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WG1: Data Sheets 7-9

Connections in Fire

Ian Burgess



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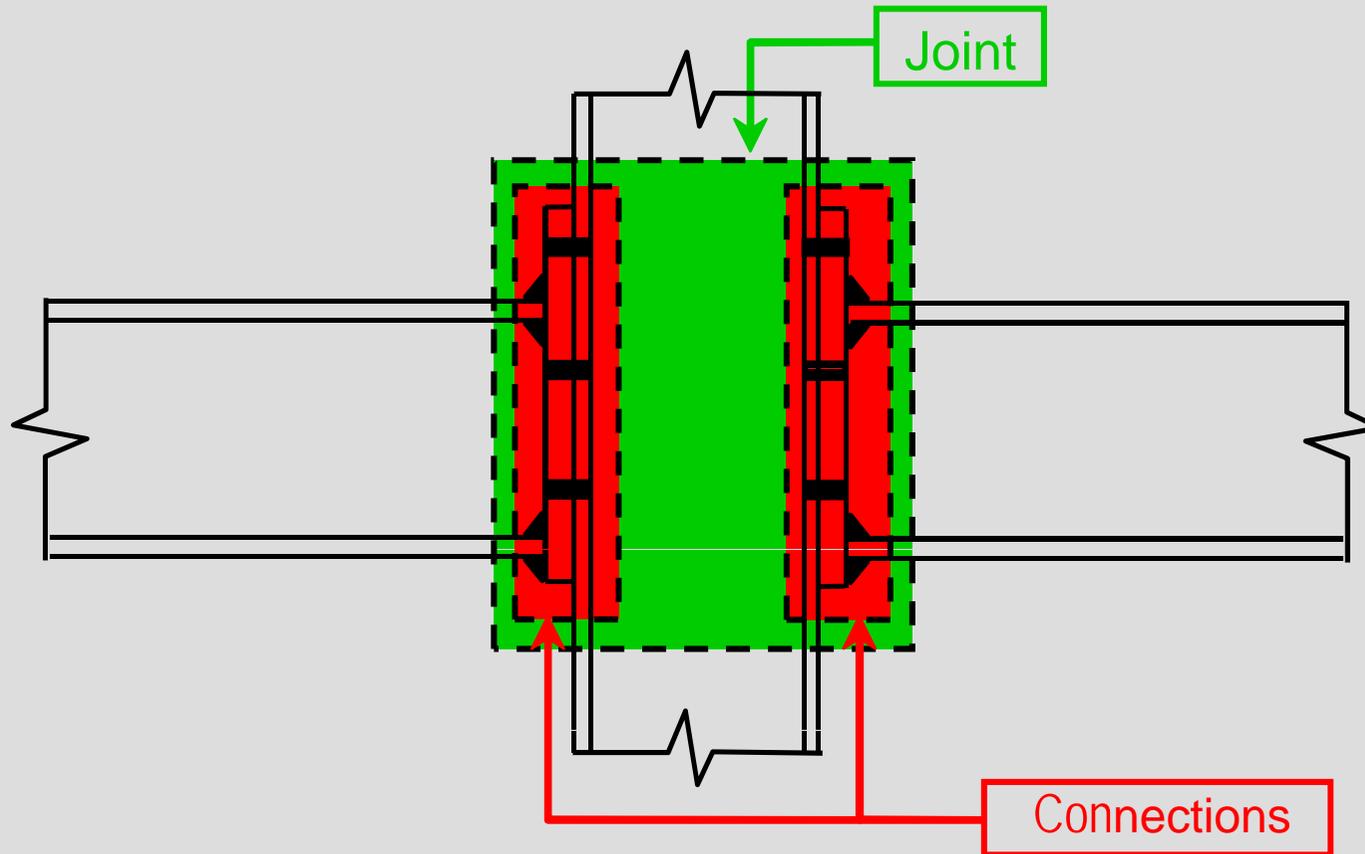
Design

WG1: Data Sheet 9

DESIGN PROCEDURES FOR STEEL AND COMPOSITE JOINTS IN FIRE

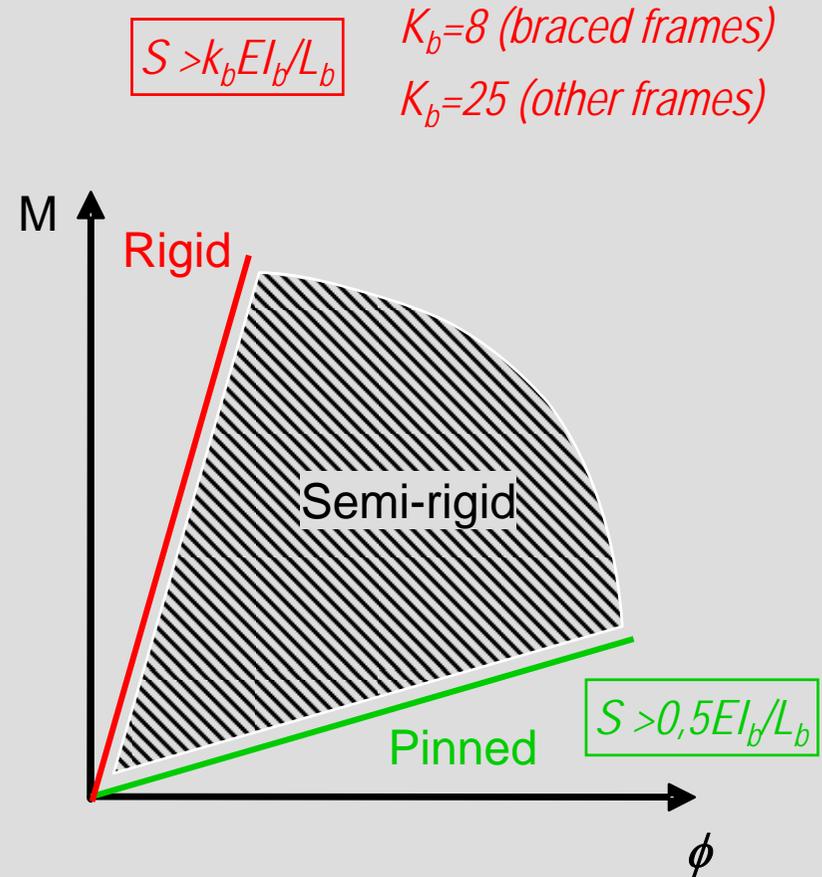
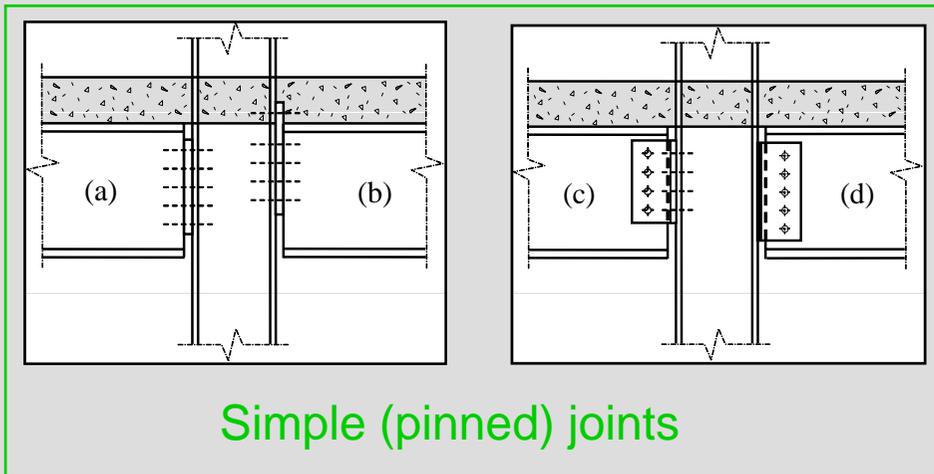
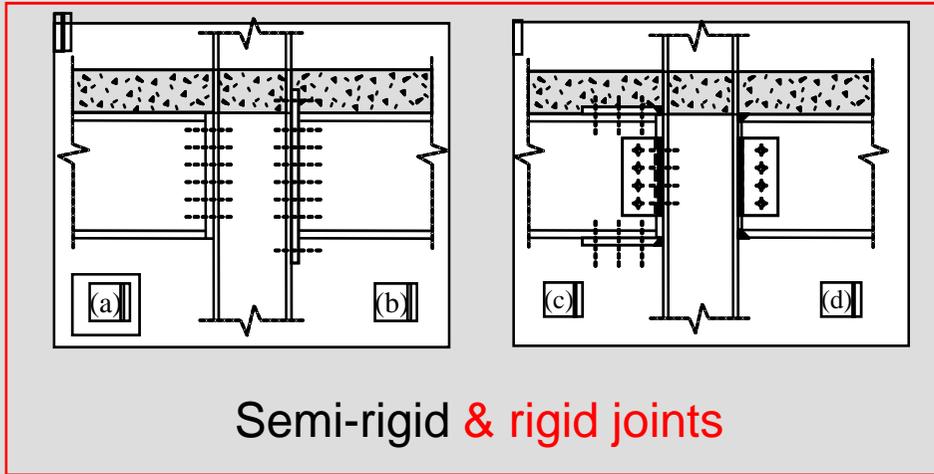


