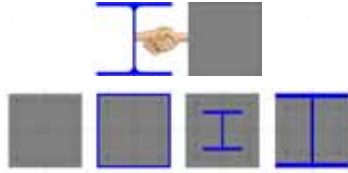




“St. CIRIL and METHODIUS” UNIVERSITY
FACULTY OF CIVIL ENGINEERING
SKOPJE - MACEDONIA



JOVANOSKA MILICA, CVETKOVSKA MERI

THE INFLUENCE OF CROSS-SECTION SHAPE ON FIRE RESISTANCE OF COMPOSITE CONCRETE-STEEL COLUMNS

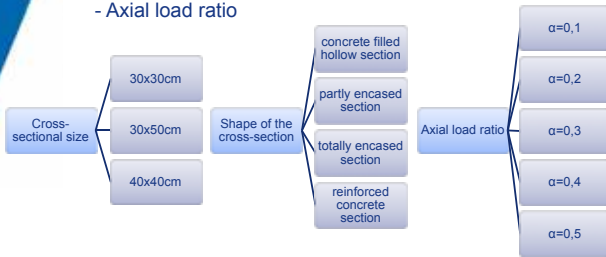
STUDY CASE. INPUT PARAMETERS



- Column length: $L=3m$
- Support condition: pinned-fixed
- Load case: centrally loaded
- Concrete compressive strength $f_c(20^\circ C)=30Mpa$
- Steel profile yielding strength $f_y=400Mpa$
- Reinforcement yielding strength $f_{yh}=400Mpa$
- All sides exposed to fire

VARIABLES CONSIDERED IN THE STUDY

- Shape of the cross section
- Cross sectional size
- Axial load ratio

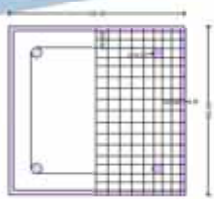


COMPUTER PROGRAM FIRE

Module FIRE-T: Nonlinear transient heat flow
Module FIRE-S: Nonlinear stress-strain response associated with fire

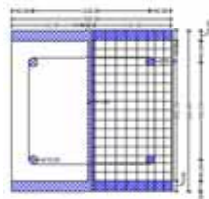
- Thermal expansion
- Shrinkage
- Creep
- Cracking, crushing
- Temperature dependent material properties are considered
- The spalling is not taken into account
- Two dimensional heat transfer is assumed
- Fire is modeled by a single valued gas temperature history, according to ISO 834
- No contact resistance to heat transmission at the interface between the steel and concrete occurs
- The easier heat penetration because of cracks and crush, is neglected
- Buckling and geometrical imperfections are not taken into account

CONCRETE FILLED HOLLOW SECTION CFH30



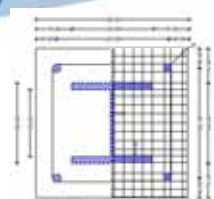
Rectangular Hollow Section 300.300.8
Reinforcement $4\phi 18$
 $N_u=6533kN$

PARTLY ENCASED SECTION PE30



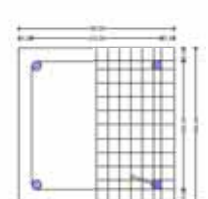
HE300B
($b=300, h=300, d=19, t=11mm$)
Reinforcement $4\phi 16$
 $N_u=8276kN$

