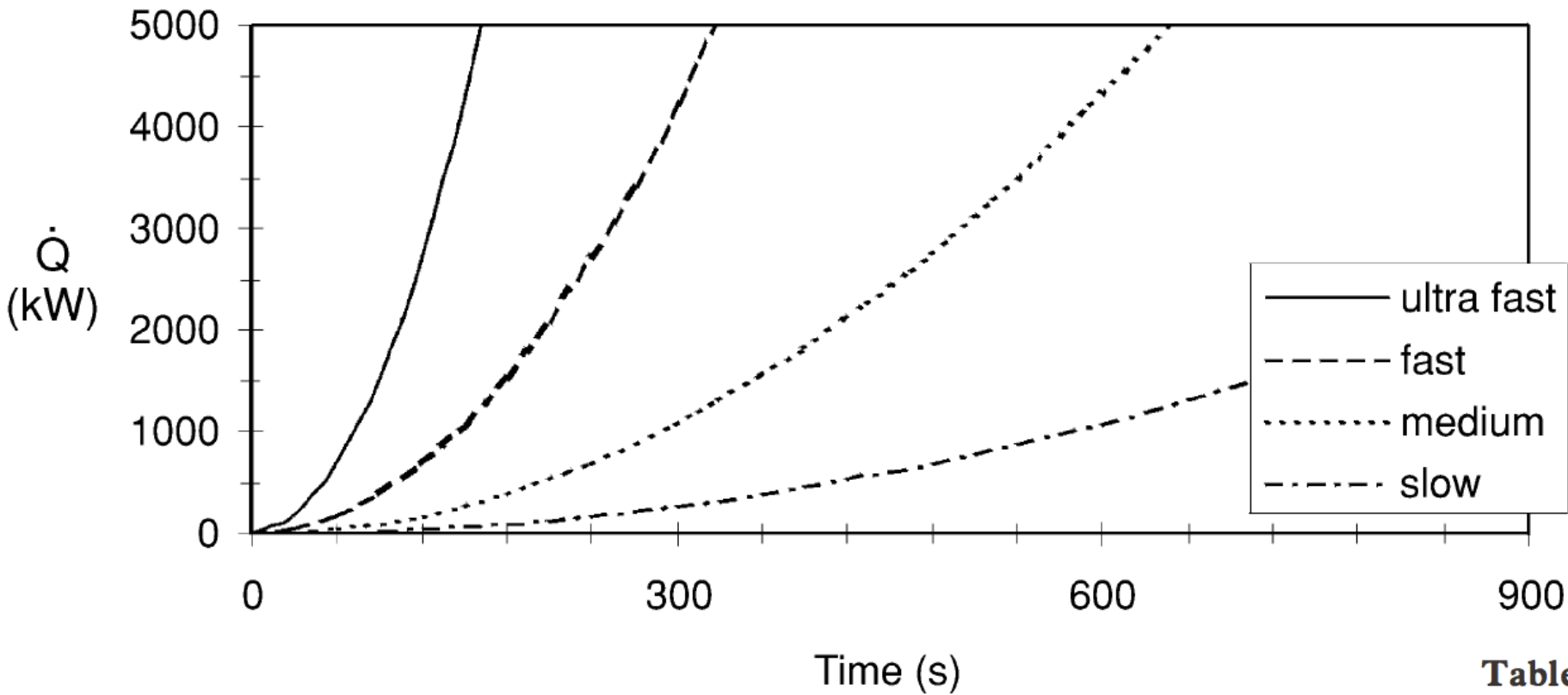
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→ Engineering judgement..