Definition of joint and connection



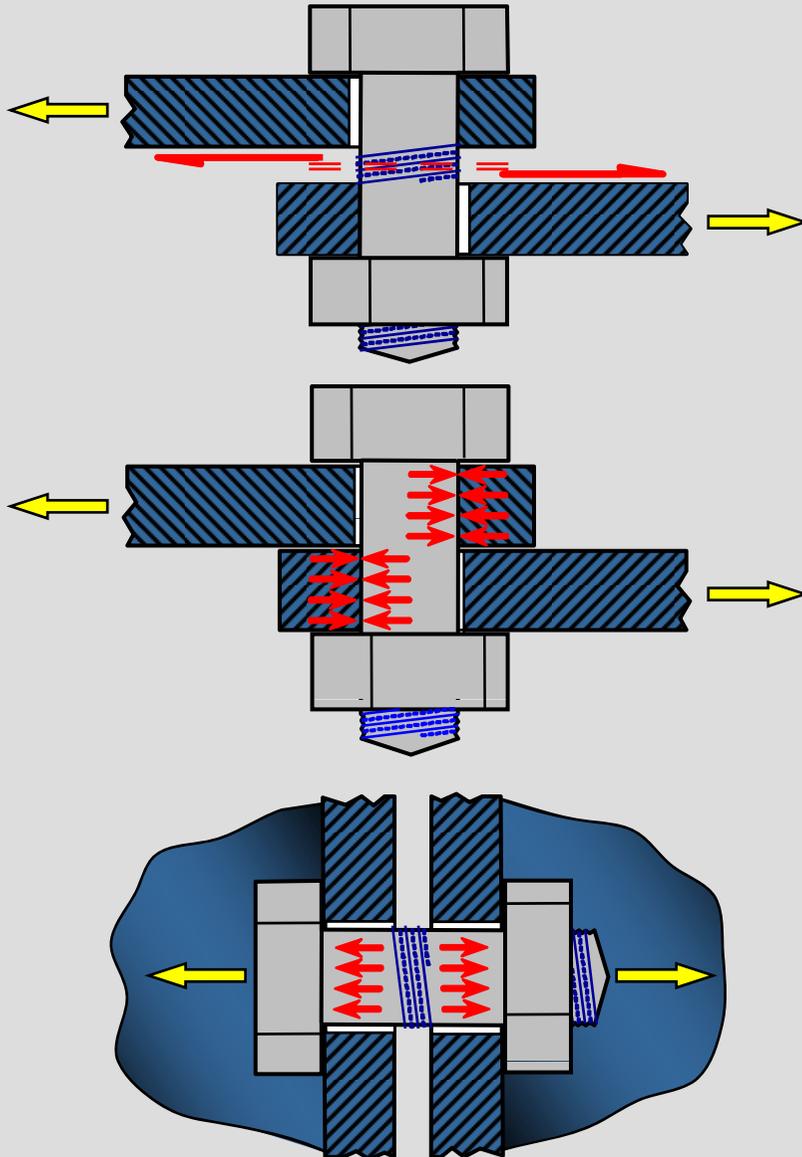


Joint classification at ambient temperature





EN1993-1-2 joint design in fire

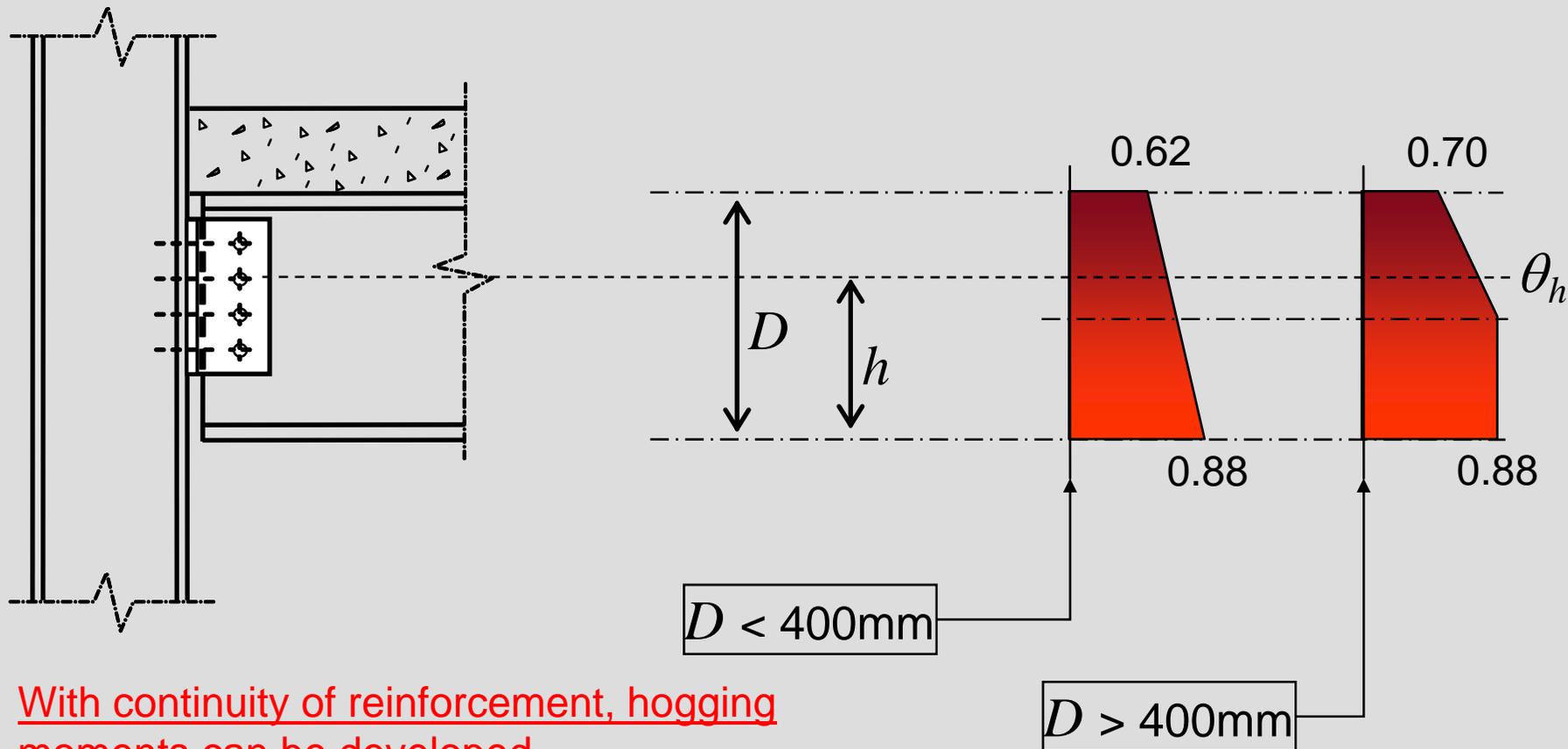


- No provision for semi-rigid behaviour.
- **Annex D** is “informative” only
 - Bolt strength reduction the same for:
 - Shear
 - Bearing
 - No friction
 - 40% reduction if slotted holes
 - Different strength reduction for:
 - Tension
 - Assumes pre-tension lost
 - Reduction factors lower than for structural steel
 - Weld strength reduction
 - Table of reductions for fillet welds
 - Full Penetration butt welds
 - Strength of weaker part joined.
 - Reduction factors over 700°C



Temperature distributions in joints

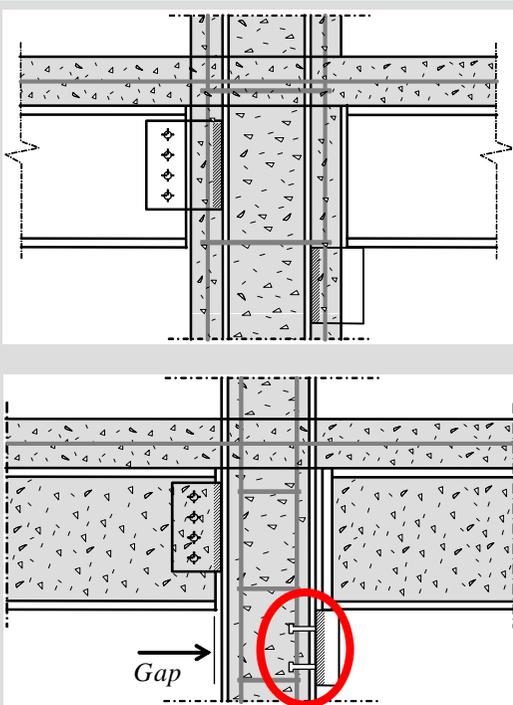
1. Use EC3 incremental temperature analysis on individual connection elements
2. Uniform temperature based on highest element temperature in 1
3. Linearised temperature distribution for beams supporting concrete floor
 - Proportions of beam bottom flange temperature



With continuity of reinforcement, hogging moments can be developed.



Connecting to concrete-encased and web-infilled columns



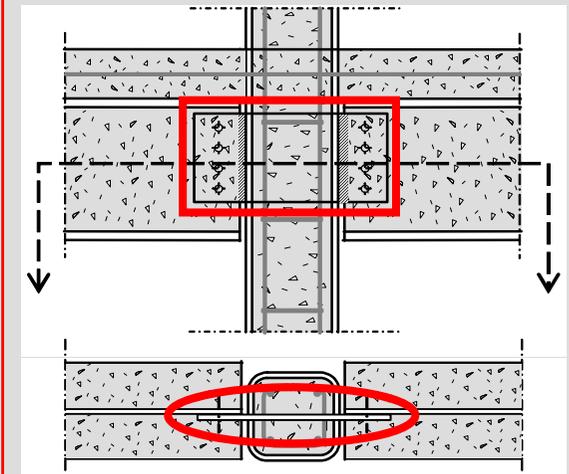
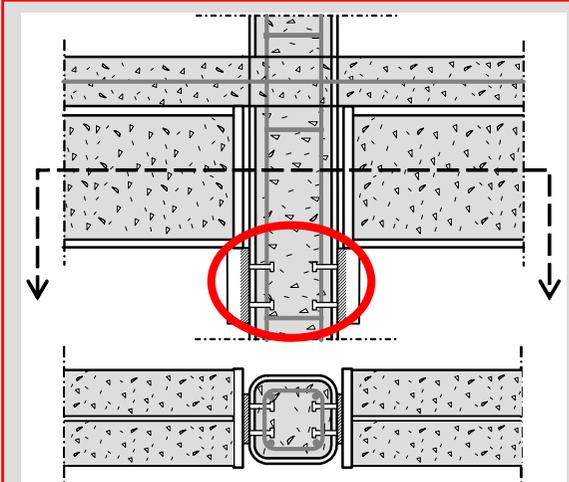
Web-infilled columns

General problem in all cases of composite columns:

- Transfer of vertical shear from beam to the concrete in the column when exposed steel parts are hot.
- Only details in EN1994-1-2 are Fin Plates and Bearing Blocks, pre-welded to column.

Solutions:

- Shear connectors (studs) on column face into infill.
- Single fin plate slotted through hollow section.