TOTALLY ENCASED SECTION TE30



HE160
($b=160, h=160, d=8, t=13mm$)
Reinforcement $4\phi 16$
 $N_u=5931kN$

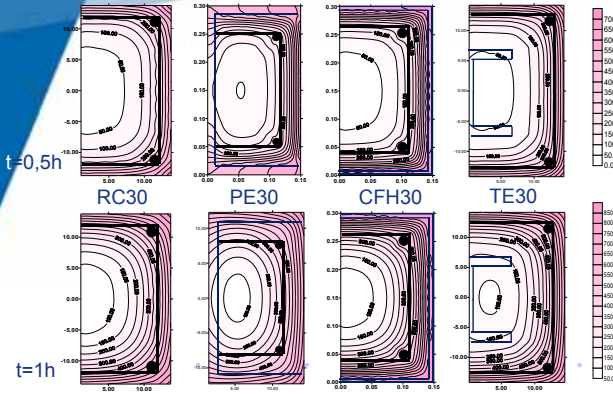
REINFORCED CONCRETE SECTION RC30



Cross sectional size $30 \times 30cm$
Reinforcement $4\phi 18$
 $N_u=3077kN$

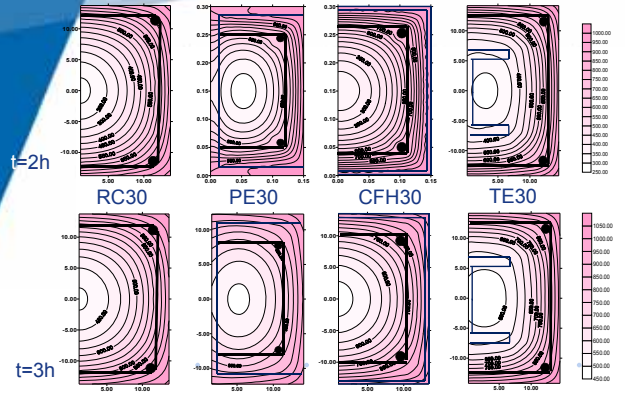
COMPUTER PROGRAM FIRE

Isotherms in the cross section



COMPUTER PROGRAM FIRE

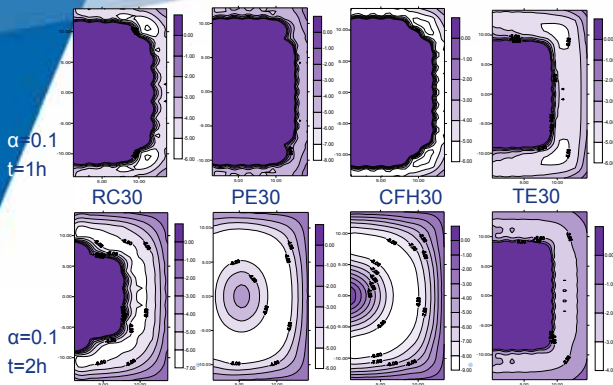
Isotherms in the cross section



COMPUTER PROGRAM FIRE

Isobars in the cross section

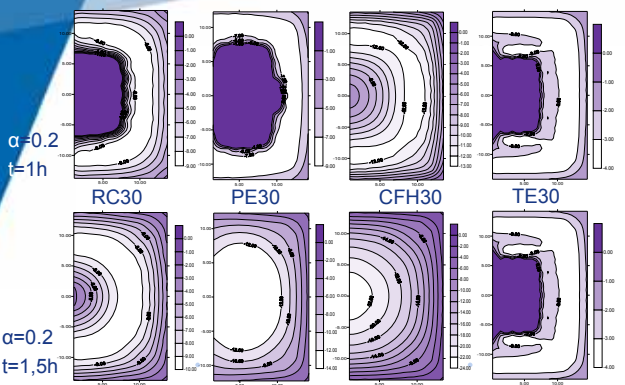
■ -cracked concrete



COMPUTER PROGRAM FIRE

Isobars in the cross section

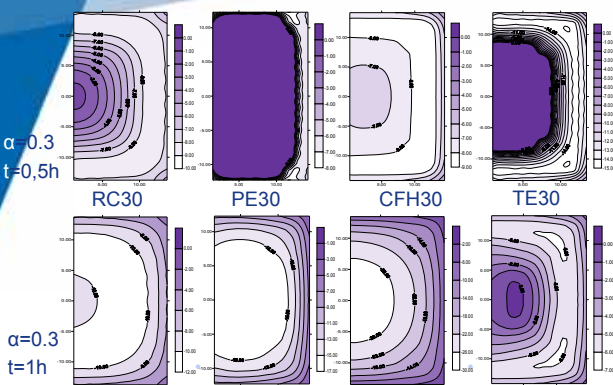
■ -cracked concrete



COMPUTER PROGRAM FIRE

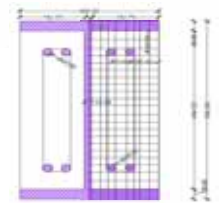
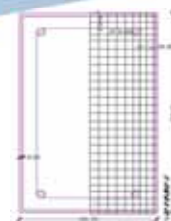
Isobars in the cross section