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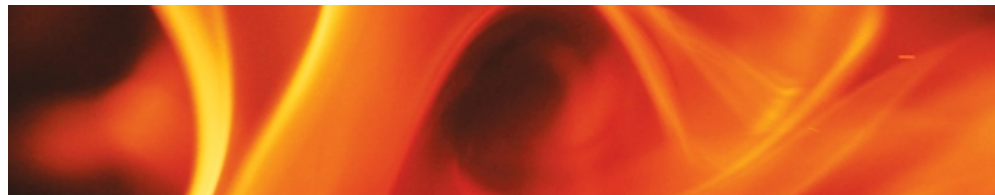


Karlsson – Enclosure Fire Dynamics

**Table 10.1** Characteristic growth time for various classes of fire

Fire class	Characteristic growth time, $t_g$ / s	Constant $a$ / kW·s <sup>-2</sup>
Ultra-fast	75	0.1876
Fast	150	0.0469
Medium	300	0.0117
Slow	600	0.0029

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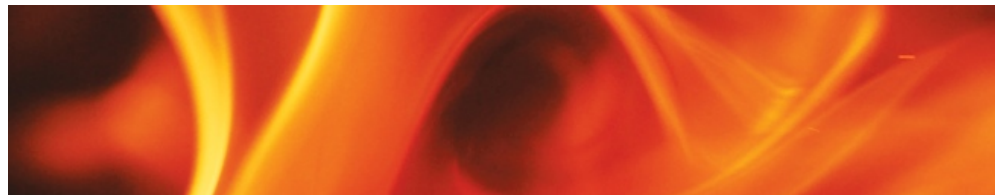
# Design Fires

**Table 10.2** Growth rates for growing fires

Building area providing fuel	Growth rate
Dwelling	Medium
Office	Medium
Shop	Fast
Warehouse	Ultrafast†
Hotel bedroom	Medium
Hotel reception	Medium
Assembly hall seating	Medium–fast
Picture gallery	Slow
Display area	Slow–medium

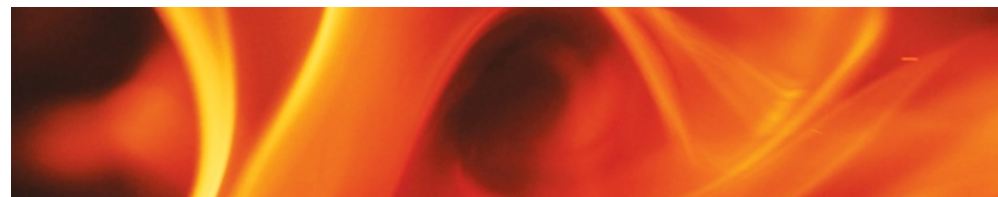
† depends on fire load

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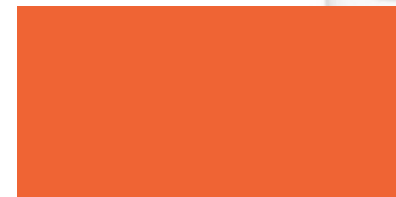
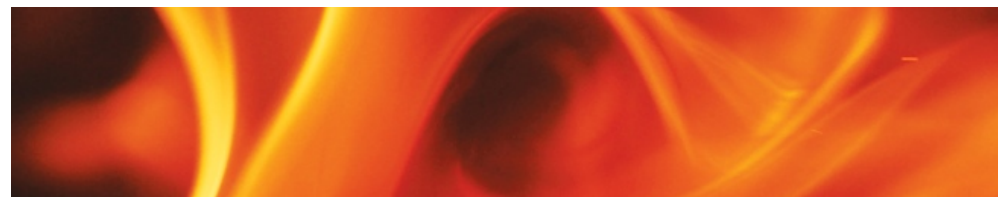
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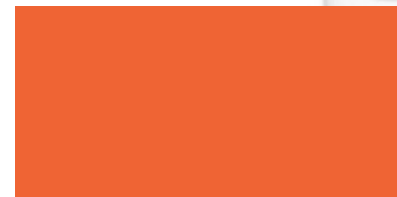
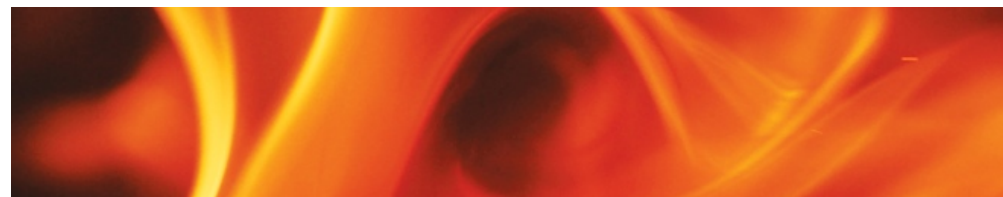
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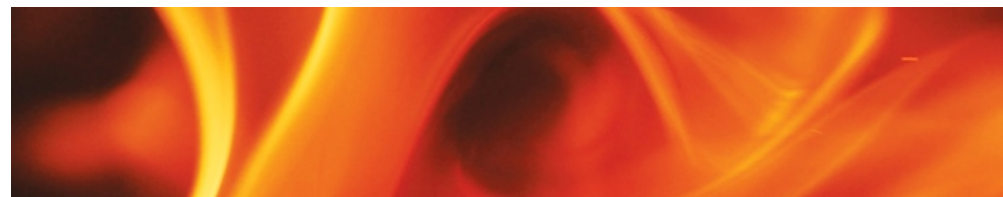