Concrete-filled hollow-section columns



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Connection Behaviour

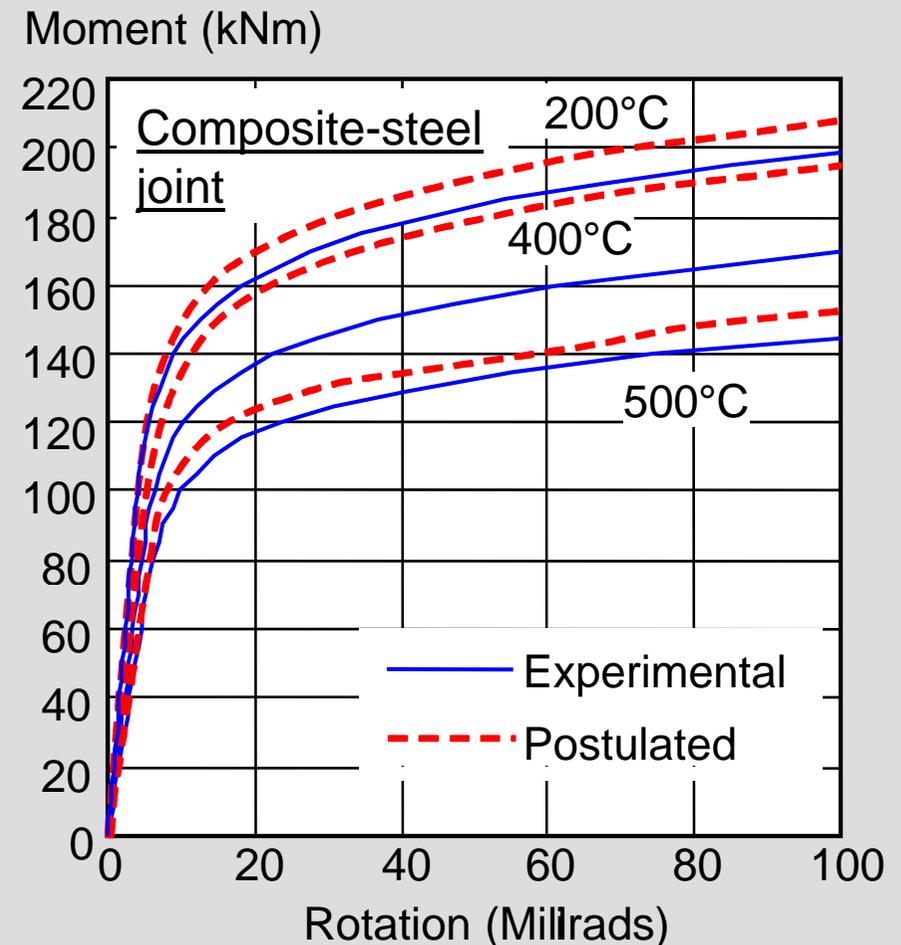
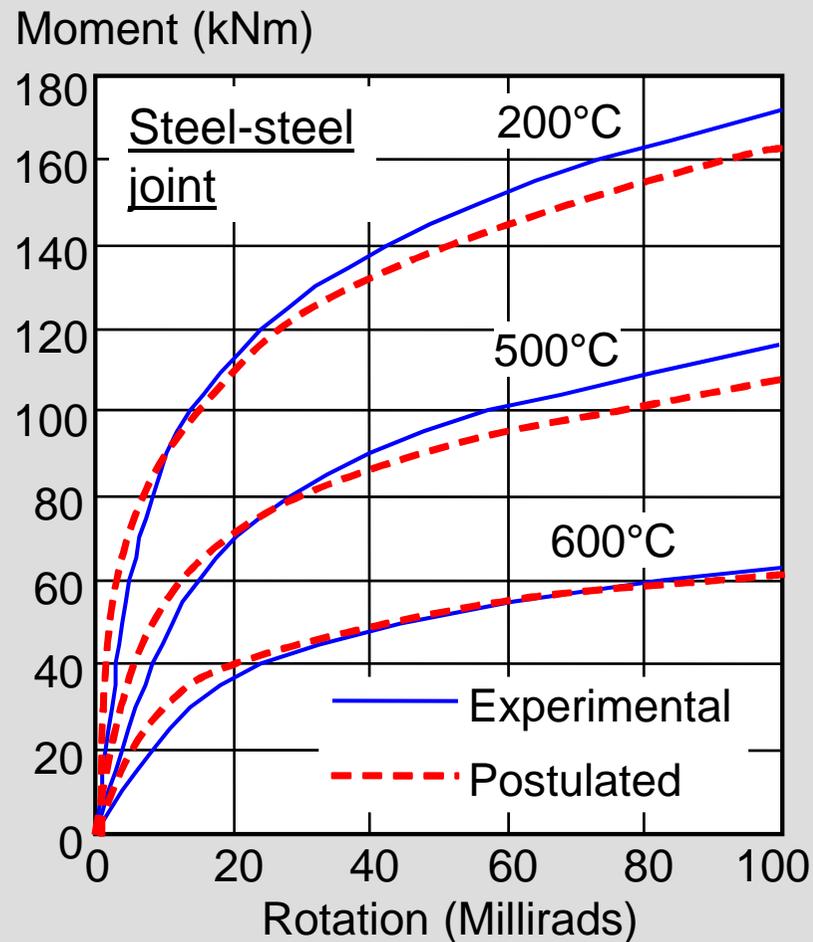
WG1: Data Sheet 7

**BEHAVIOUR OF STEEL AND COMPOSITE
JOINTS IN FIRE**



Moment-rotation at high temperature

- Cruciform tests from early 1990s
- Originally, joints being cooler than beams considered to be a design advantage for beams in fire
- Semi-empirical rules for $M-\phi$ by Al-Jabri (2004)

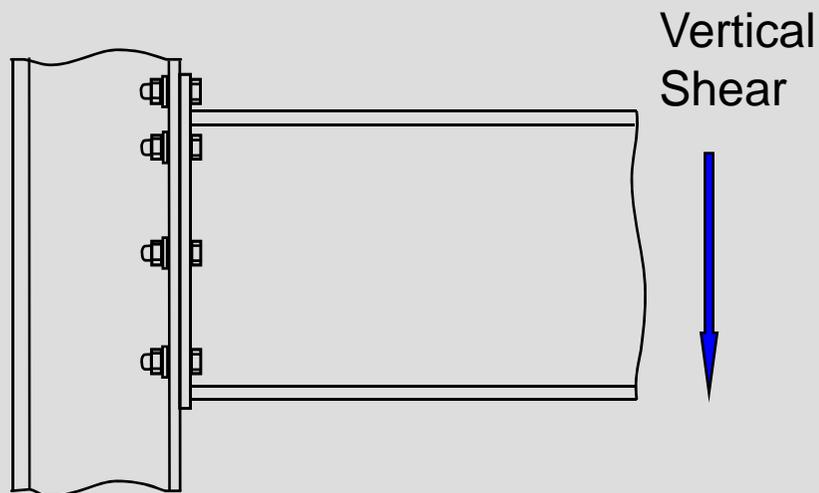




Behaviour in real buildings in fire

Observations from Cardington and other full-scale tests, and from accidental fires show:

- Buckling of lower flange of connected beam.
- Shear buckling in web of connected beam.
- Large beam deflections (high joint rotations).
- Some bolt fracture.



Ambient temperature:

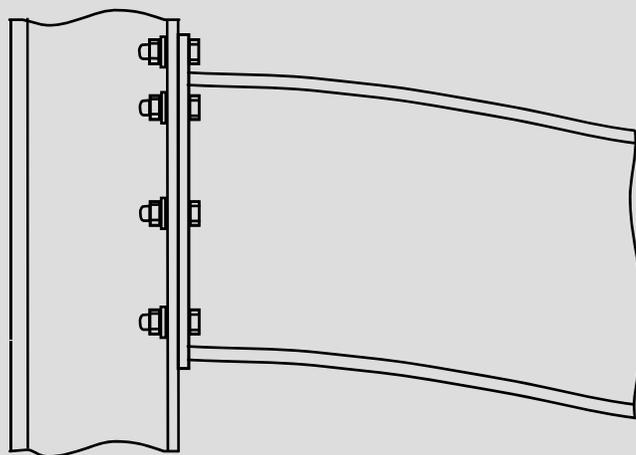
- Connection subjected mainly to vertical shear.



Behaviour in real buildings in fire

Observations from Cardington and other full-scale tests, and from accidental fires show:

- Buckling of lower flange of connected beam.
- Shear buckling in web of connected beam.
- Large beam deflections (high joint rotations).
- Some bolt fracture.



Vertical Shear



Hogging Moment

Restrained expansion

Initial heating stage:

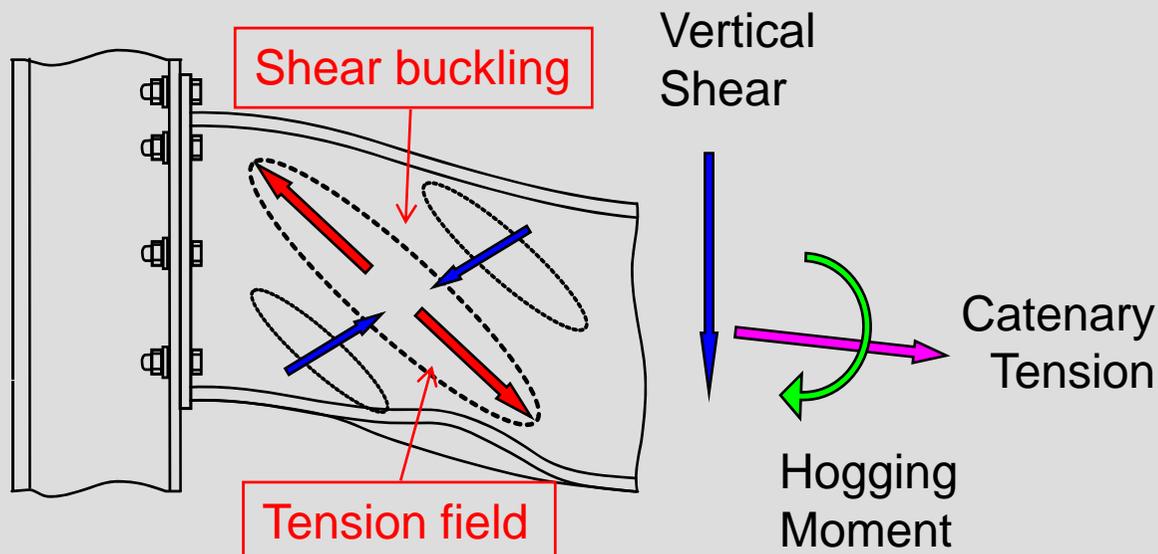
- Beam attempts to expand – columns and adjacent structure resist. Net compression caused.
- Thermal curvature generates rotation and hogging moments.



Behaviour in real buildings in fire

Observations from Cardington and other full-scale tests, and from accidental fires show:

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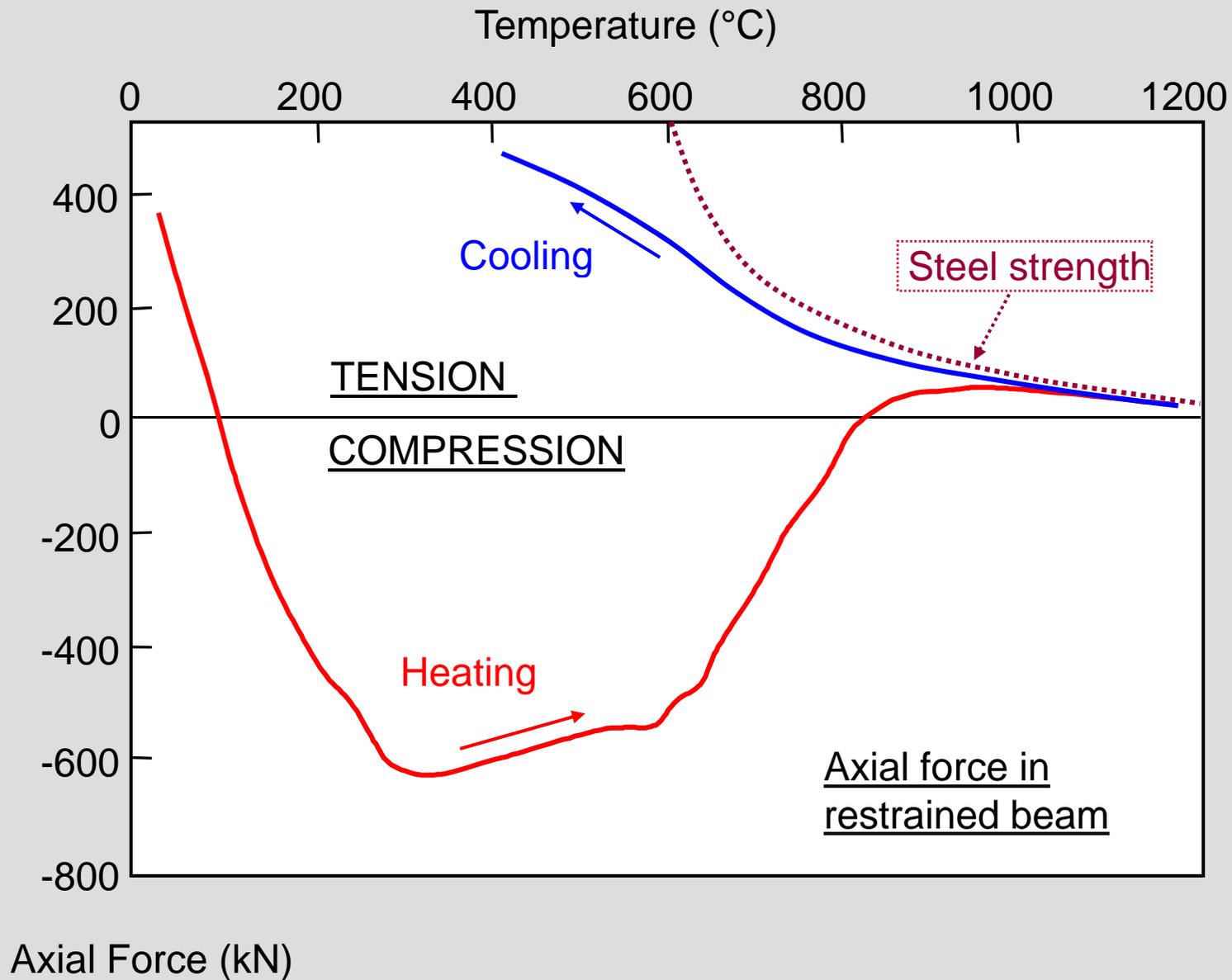


