



decivil universidade de aveiro
departamento de engenharia civil

EN 1993-1-2: FLEXURAL BUCKLING RESISTANCE OF STAINLESS STEEL COLUMNS IN CASE OF FIRE

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LABEST - Universidade de Aveiro



EN1993-1-2 fire resistance formulae

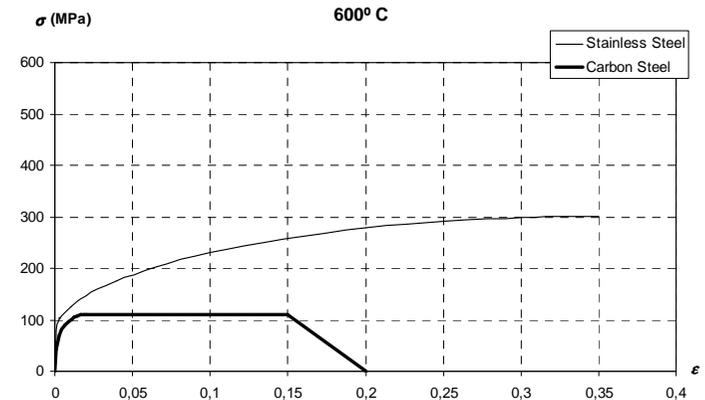
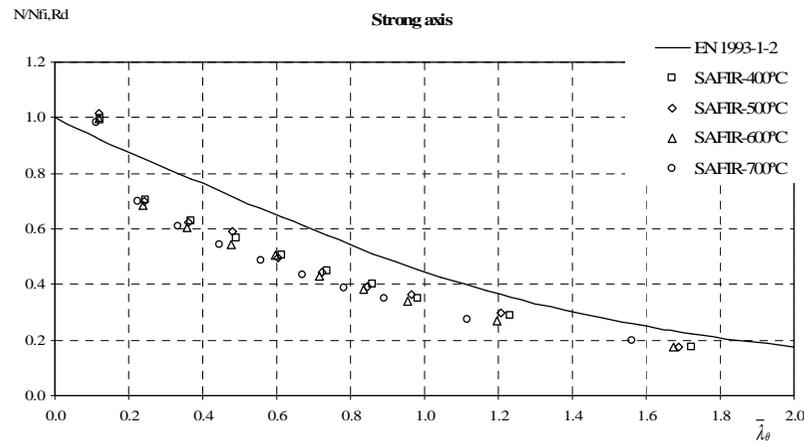


Same formulae developed for carbon steel columns



$$N_{b,fi,t,Rd} = \chi_{\min,fi} A k_{y,\theta} \frac{f_y}{\gamma_{M,fi}}$$

$$\chi_{i,fi} = \frac{1}{\phi_{i,\theta} + \sqrt{\phi_{i,\theta}^2 - \bar{\lambda}_{i,\theta}^2}} \quad \text{with} \quad \chi_{i,fi} \leq 1$$



$$\phi_{i,\theta} = \frac{1}{2} \left(1 + \alpha \bar{\lambda}_{i,\theta} + \bar{\lambda}_{i,\theta}^2 \right)$$

$$\alpha = 0.65 \sqrt{235 / f_y}$$



New proposal



Developed for stainless steel Class 1 and 2 I-sections

**“full”
proposal**

$$\chi_{fi} = \frac{1}{\phi_{\theta} + \sqrt{\phi_{\theta}^2 - \beta \bar{\lambda}_{\theta}^2}}$$

$$\phi_{\theta} = \frac{1}{2} \left[1 + \alpha \bar{\lambda}_{\theta} + \beta \bar{\lambda}_{\theta}^2 \right]$$

	β
Strong axis	1.0
Weak axis	1.5

$$\alpha = \eta \sqrt{\frac{235}{f_y} \frac{E}{210000} \sqrt{\frac{k_{E,\theta}}{k_{y,\theta}}}}$$