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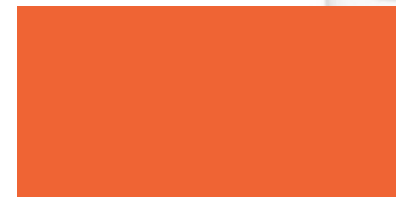
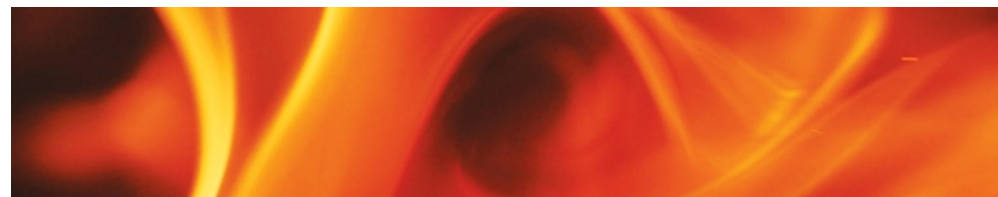


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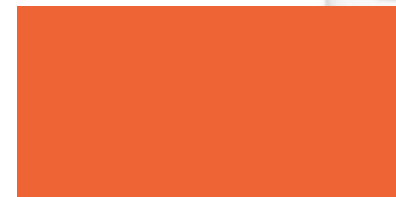
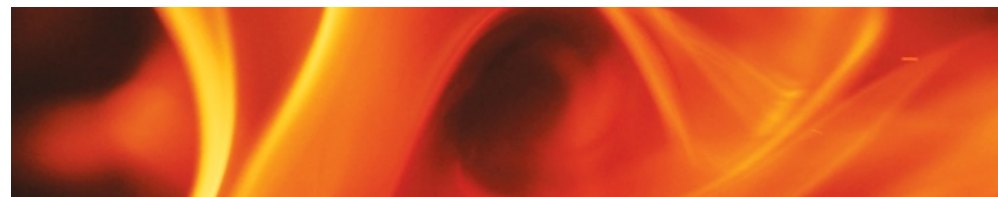
Indications can be found in CIBSE Guide E, SFPE Handbook or NFPA.