High beam temperature:

- Beam loses strength in bending – hangs in catenary. Joints have to resist catenary tension.
- Large hogging rotation caused locally by catenary action.

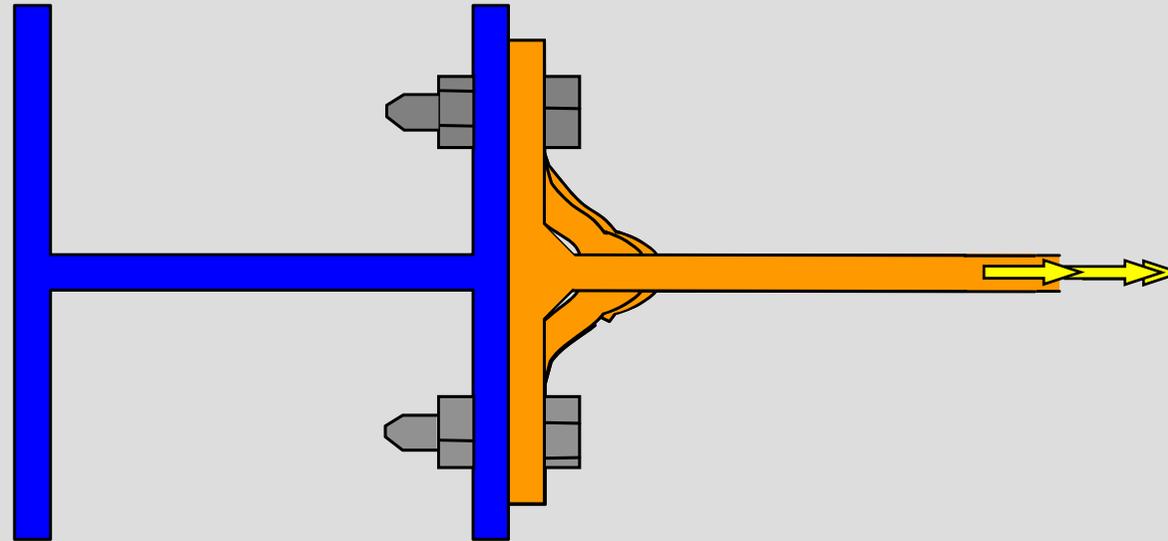


Axial force in steel downstand of composite beam

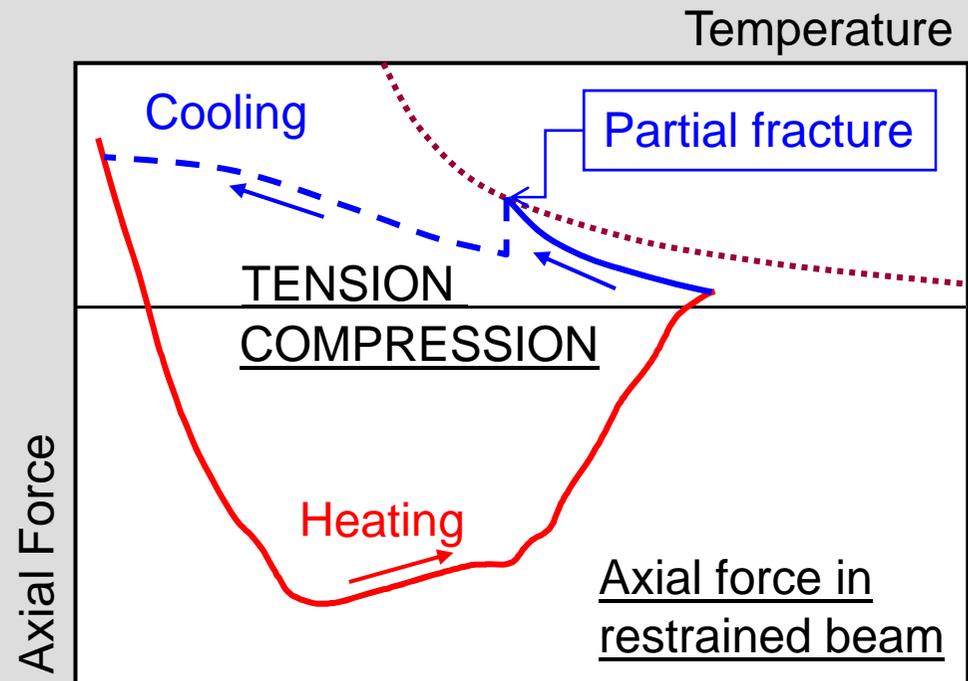




Fracture in cooling at Cardington

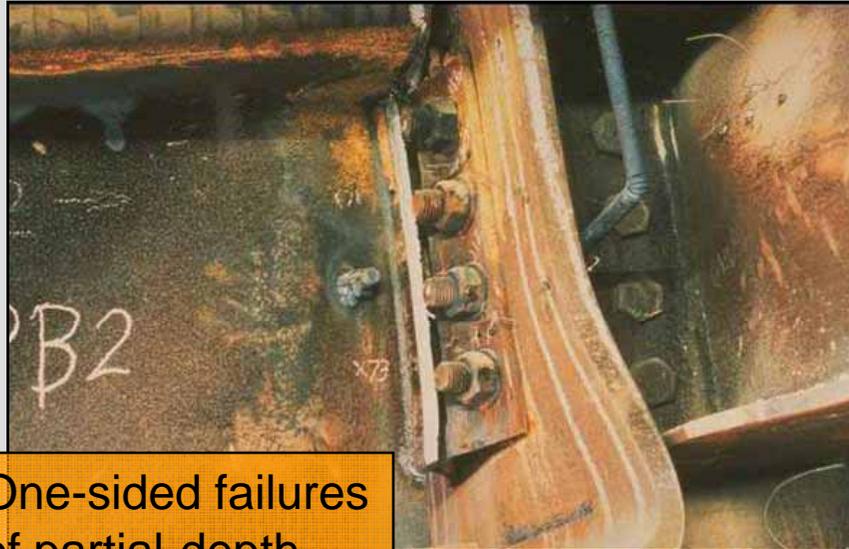


- One-sided failure of partial-depth end plates during cooling phase of fire.
- Reduced stiffness retains the integrity of the joint.
- Shear failure of bolts also observed in fin-plate beam-beam connections during cooling.