■ -cracked concrete



CONCRETE FILLED HOLLOW SECTION CFH50

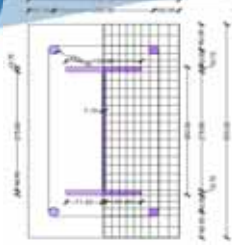
PARTLY ENCASED SECTION PE50



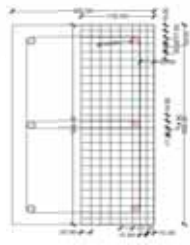
Rectangular Hollow
Section 300.500.8
Reinforcement 4 ϕ 18
 $N_u=9517kN$

HE500B
($b=300, h=500, d=28, t=14.5mm$)
Reinforcement 8 ϕ 20
 $N_u=14027kN$

TOTALLY ENCASED SECTION TE50



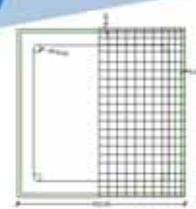
REINFORCED CONCRETE SECTION RC50



IPE160
(b=150, h=300, d=10,7, t=7,1mm)
Reinforcement 4φ20
Nu=6883kN

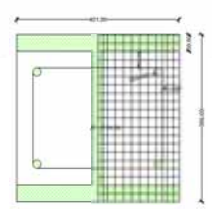
Cross sectional size 30x50cm
Reinforcement 6φ18
Nu=5066kN

CONCRETE FILLED HOLLOW SECTION CFH40



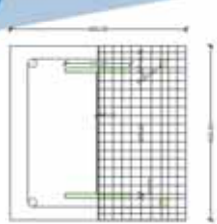
Rectangular Hollow Section 400.400.8
Reinforcement 4φ18
Nu=9817kN

PARTLY ENCASED SECTION PE40



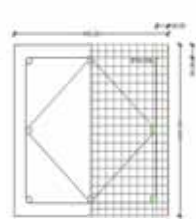
HD400x314 (b=401, h=399, d=39,6, t=24,9mm)
Reinforcement 4φ20
Nu=19963kN

TOTALLY ENCASED SECTION TE30



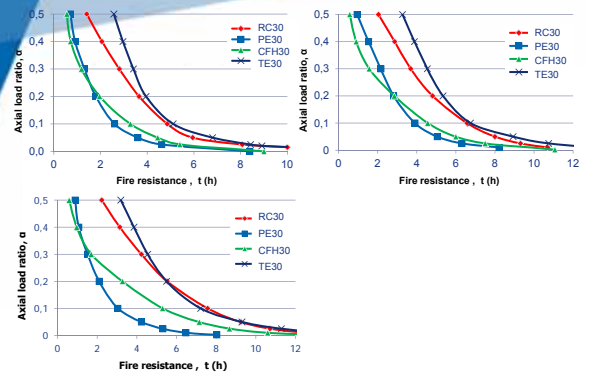
I30
(b=150, h=300, d=10,7, t=7,1mm)
Reinforcement 4φ20
Nu=7183kN

REINFORCED CONCRETE SECTION RC30

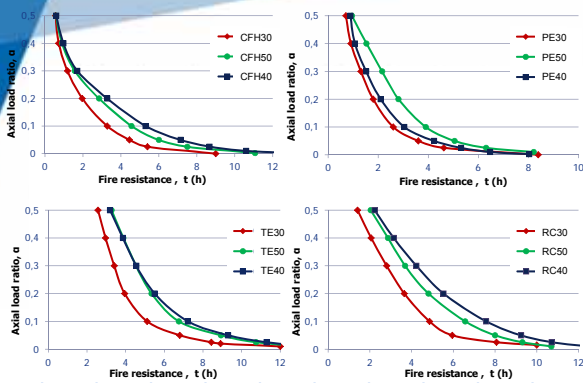


Cross sectional size 40x40cm
Reinforcement 8φ16
Nu=5392kN

COMPARATIVE ANALYSIS



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COMPARATIVE ANALYSIS

-For a load coefficient from 0.1 to 0.3, which is a very common case in practice, the fire resistance of PE and CFH is approximately 35-50% of the fire resistance of TE section

*The steel profiles significantly increase the initial bearing capacity. Because of the peripheral position of the steel it is heated to high temperatures. Reduction of the mechanical properties of steel is caused, which results in lower fire resistance

-The bigger the dimensions are, the slowly the section is heated, achieving higher fire resistance

*There is an exception for the partly encased section - in the section with 40x40cm, the steel profile participates with 25,6%, while in the section with 30x50cm only 17%



THANK YOU !!!