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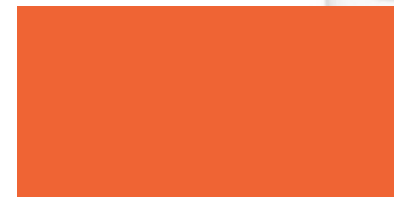
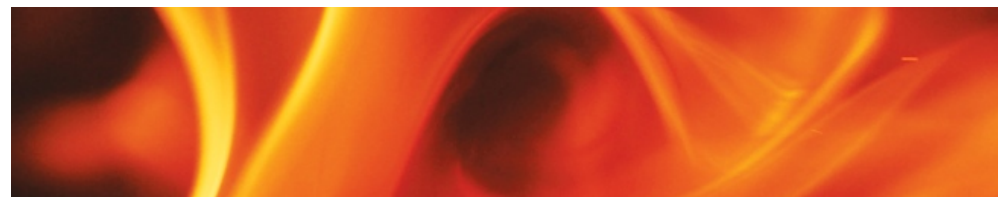
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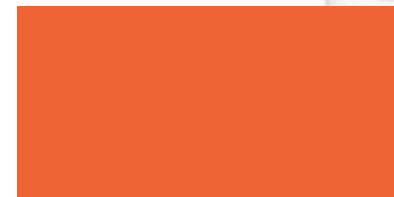
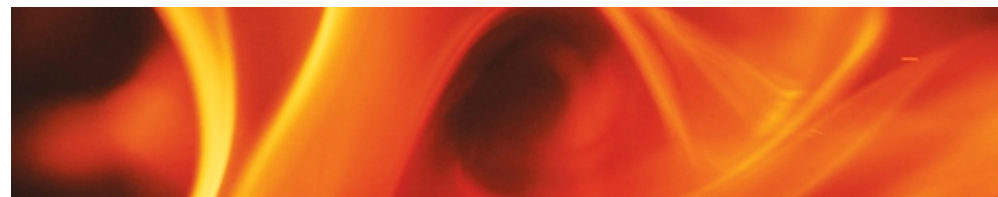
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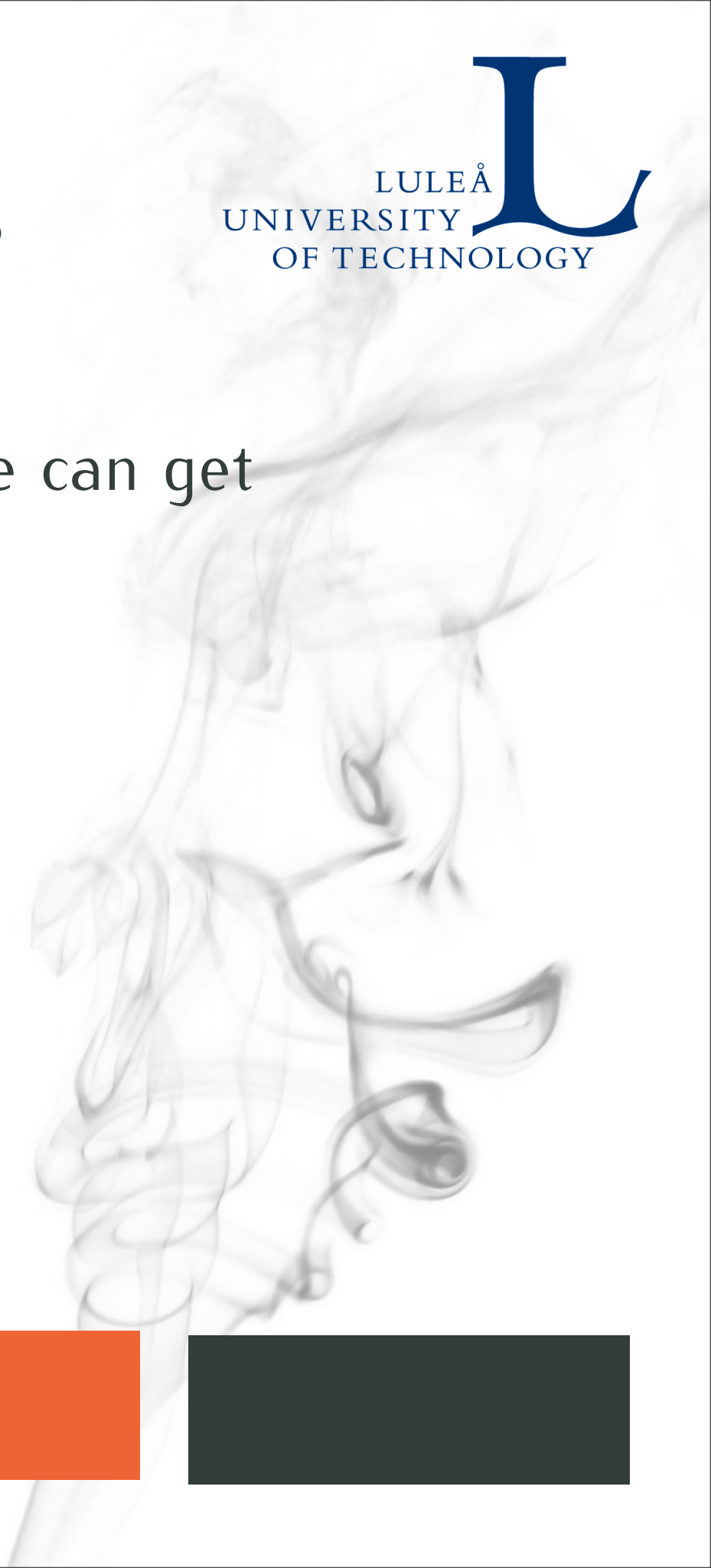
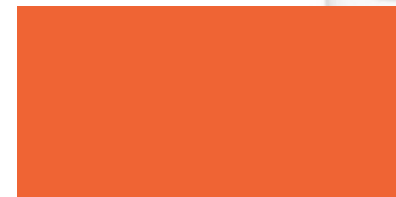
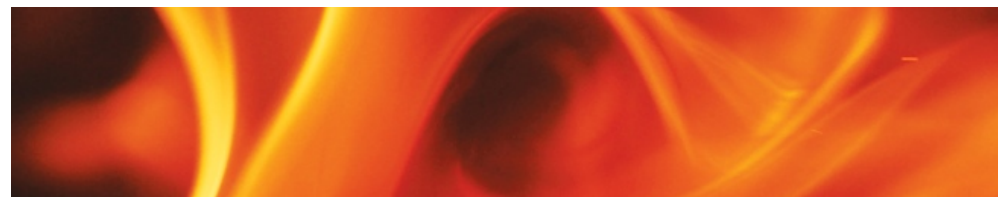