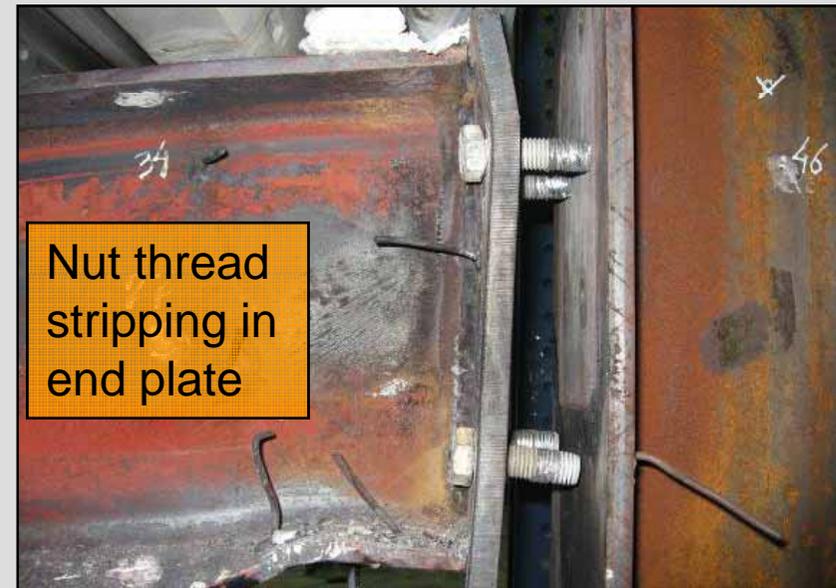
Joint failures in cooling



One-sided failures of partial-depth end plates



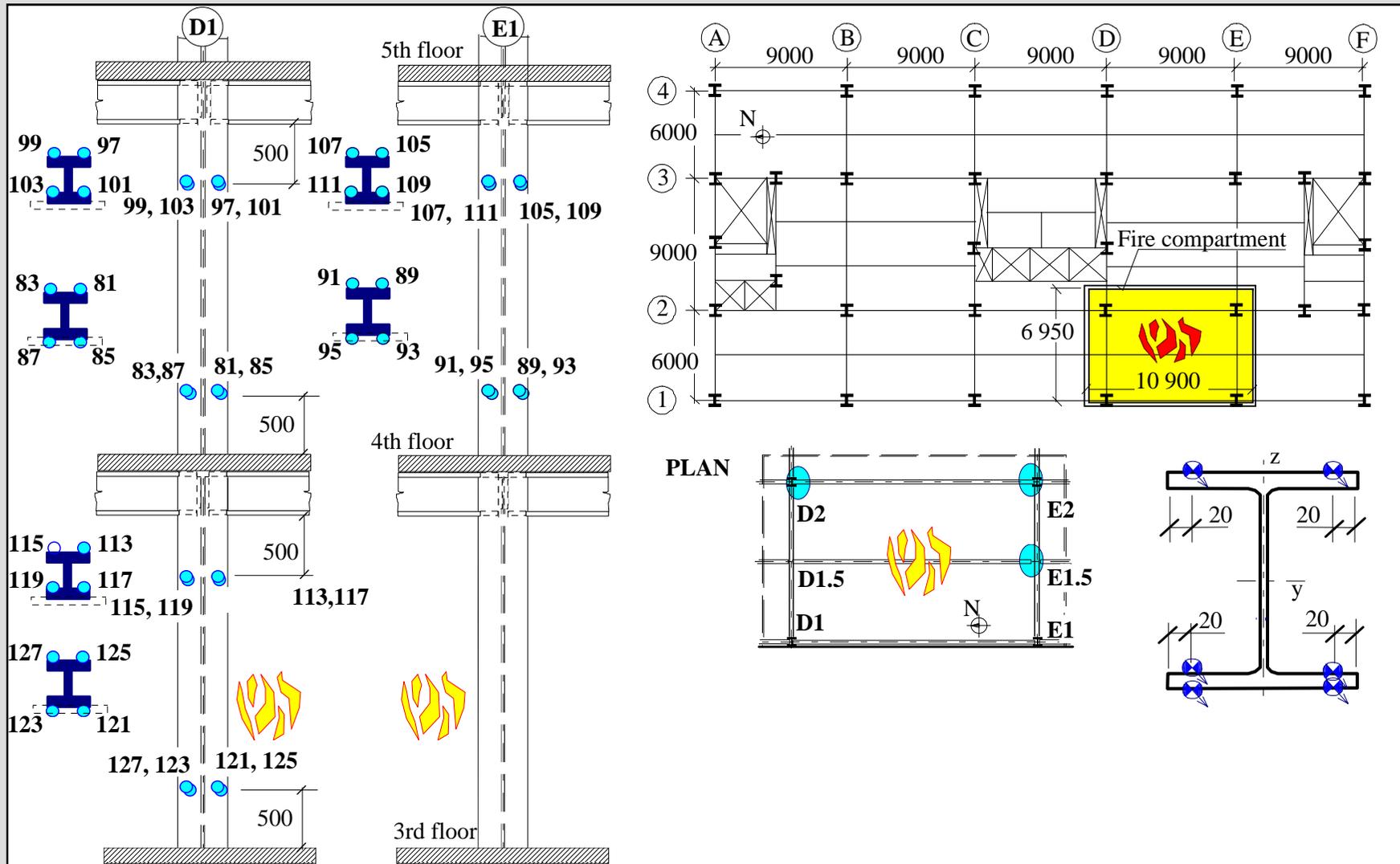
Bolt shear in fin plate



Nut thread stripping in end plate



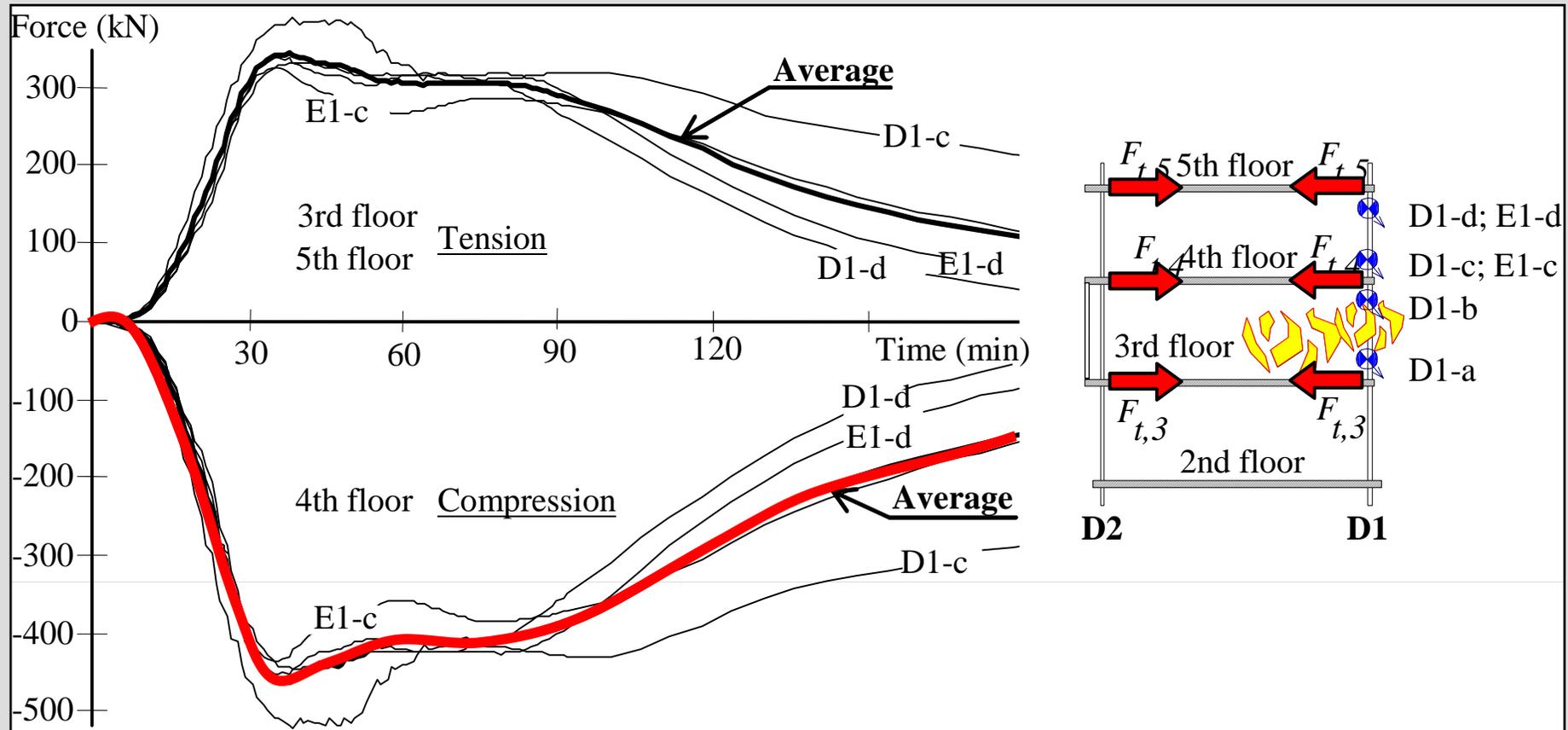
A research study of joint forces in fire



"Cardington 7" Wald et al. (2003)



Measured joint forces in natural fire



- General shape of compression curve is as usual.
- This is plotted in terms of time, not temperature – no reversal.
- In a particular natural fire curve the fire characteristics, load levels etc. determine whether the beam goes into tension



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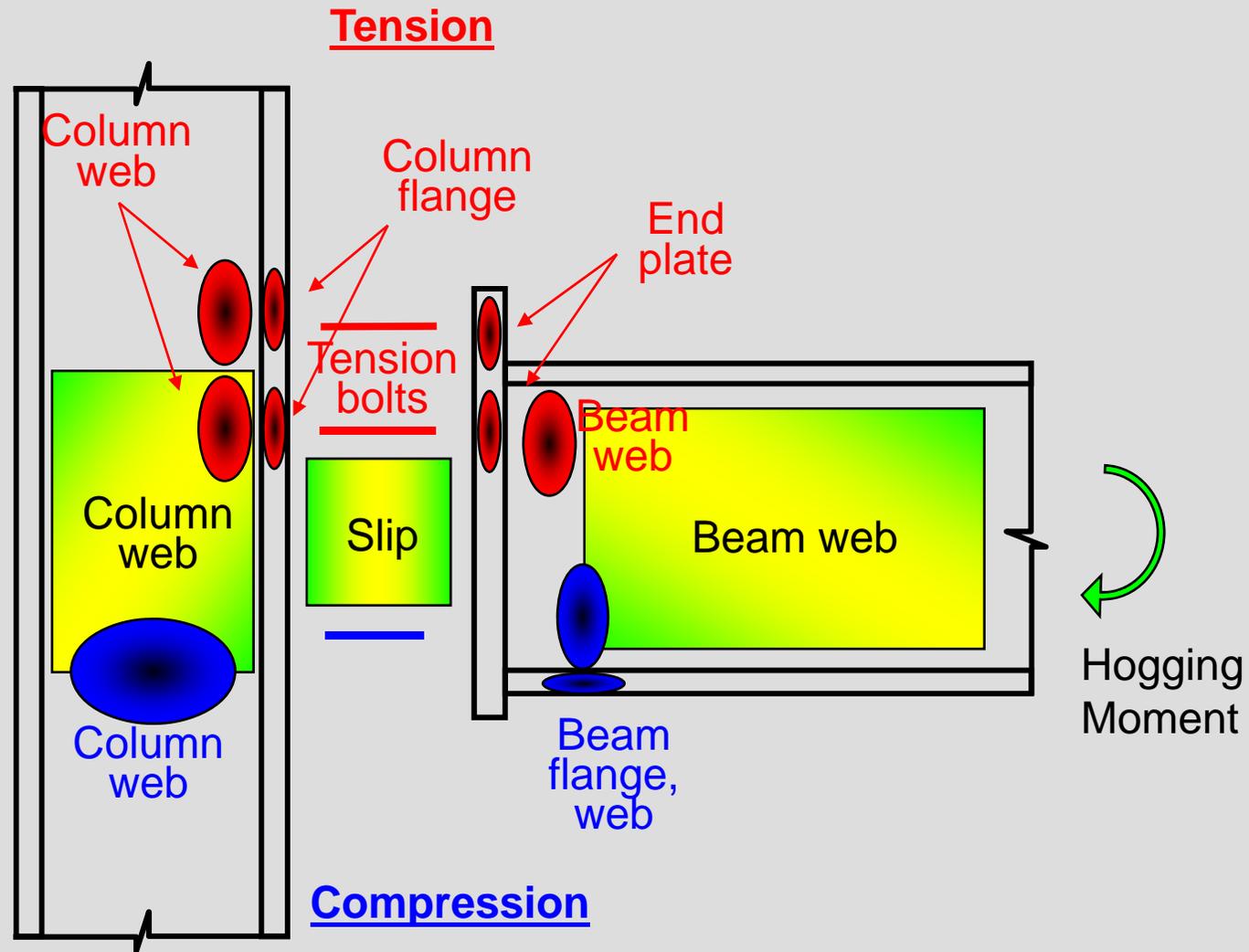
Component Approaches