	1.4301, 1.4401, 1.4404,	1.4462
η	1.3	0.9



**Simplified
proposal**

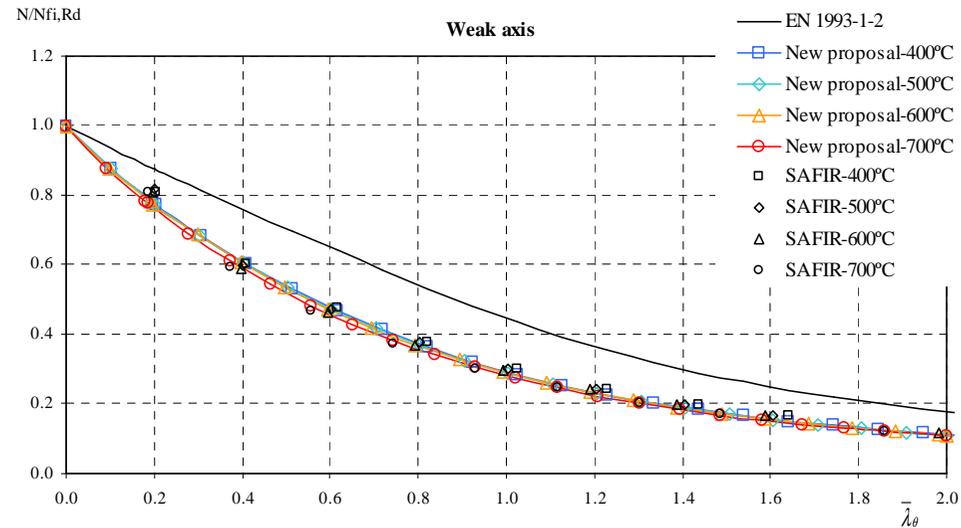
$$\alpha = \beta \sqrt{235/f_y}$$

	Carbon Steel	Stainless Steel
β	0.65	1.5

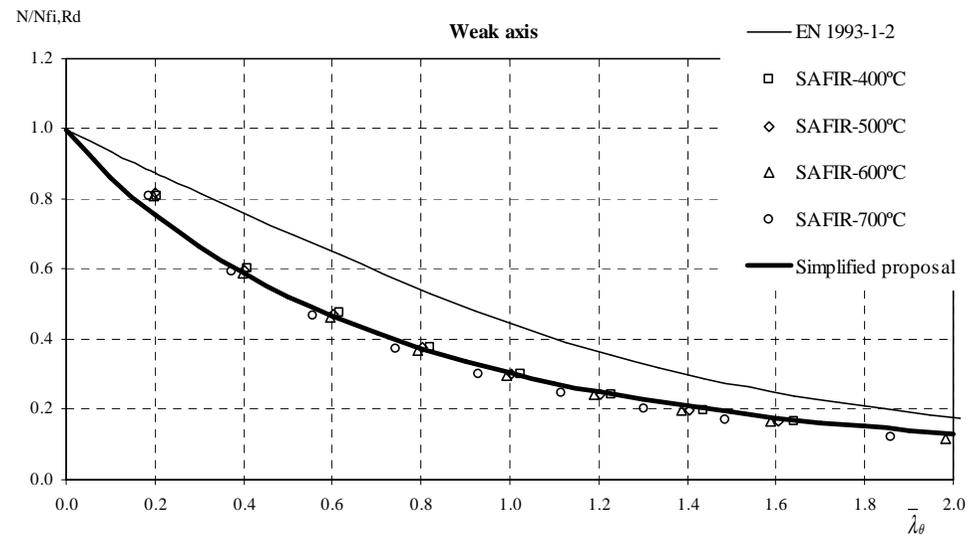
Lopes, N.; Vila Real, P.; Simões da Silva, L.; Franssen, J.-M. “Axially loaded stainless steel columns in case of fire”, Journal of Structural Fire Engineering, Multi-Science Publishing Co. Ltd, volume 1/1, pp 43-59, ISSN 2040-2317, March of 2010.