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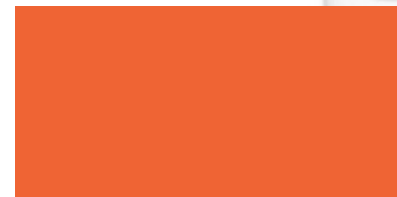
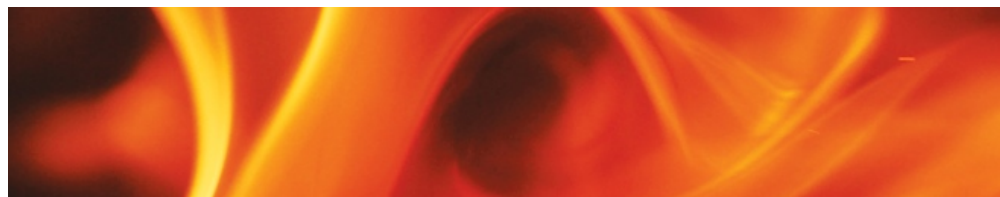
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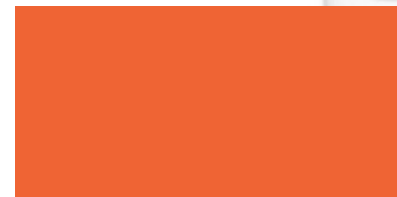
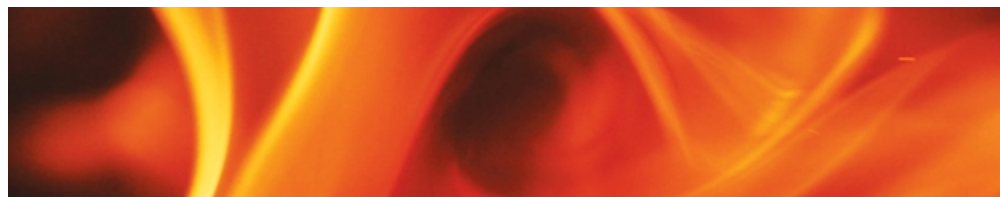
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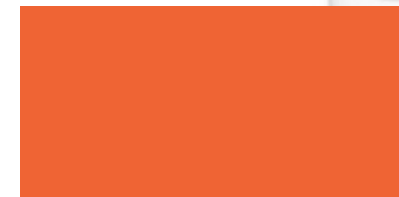
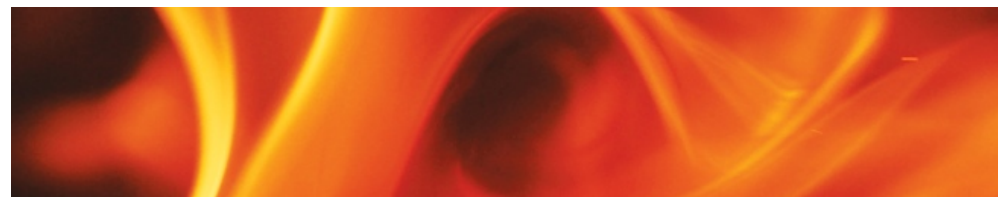