WG1: Data Sheet 8

**COMPONENT-BASED APPROACHES TO STEEL
AND COMPOSITE JOINTS IN FIRE**

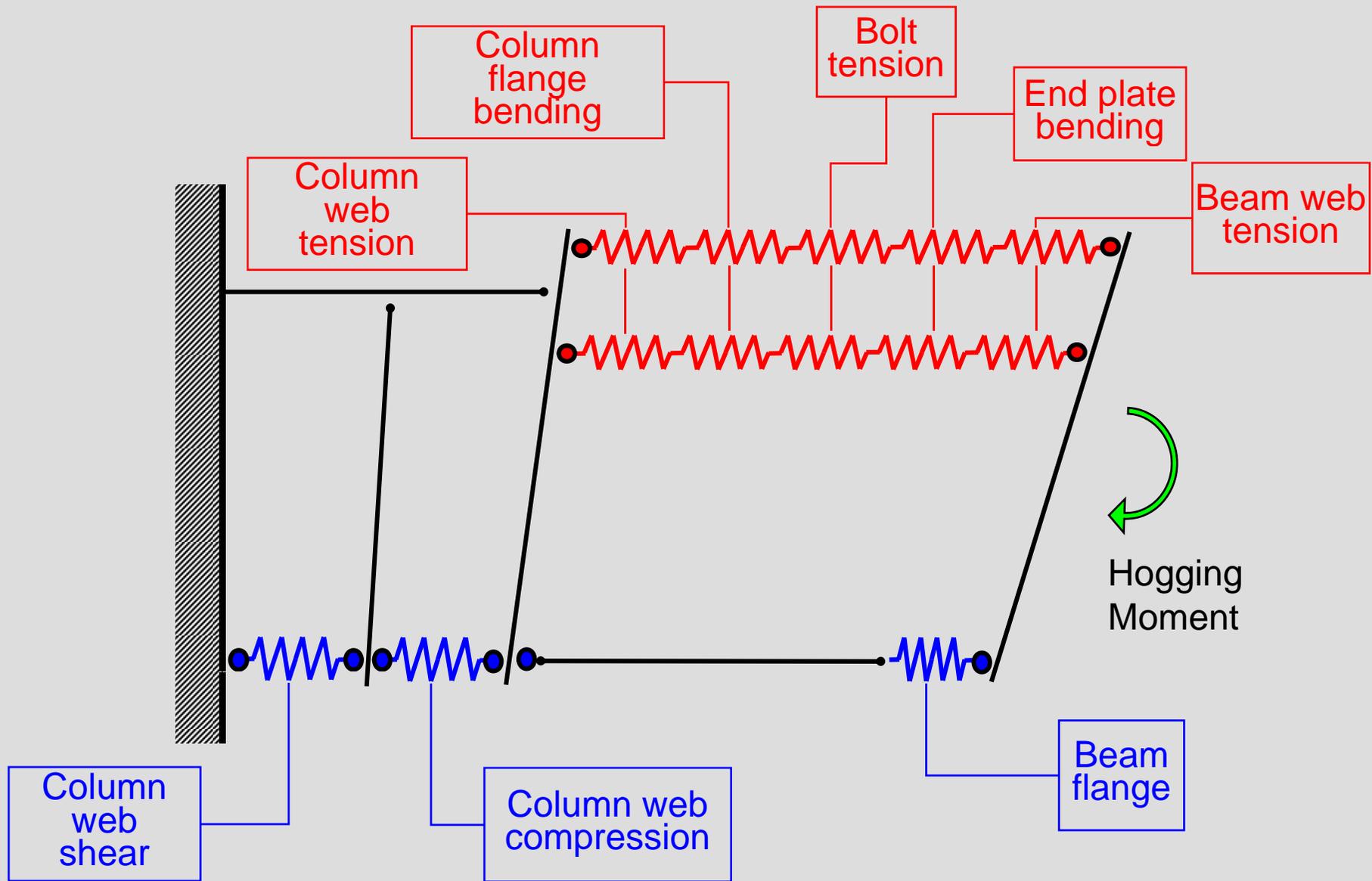


Principal component zones of end-plate





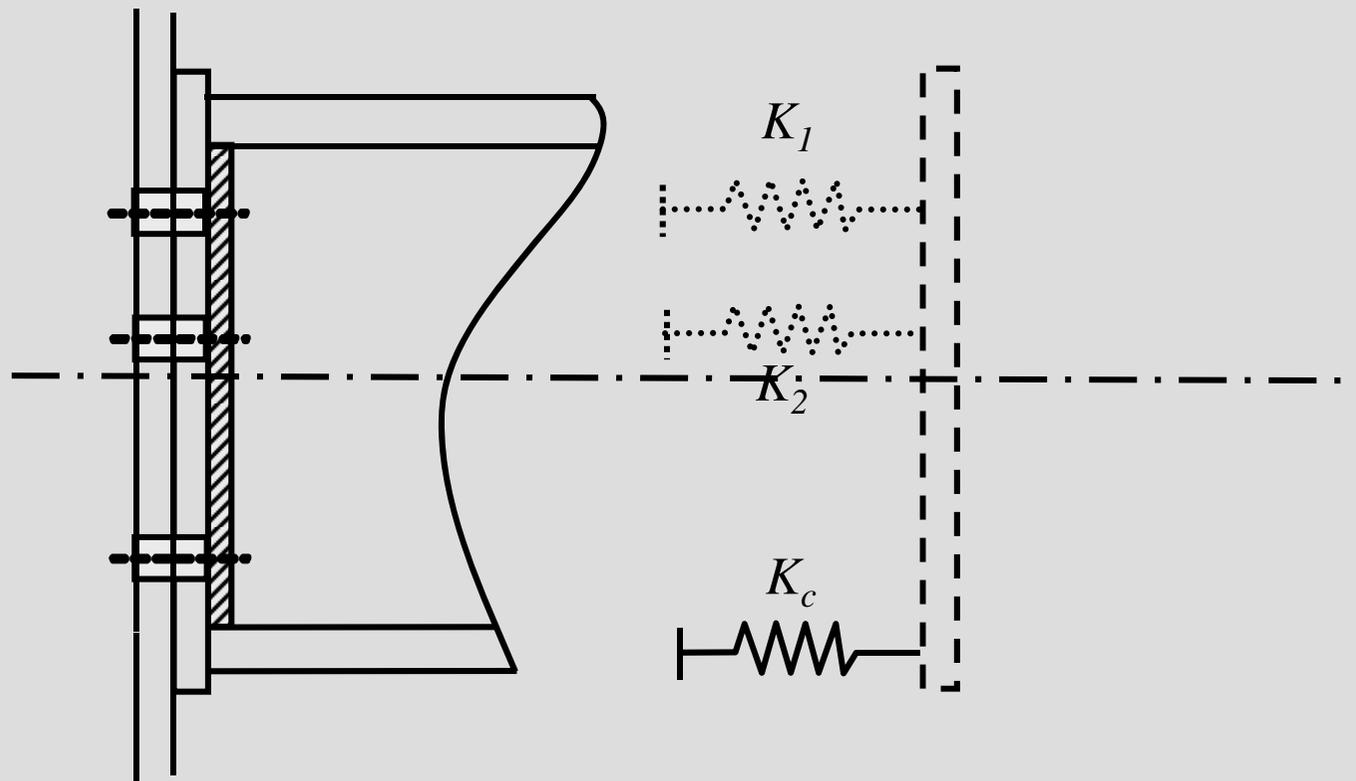
EC3-1.8 extended end-plate joint model





The “Component” method with axial force

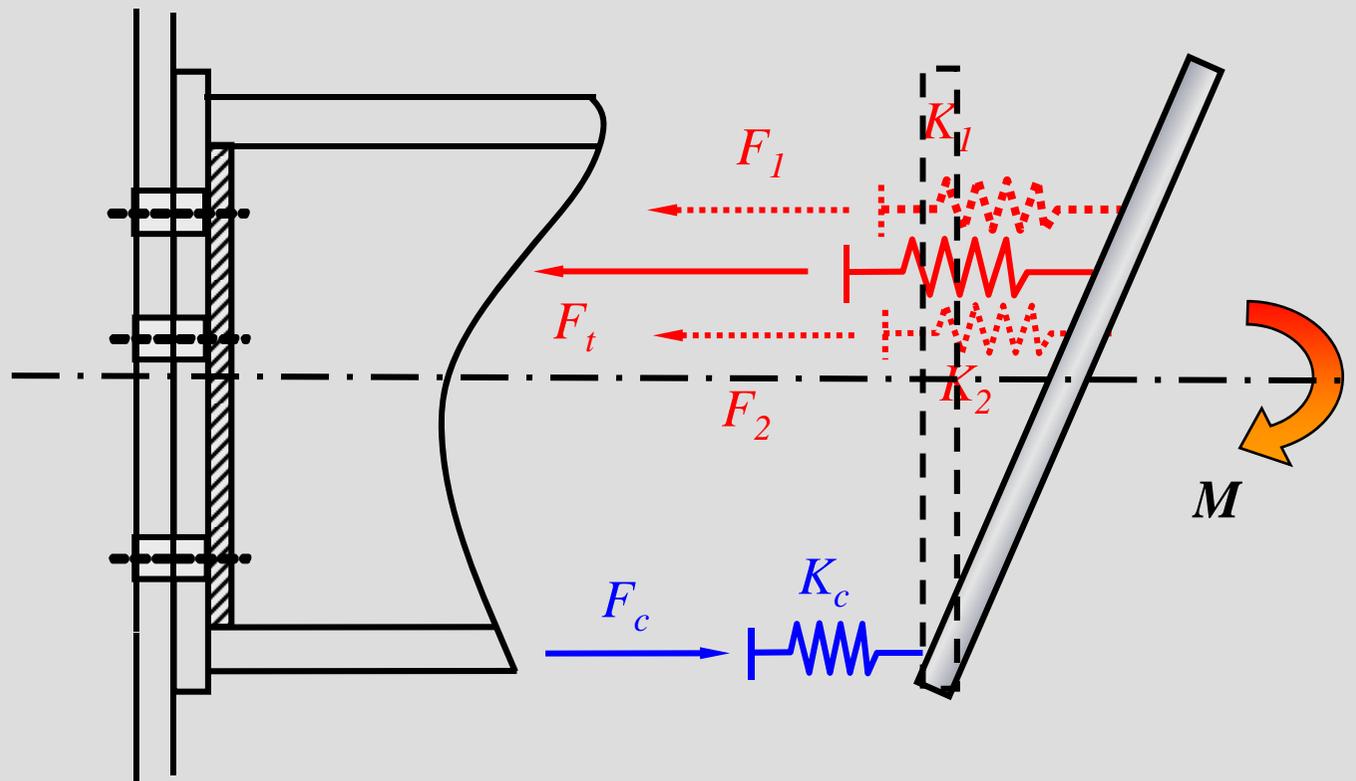
- Component model deals with load combinations automatically, though M- ϕ curves change due to thrust.





