# 2nd task: Two-way slab supported on 4 sides







### **Elements subjected to bending**





One-way slab – (1st task)



Two-way slab supported on 4 sides – **2nd task** 



Two-way flat slab – **3rd task** 



## Two-way slab supported on 4 sides

- The panel is given by the assignment
- Depth  $h_{\rm s}$  is given
- Calculate bending moments using linear analysis
- Calculate bending moments using precalculated tables based on the theory of plasticity
- For "plastic" moments, check  $h_{\rm S}$
- Calculate load of given supporting element (beam or wall)

### Introduction

- Elastic theory always applicable, but usually less fitting; no cracks in the structure
- **Plastic theory** closer to real behaviour of RC structures, but sufficient plastic hinge rotational capacity is necessary; the structure is cracked



### Introduction

 Plastic behaviour enables redistribution of internal forces => better utilization of material



- Less fitting, but very simple
- Good for **quick check** of bending moments calculated by more complex theories
- *Idea:* Deflection of the slab in both directions must be the same



- Calculate total design load of the slab  $f_{\rm d}$
- The load will be **divided in two directions**:

$$f_d = f_{d,x} + f_{d,y}$$

- We can model the behavior of the slab in each direction as one of the following beam types:
- **Fixed end** = continuity or outer edge with wall
- **Pinned end** (simply supported) = outer edge with beam
- Select the correct beam types for your structure



• As 
$$w_x = w_{y_x}$$
 we can say that:

$$k_x \cdot \frac{f_{d,x} l_x^4}{EI} = k_y \cdot \frac{f_{d,y} l_y^4}{EI}$$

- $E_x = E_y$  and  $I_x = I_y$  (in both directions, we consider that the cross-section is  $h_s*1$  m)
- After rearranging:

$$\frac{f_{d,x}}{f_{d,y}} = \frac{k_y}{k_x} \cdot \left(\frac{l_y}{l_x}\right)^4$$

• As 
$$f_d = f_{d,x} + f_{d,y}$$
, we can say that:  

$$\frac{f_{d,x}}{f_d - f_{d,x}} = \frac{k_y}{k_x} \cdot \left(\frac{l_y}{l_x}\right)^4$$

• And after rearranging, we receive **formulas for the loads** in *x* and *y* directions:



• Now we can calculate "linear" bending moments in the slab in each direction



# Assumptions for use of the tables based on the theory of plasticity

- Constant depth of the slab
- Rigid supports
- Corners prevented from lifting



- Approximately same load of adjacent panels
- Approximately same spans of adjacent panels
- Sufficient ductility of reinforcement (steel class B, C)
- Sufficient rotational capacity (x/d  $\leq$  0.25)

# **Plastic analysis**

Select the type of the panel



- Calculate ratio of spans
- Look up  $\beta$  coefficients in the table



!!! For all panel types,  $l_x$  is the <u>shorter</u> span

Fixed end

mym

mvm

хет

 $\rightarrow \vee$ 

Pinned end

...etc.

Support condition	Factor	Coefficients β <sub>&amp;e</sub> , β <sub>×m</sub> , β <sub>νe</sub> , β <sub>νm</sub> , for <mark> </mark> <sub>ν</sub> /l <sub>×</sub> =							
		1,0	1,1	1,2	1,3	1,4	1,5	1,75	≥2,0
y m xe m xm m ye m ym y	β <sub>‰</sub>	-0,031	-0,037	-0,042	-0,046	-0,050	-0,053	-0,059	-0,063
	β <sub>×π</sub>	0,024	0,028	0,032	0,035	0,037	0,040	0,044	0,048
	β <sub>γe</sub>	-0,032							-0,032
	β <sub>ym</sub>	0,024							0,024
^									

# **Plastic analysis**

- Use linear interpolation to calculate  $\beta$  coefficients
- $\beta_y$  coefficients are constant for all values of  $l_y/l_x$
- Be careful when selecting the type of the panel:



# **Plastic analysis**

• Calculation of bending moments

$$m_{\rm xe} = \beta_{\rm xe} m_0$$
$$m_{\rm xm} = \beta_{\rm xm} m_0$$

$$m_{\rm ye} = \beta_{\rm ye} m_0$$

$$m_{\rm ym} = \beta_{\rm ym} m_0$$
$$m_0 = f_{\rm d} \cdot l_{\rm x}^2$$

!!! Be careful about directions –  $m_x$  is the moment in the direction of  $l_x$ , the same applies to  $\gamma$  index.

Basic value of bending moment, constant for all moments!!!

- Indices:
  - x, y direction of a moment
  - m midspan moment
  - e support moment





# **Design of bending reinforcement**

- In the homework, you DO NOT HAVE TO design the reinforcement
- BUT remember, that the procedure of design of bending reinforcement for two-way slabs is IDENTICAL to beams (see 3rd seminar)
- You should use the plastic moments for design of reinforcement (closer to real behaviour of RC structure)
- The only difference is that you design the reinforcement in 2 directions and that the width of the cross-section is taken as b = 1 m

# Check of *h*<sub>s</sub>

- Check the given value of h<sub>s</sub> for the biggest moment from **plastic** analysis (m<sub>Ed,max</sub>)
- Calculate the required cross-sectional area of reinforcement:

$$a_{s,rqd} = \frac{m_{Ed,\max}}{0.9df_{yd}}$$

Calculation of effective depth – see 3rd seminar.

Estimate 10 mm rebars and take cover depth from the frame structure

• Estimate the depth of the compressed zone:

Estimation of  

$$a_{s,prov}$$
 $x = \frac{1.2a_{s,rgd}f_{yd}}{0.8bf_{cd}}$ 
For slabs, you generally consider 1 m  
wide strip => b = 1000 mm

# Check of *h*<sub>s</sub>

- Check the span/depth ratio (deflection control) see 1st seminar
- If:
  - 1.  $a_{s,rqd} \ge a_{s,min}$  (calculation of  $a_{s,min}$  see 3rd seminar) 2.  $\xi = \frac{x}{d} \le 0.25$

3. Span to depth ratio is checked then the original  $h_s$  is **correct.** 

 If some of the conditions are not checked, propose a solution (just describe it, don't calculate anything)

## Load of beam/wall

- Draw tributary areas of all the supporting elements
- The angle between identical supports (fixed/fixed, pinned/pinned) is **45**°
- Between fixed and pinned, **60**° go to fixed
- **Calculate the load** of one given supporting element (wall or beam)



# Load of beam/wall

- For your given element, draw load diagram (with values, not just the shape!)
- The load in each point is: total load of the slab  $(f_d)$  \* width of the tributary area



 Be careful – inner walls and beams are loaded by 2 adjacent panels!