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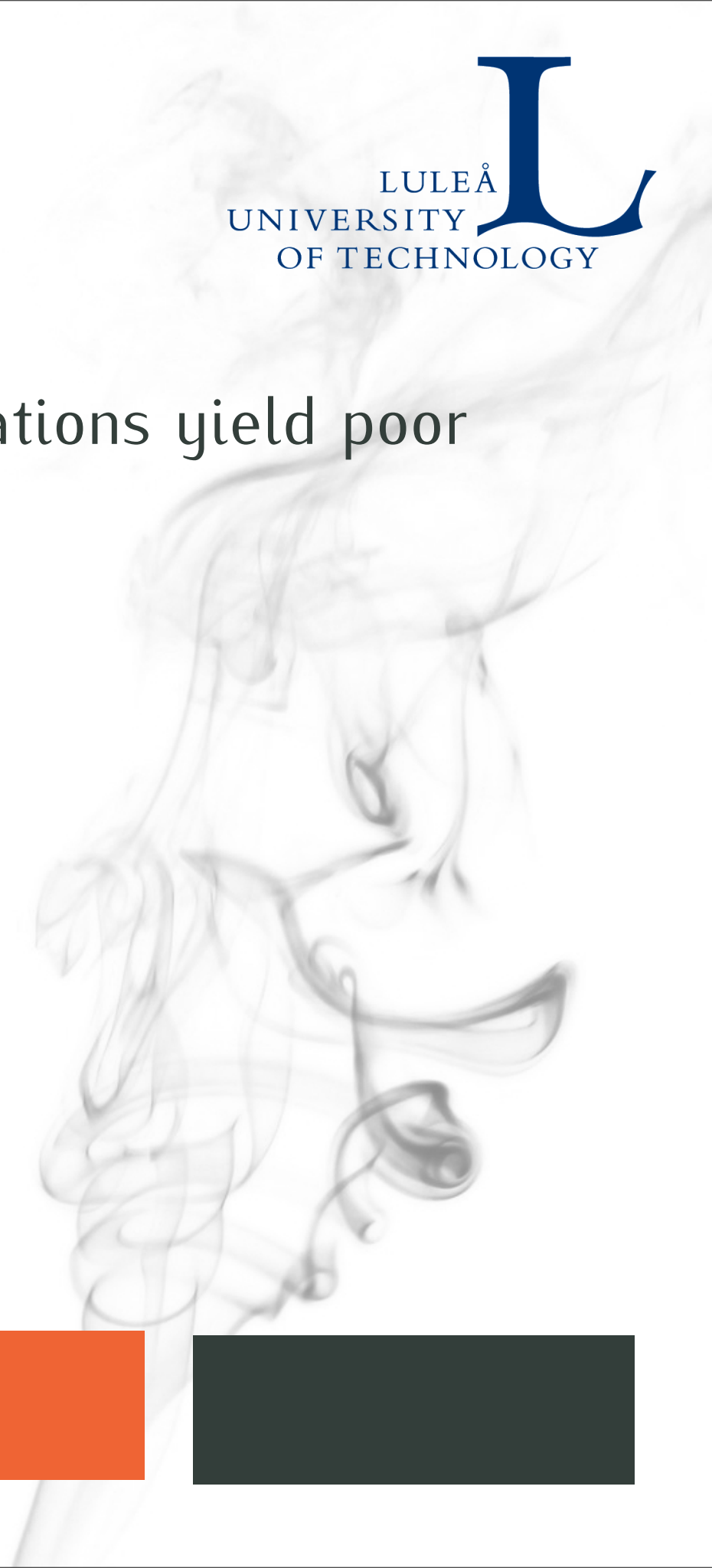
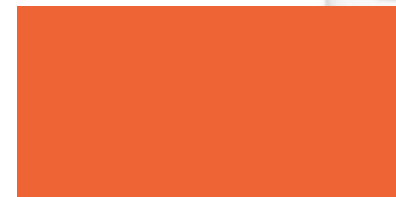
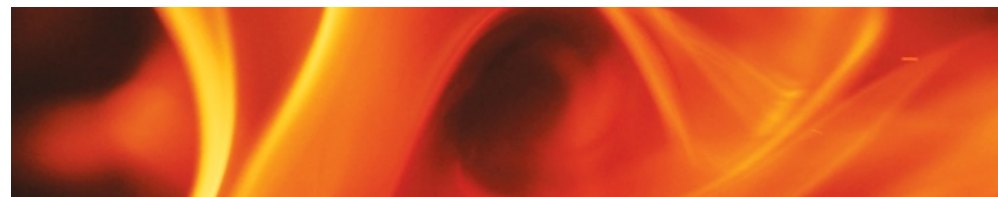
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→ Volume of smoke
- Plume temperature  $T_{\text{smoke}} = T_{\infty} + \frac{\dot{Q}_c}{\dot{m}_{\text{ent}}c_p}$
- Plume velocity  $u_{\text{smoke}} = 3.4 \left( \frac{g}{\rho_{\infty}T_{\infty}c_p} \right)^{1/3} \dot{Q}_c^{1/3} (z - z_0)^{-1/3}$