The “Component” method with axial force

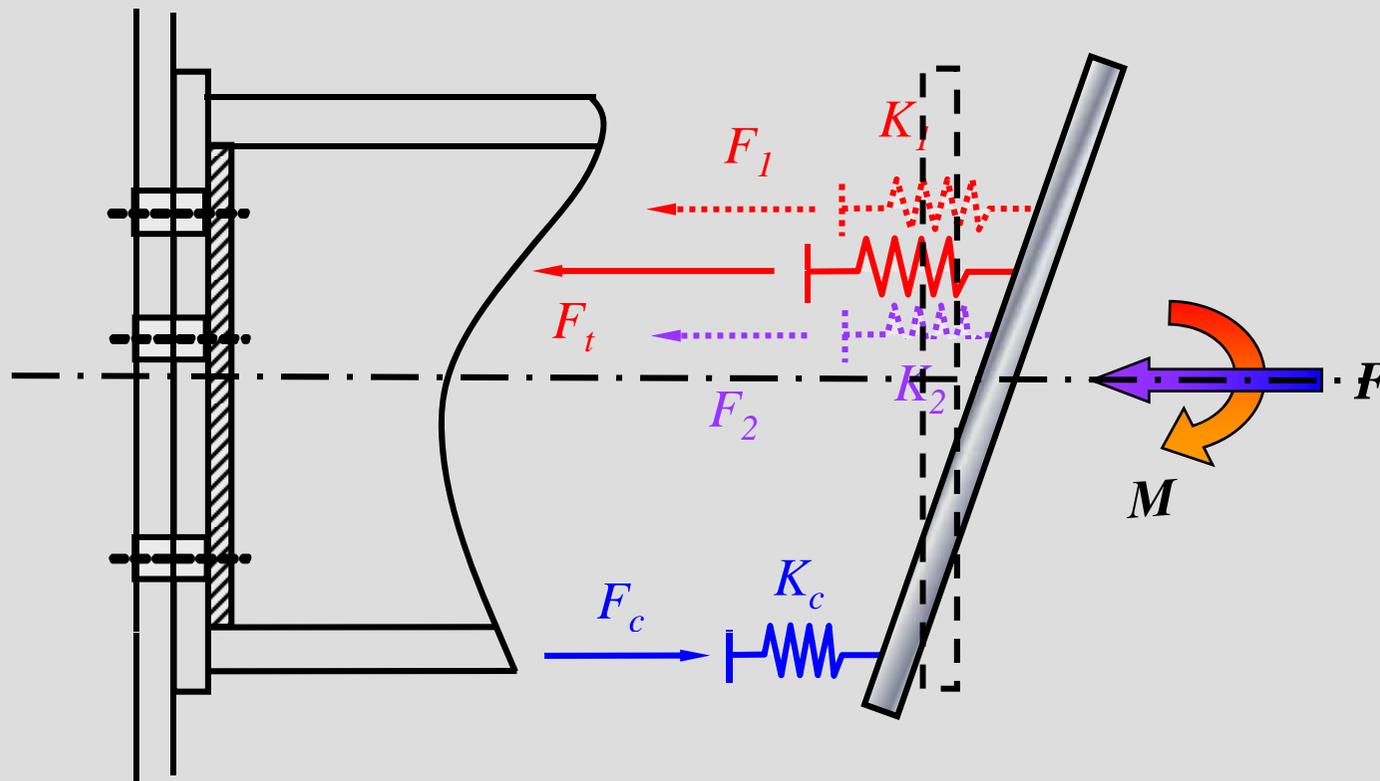
- Component model deals with load combinations automatically, though M- ϕ curves change due to thrust.





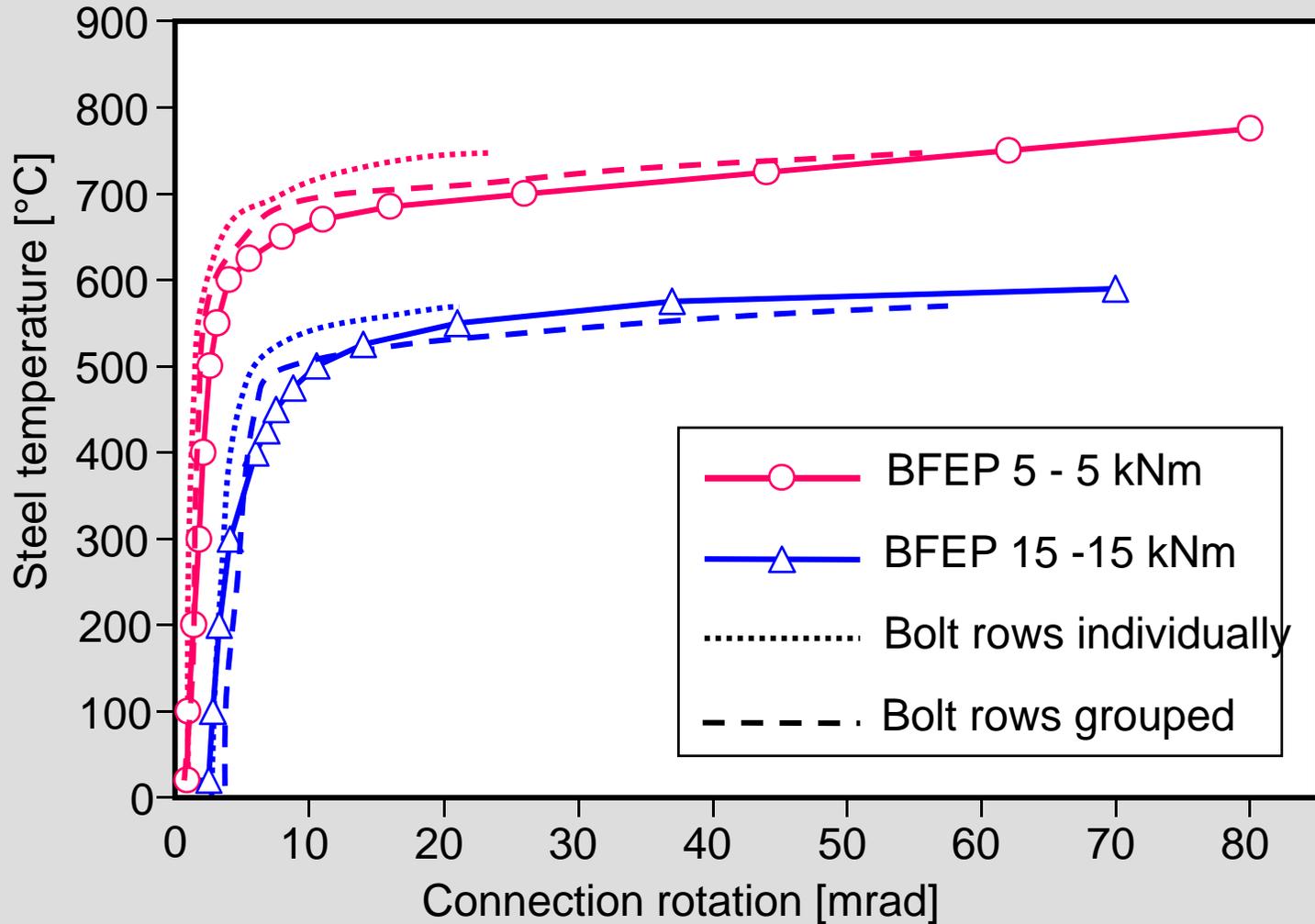
The “Component” method with axial force

- Component model deals with load combinations automatically, though $M-\phi$ curves change due to thrust.