Validation

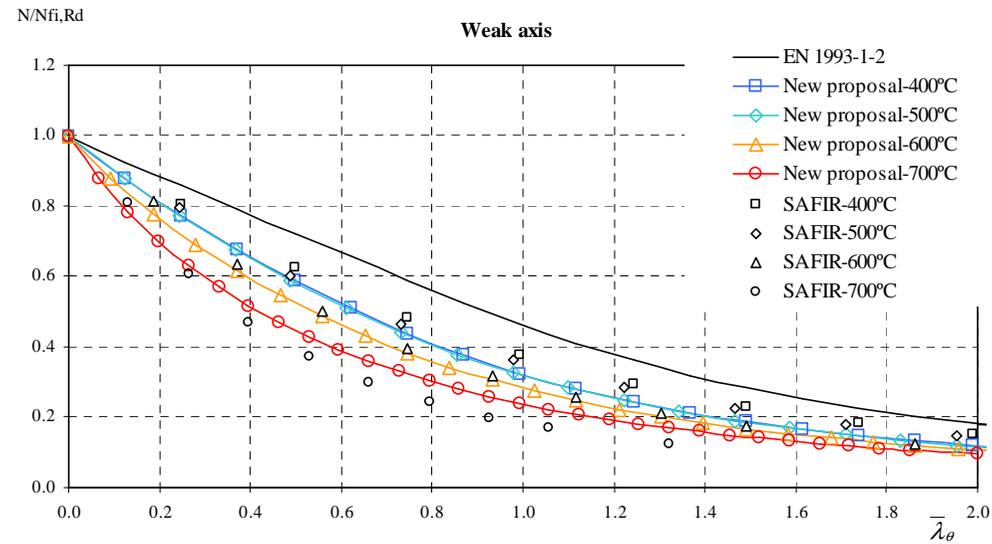


HEB200 1.4301

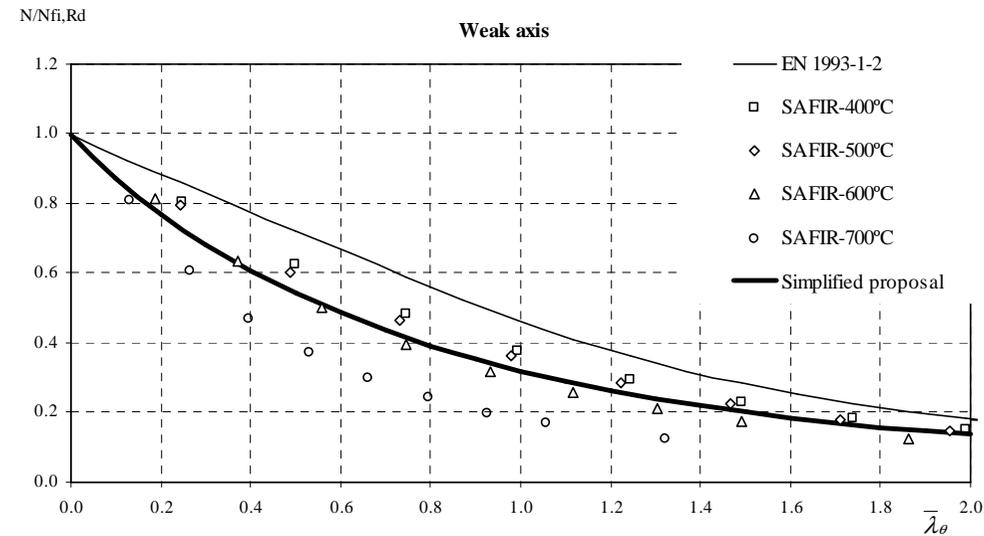




Validation



HEB200 1.4003

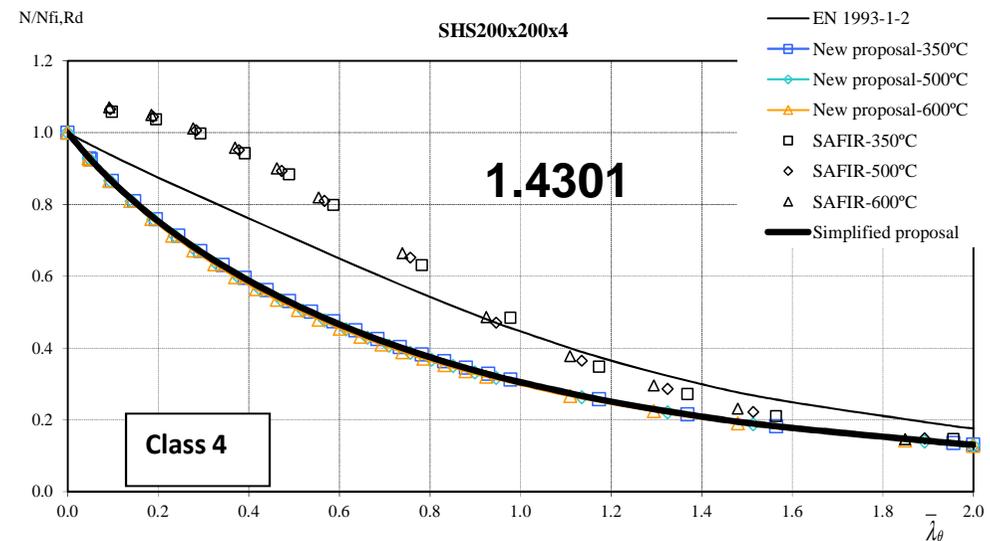
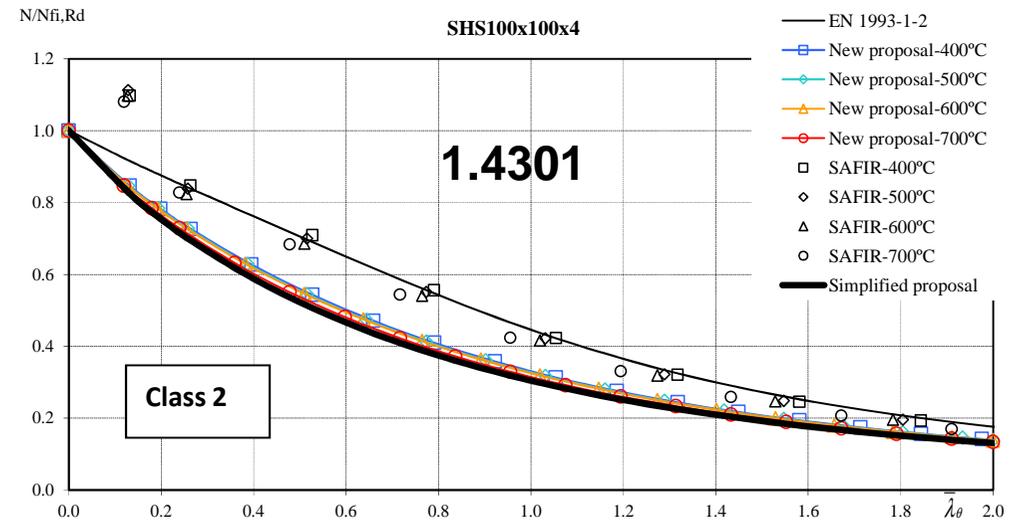




Future developments



- Square hollow sections (SHS)
- Class 4 sections
 - SHS
 - I-shaped





Integrated Fire Engineering and Response Meeting - 20-21 February 2014 Krakow



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Thank you for your attention

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