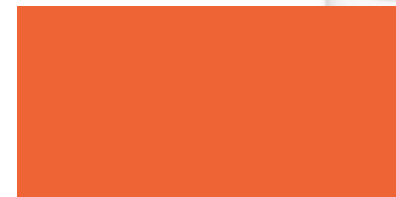
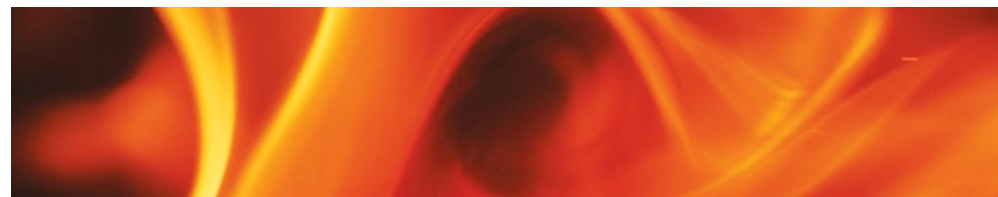
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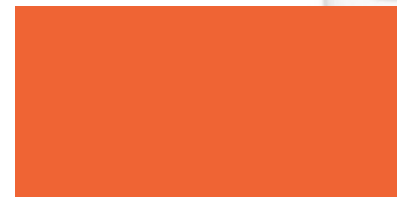
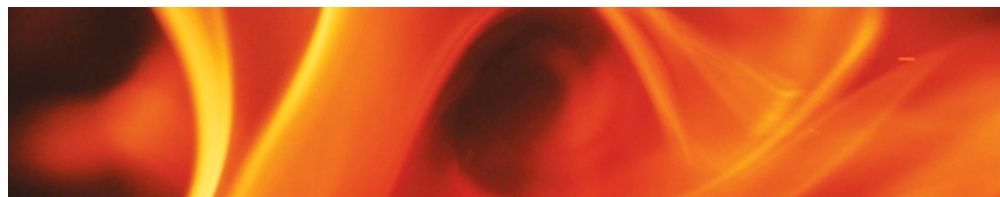
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# Why use Other Models?

- For confined spaces, free plume correlations yield poor results.
- Heat transfer calculations from a fire to the structure.
  - Requires more sophisticated models.
  - If you need spatial resolution (e.g. location of exhaust outlets, gas temperatures for heat transfer calculations), use field models (CFD).