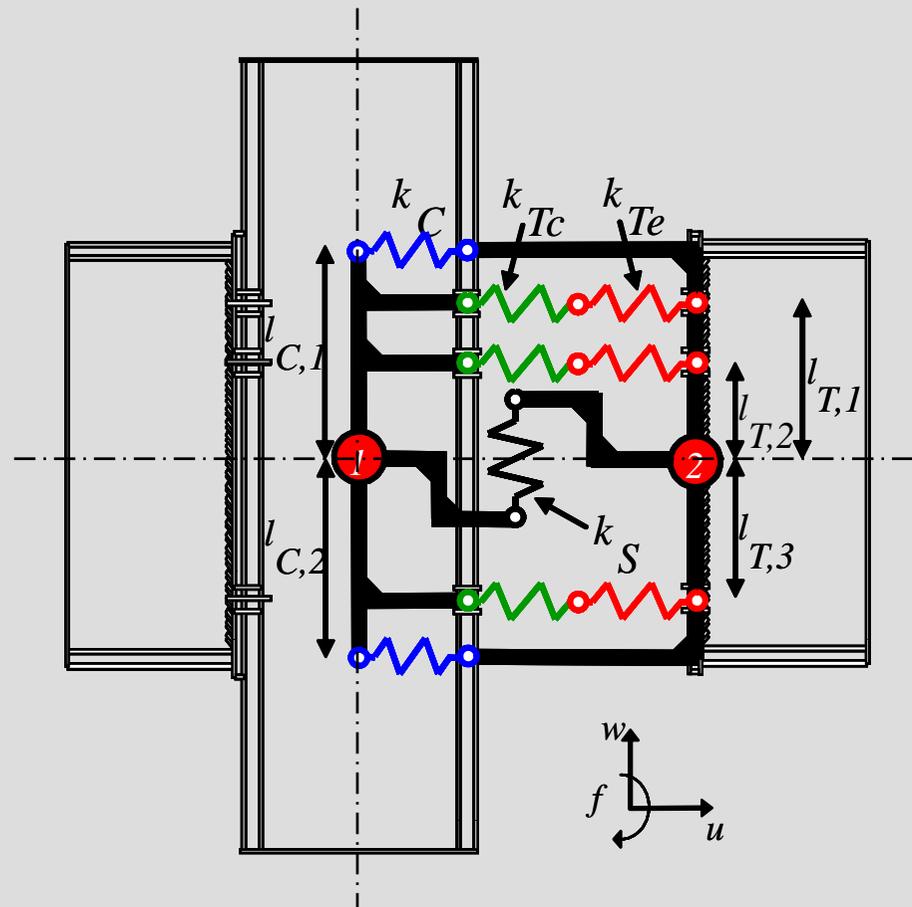


Comparison of joint element with $M-\phi-T$ tests by Leston-Jones





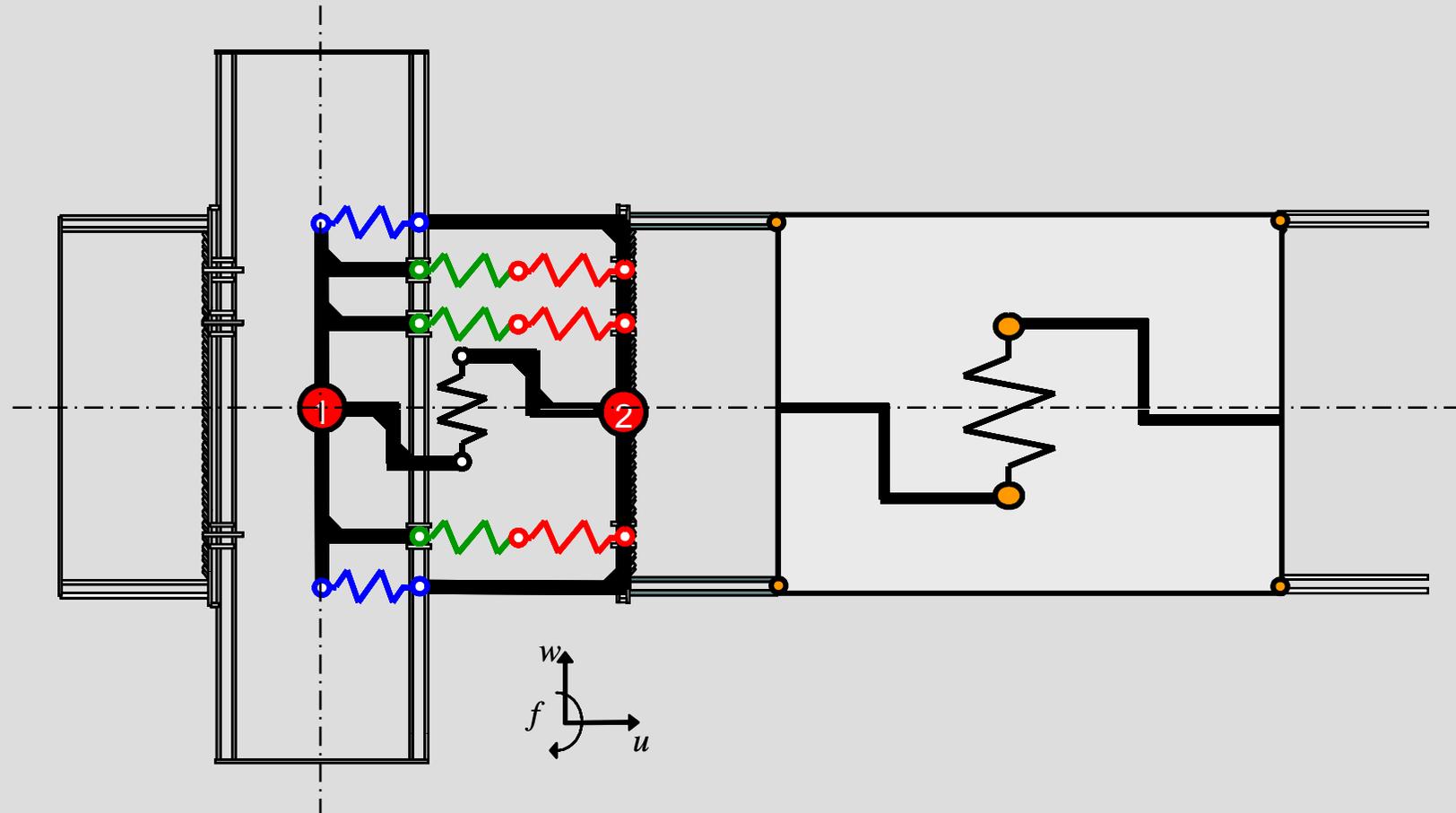
Component-Based Connection Element (Block)



-  Tension Spring –
-  T-Stub in End-Plate
-  Compression Spring
- Column Web
-  Shear Spring
- Bolts

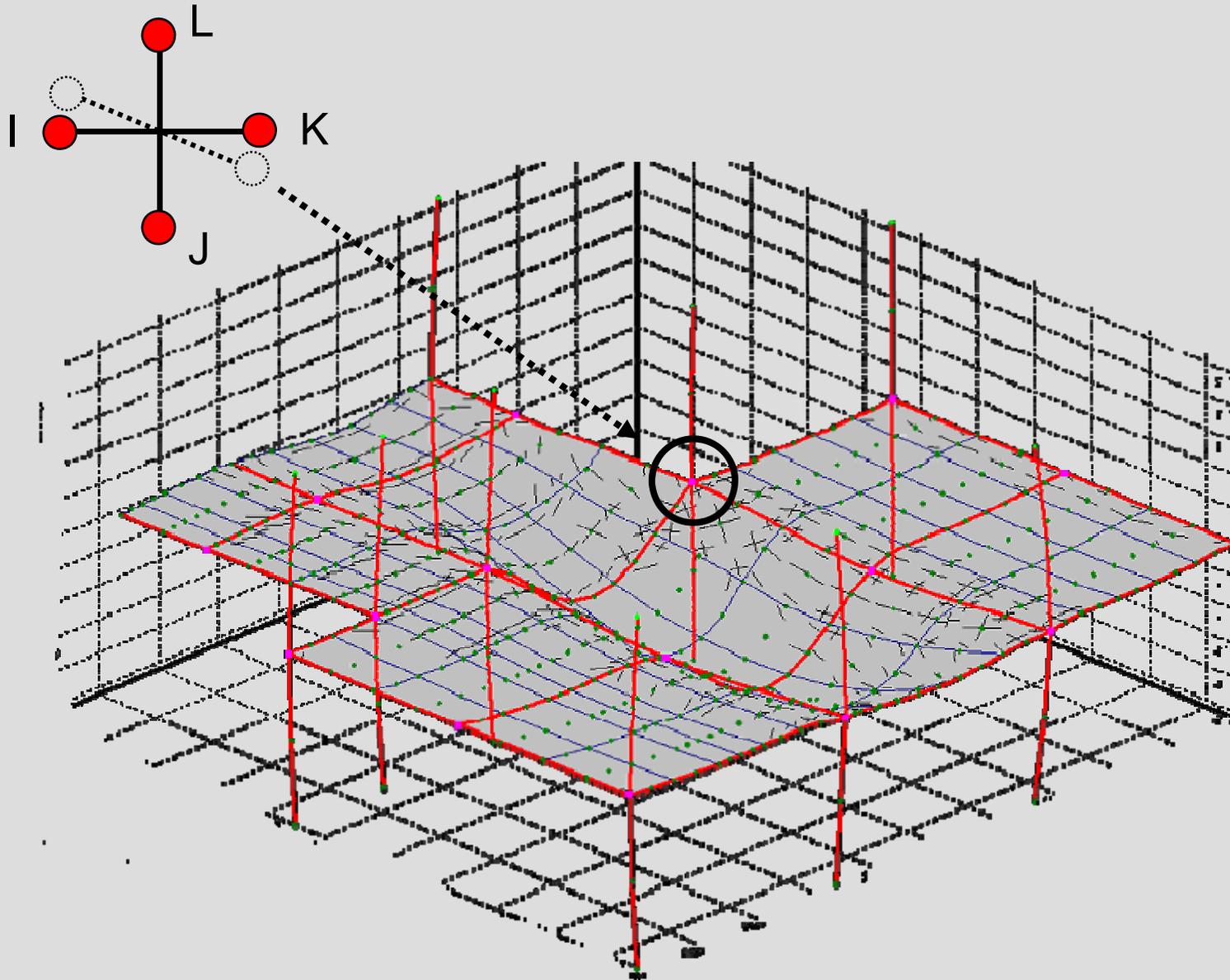


Component-based connection element: beam shear panel





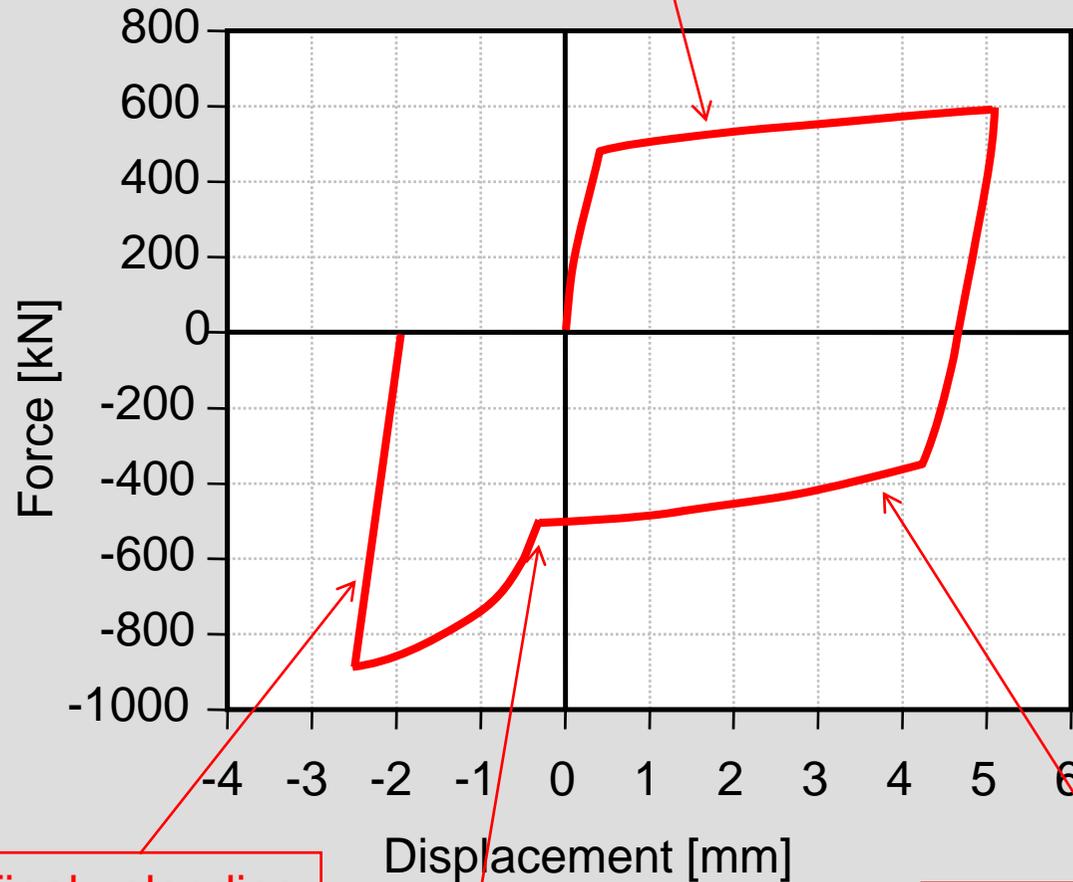
Implementation of joint element in software





How complex? Tension force on end plate

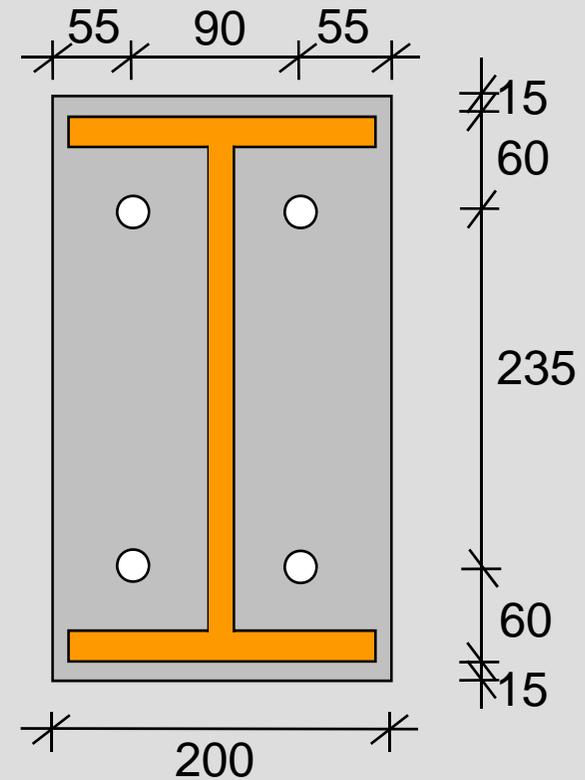
Loading (tension) below failure load



Final unloading

Plates in contact

Unloading (tension to compression)





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